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# Corrosion Behavior of a AISI-316 Stainless Steel Grade Type in Nitrogen **Environnment for a Sodium Gas Heat Exchanger** S. BOSONNET<sup>a</sup>, K. GINESTAR<sup>a</sup>, D. GOSSET<sup>b</sup>, F. BARCELO<sup>b</sup>, B. DUPREY<sup>a</sup>, L. MARTINELLI<sup>a</sup>

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# CONTEXT: Generation IV for nuclear power plants: Energy Conversion System for ASTRID project

**Energy Conversion** in nuclear plants uses to be operated by steam generators. To eliminate the Sodium-Water Reaction Risk , an alternative option of Energy Conversion System operating with gas is developped in the framework of ASTRID project. Heat of the nuclear reaction is recovered by a secondary sodium system and transferred to a 3<sup>rd</sup> circuit containing **Nