



Stress corrosion cracking in the context of deep geological nuclear storage

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STRESS CORROSION CRACKING IN THE CONTEXT OF DEEP GEOLOGICAL NUCLEAR DISPOSAL: INVESTIGATIONS ON P235 AND P265 STEELS

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LTC 2016, 6TH INTERNATIONAL WORKSHOP ON LONG -TERM
PREDICTION OF CORROSION DAMAGE IN NUCLEAR WASTE
SYSTEMS, TORONTO, CANADA, MAY 9-12, 2016



CONTENT

Background & experimental procedure

Susceptibility to SCC

Slow strain rate tests
Corrosion Potential & Temperature
Base metal and welded zone

Crack Initiation

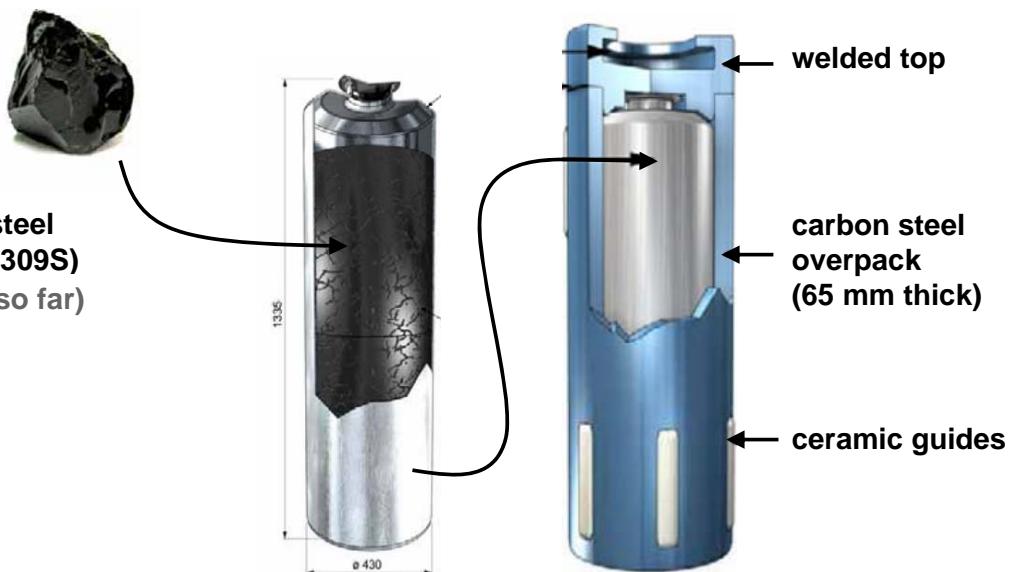
Constant deformation tests
Welded zone
Hardness, Perlite

- ① Vitrified nuclear waste
Limitation of radionuclides' release
(10^5 years)

- ② Stainless steel container (309S)
No function (so far)

③ Carbon steel overpack

Isolation of the vitrified nuclear waste from interstitial water
(10^3 years)

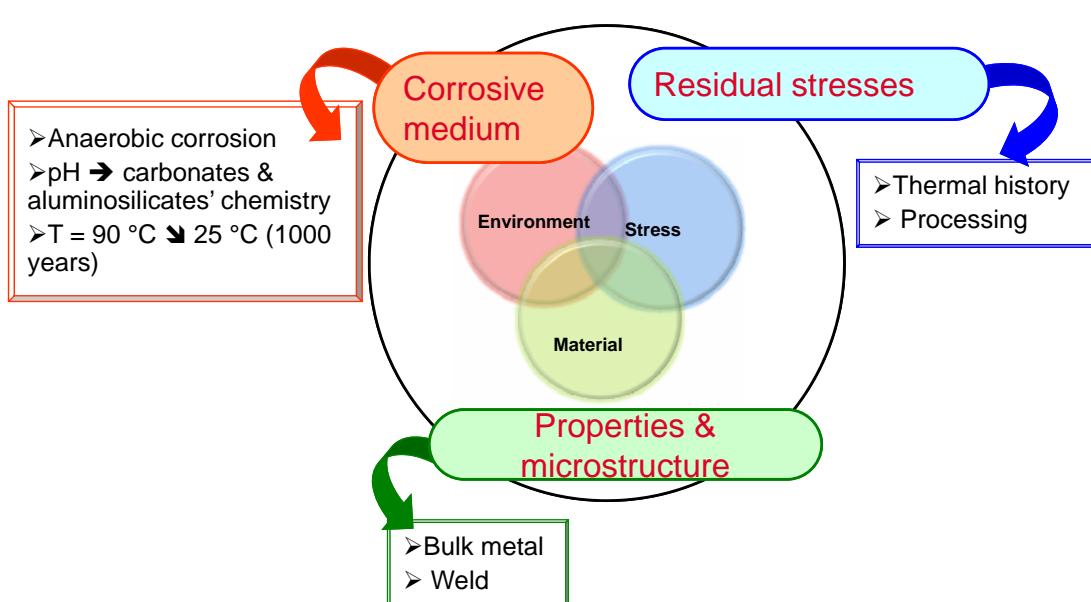


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Sensitivity to stress corrosion cracking of the carbon steel used for the overpack container in the conditions of the storage



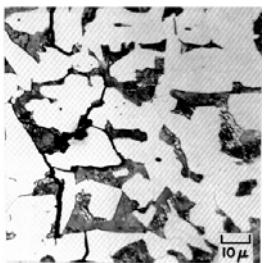
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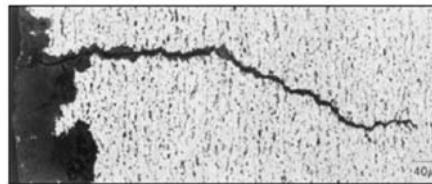
2 cracking mechanisms have been identified in buried pipes,
characterized by specific potential-pH domain

Intergranular



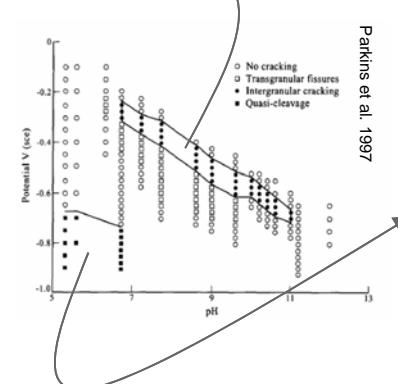
« passive » Steel
alcaline pH

Transgranular



Parkins et al. 1994

« active » steel
quasi-neutral pH
Dynamic loading



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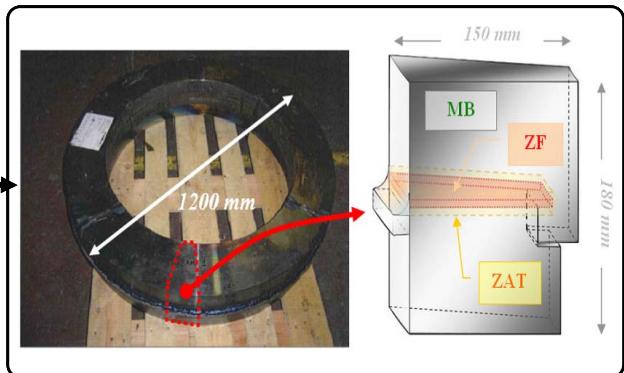
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Coupons have been taken from two mock-ups.

2 grades

P265
→ weld
P235
→ bulk



Composition Massique (%)

	C	Mn	Si	P	S	Al	N	Cr	Cu	Mo	Nb	Ni	Ti	V
P235 GH	0,152	1,08	0,21	0,008	0,006	0,040	-	0,19	0,21	0,05	0,004	0,13	-	0,003
P265 GH	0,116	1,19	0,286	0,012	0,0011	0,040	0,0044	0,032	0,015	0,007	0,000	0,024	0,009	0,001

Caractéristiques mécaniques

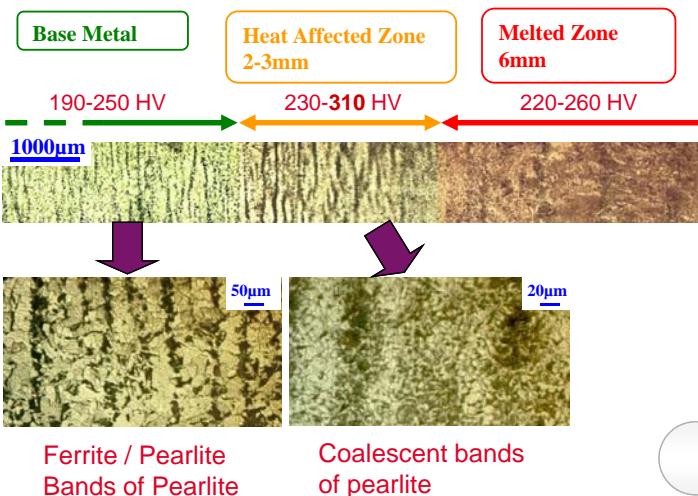
	Rp0,2% (MPa)	Rm (MPa)	At (%)
P235 GH	270	460	32
P265 GH	280	453	40

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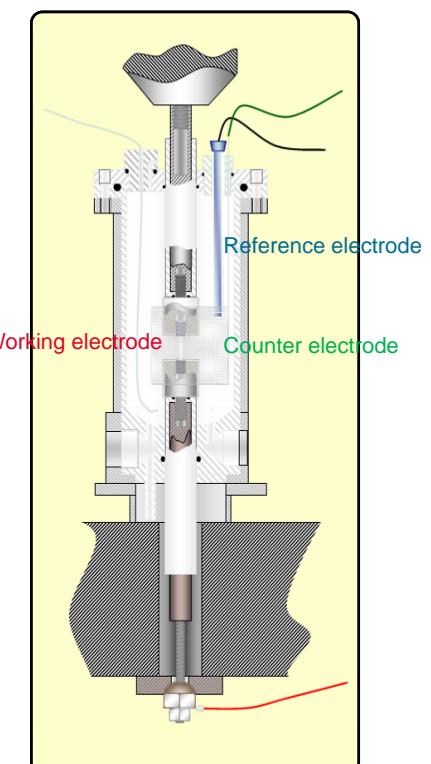
P265 (weld)

P235 (base metal)
Bands of PearliteMicrostructure in bands:
risk of SCCHardness>250Hv
risk of Hydrogen EmbrittlementSensitivity to stress corrosion cracking of
the steel in storage environmentMechanical dynamic solicitations
(10^{-7} à 10^{-4} s⁻¹ → 1 - 800 hours).

- Influence of parameters: corrosion potential, temperature, microstructure...

Environment

- synthetic representative Bure water (Na^+ , K^+ , Ca^{2+} , Mg^{2+} , SO_4^{2-} , Cl^- , HCO_3^-)
- pH ~ 7 (p_{CO_2})
- without oxygen
- 25 et 90 °C.



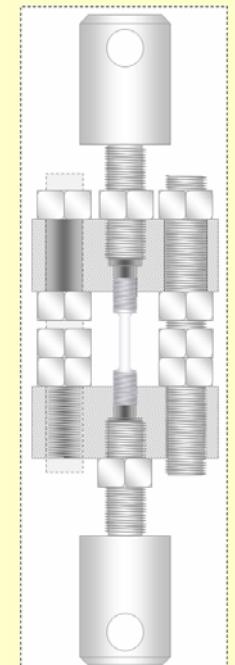
Initiation of stress corrosion cracking under representative conditions (mechanical & chemical)

Static mechanical solicitations

- 2 degrees of initial stresses as function of the yield strength (0,8 et 1,2 Rp_{0,2%}) relaxation (creep, cracks)
- **1 year test** ➔ initiation of the phenomena (not initiation time).

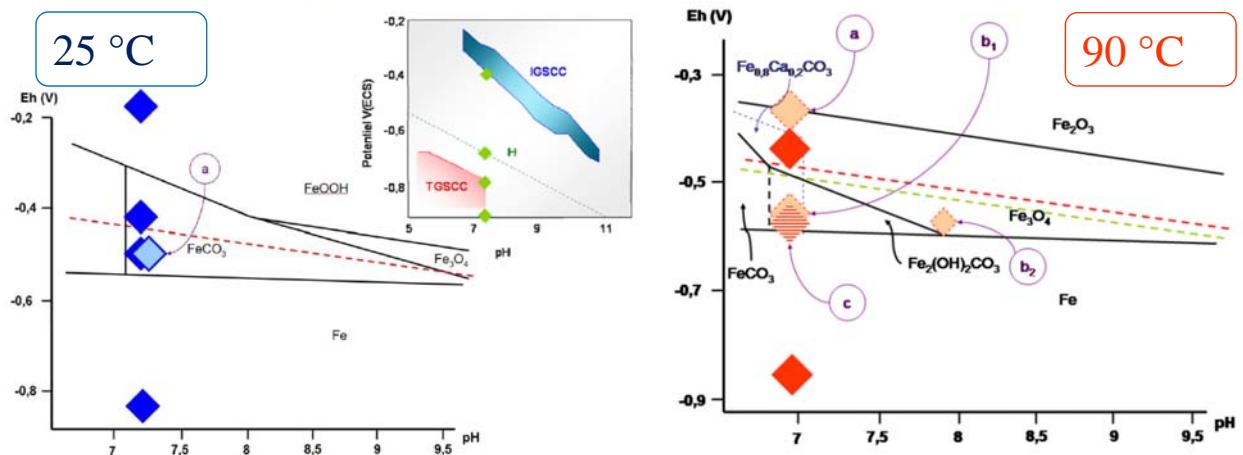
Environment

- Bure clay and bure synthetic water
- pH ~ 7 (pCO₂)
- no oxygen
- 90 °C



SENSITIVITY TO STRESS CORROSION CRACKING

SLOW STRAIN RATE TESTS

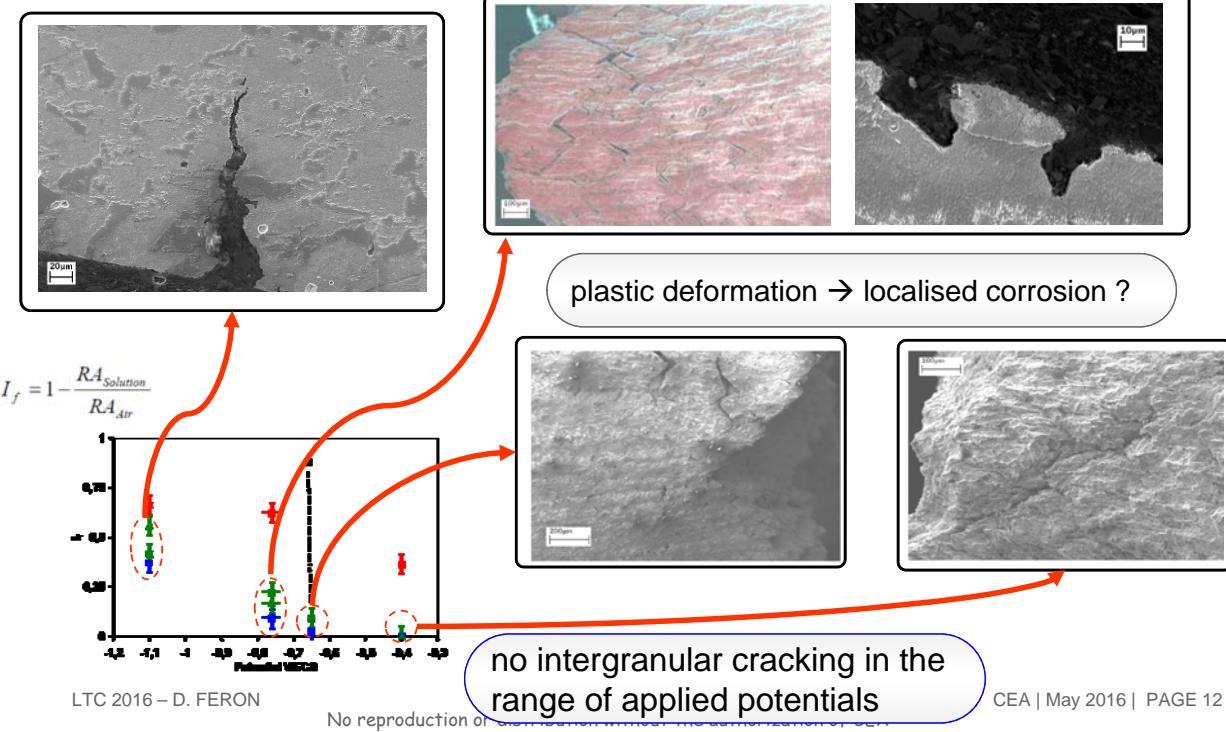


Polarisation potentials used during the slow strain rate tests plotted in the Pourbaix diagram

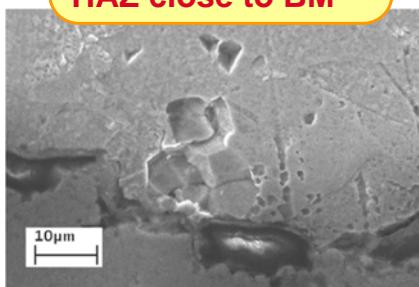
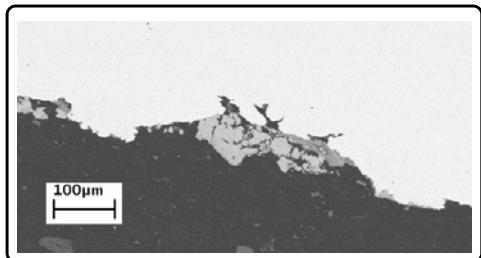
- ❖ a and b₁ are related to measured or calculated corrosion potentials
- ❖ b₂ is related to a measured pH

Transgranular cracking

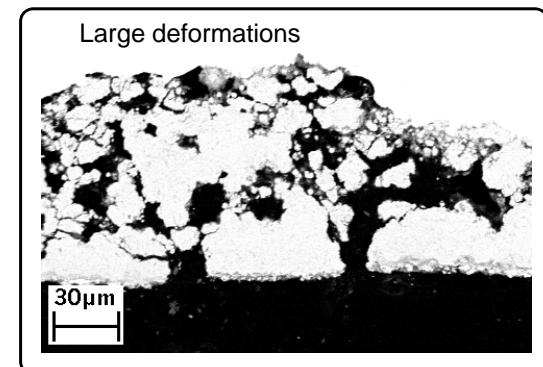
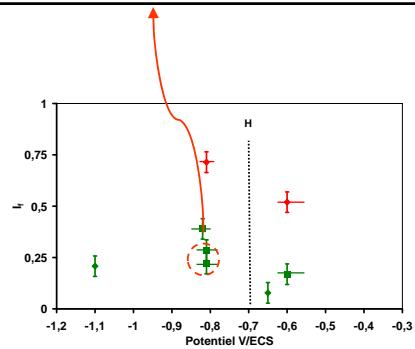
25 °C



Intergranular degradation



90 °C



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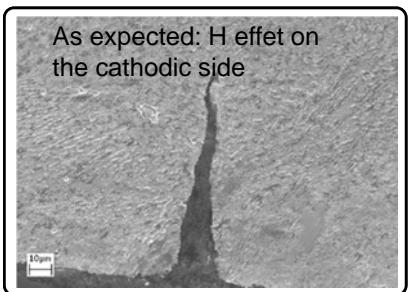
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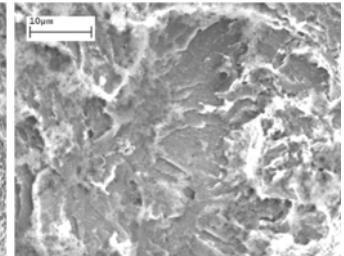
Hydrogen embrittlement at the tested corrosion potentials

25 °C

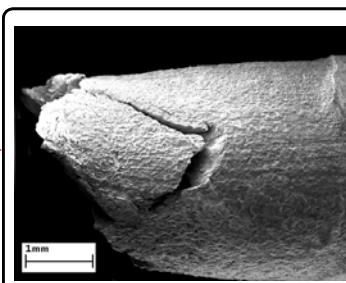
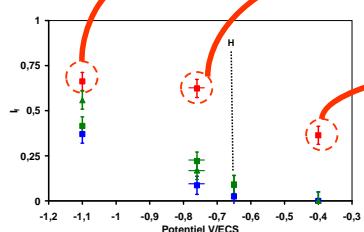
As expected: H effect on the cathodic side



Transgranular cracking after limited deformation



Severe plastic deformation and localized corrosion



Severe plastic deformation and localized corrosion

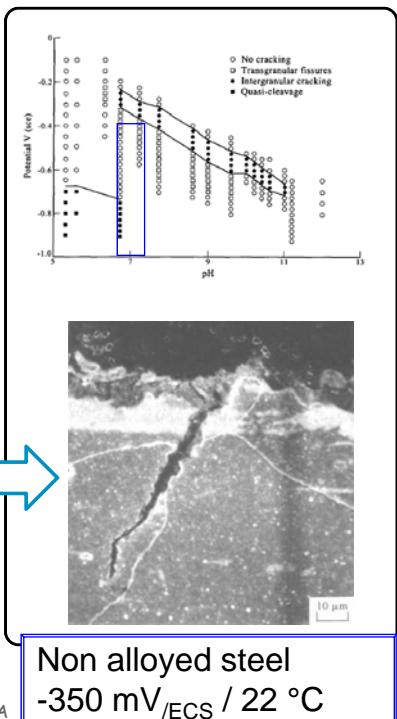
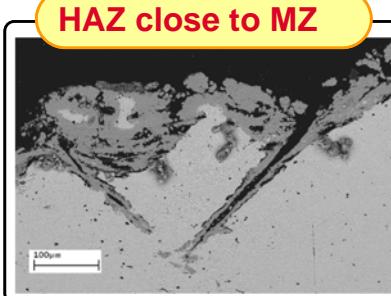
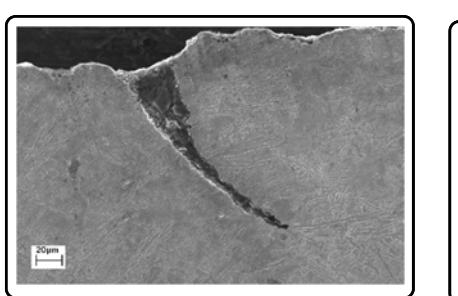
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Hydrogen embrittlement ?
→ plastic deformation & localized corrosion.

90 °C



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SUMMARY & DISCUSSION OF SLOW STRAIN RATE TESTS

Welded Zone

Hydrogen embrittlement at the corrosion potential at 25 °C.

Base Metal

no domain of sensitivity to intergranular cracking in the range of applied potentials at 25 °C

The mechanism of passive film cracking is possible at 90 °C.

With rapid generalized corrosion

brittleness ↗

SCC or too severe test ?

Intergranular attacks

Competition generalized corrosion/SCC?

INITIATION OF STRESS CORROSION CRACKING

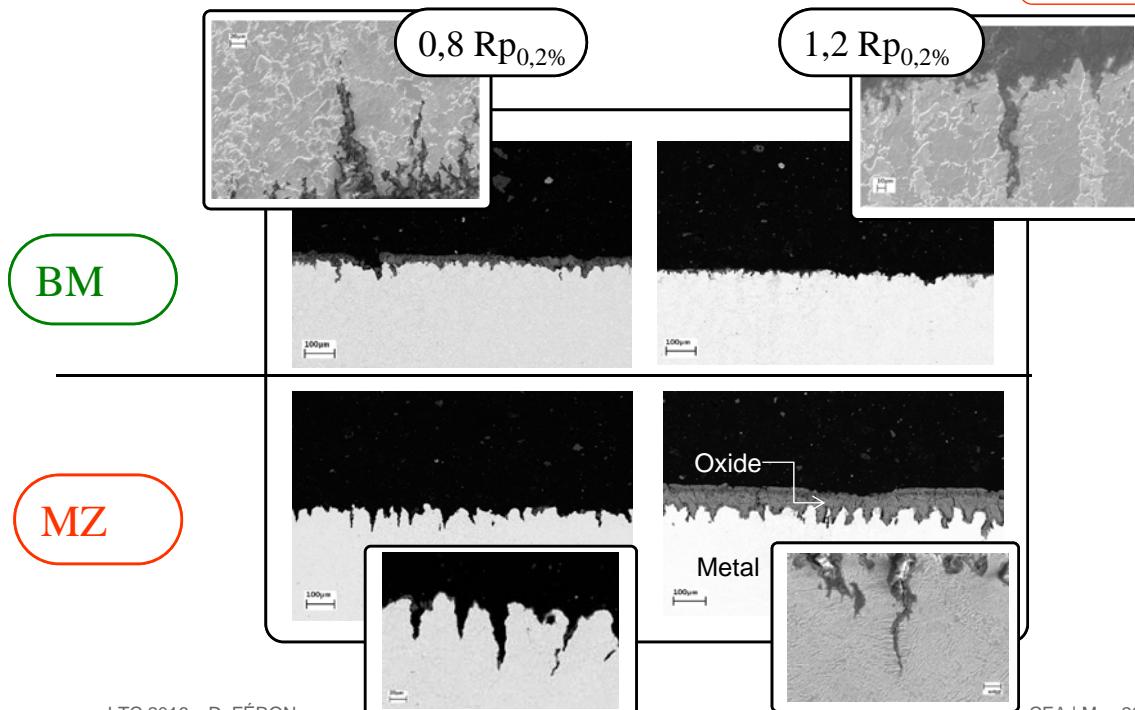
CONSTANT DEFORMATION TESTS

ceaden

P265

After 1 year → Multi cracking in BM and WZ

90 °C



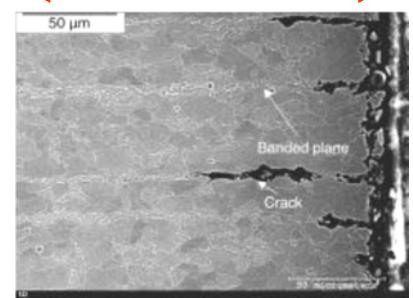
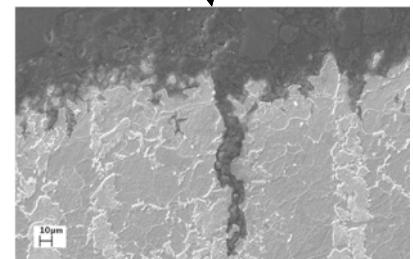
Cracks localized on the pearlite bands.

Cracks resulting from stress?
From chemical attack?

Literature → same results reported,
But not necessarily correlated to the
stress direction.

Galvanic coupling between ferrite and pearlite.

Deleterious effect of band structures.



Chu et al. 2004

Transgranular cracking

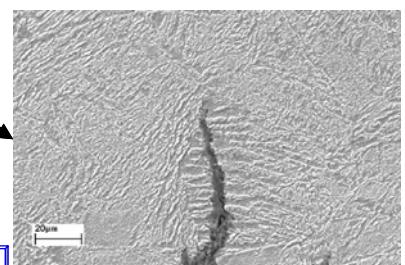
Not localized corrosion (no branching in secondary dendrites)

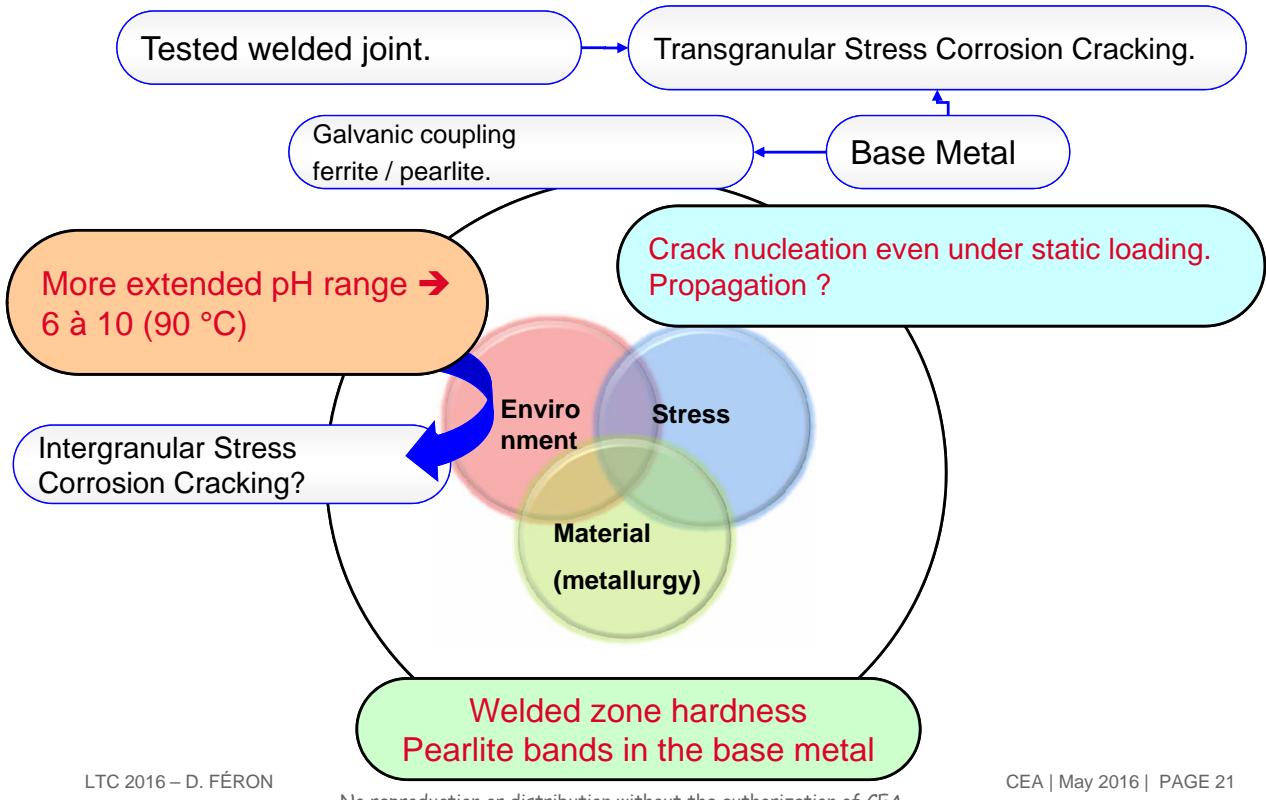
+
Mechanical loading

Hydrogen embrittlement-like phenomenon with
a delayed cracking.

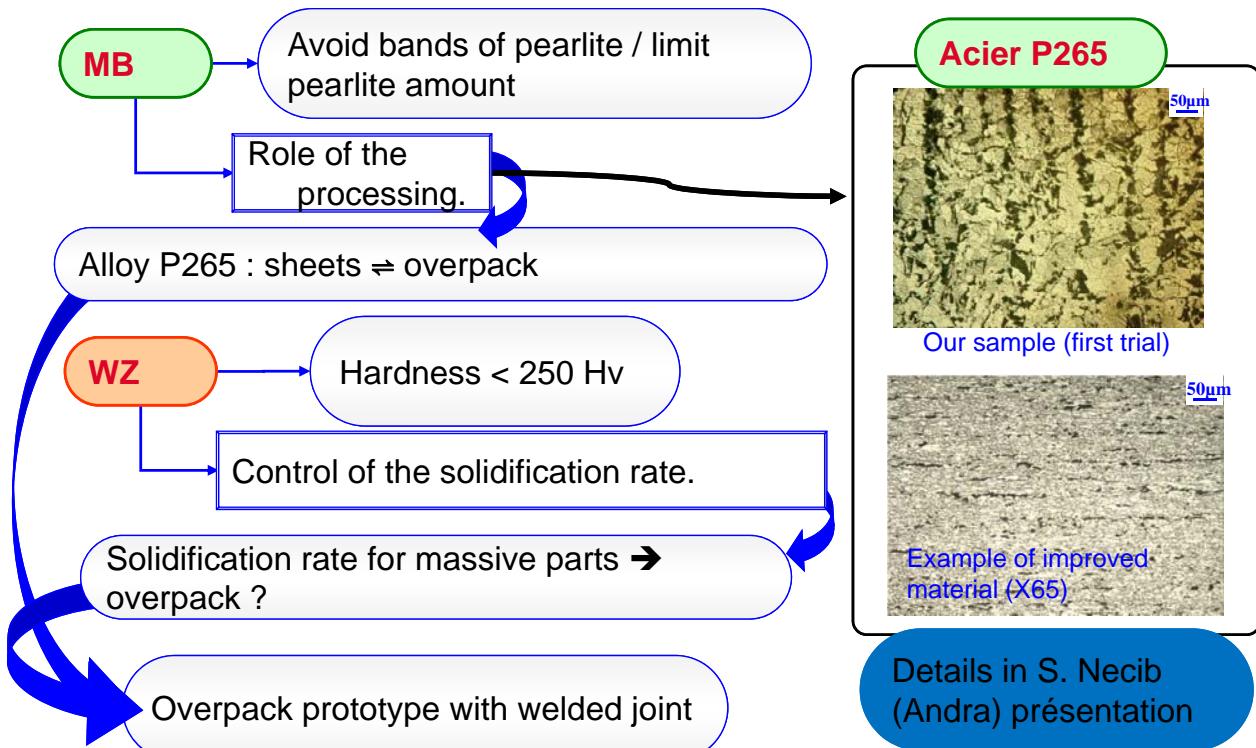
Caused by the excessive hardness of the
welded zone (up to ~ 300Hv)...

... in the case of buried pipes, recommended
hardness shouldn't exceed 250 Hv





TOWARDS NEW MATERIALS LESS SENSITIVE TO SCC



Thank you for your attention



Commissariat à l'énergie atomique et aux énergies alternatives
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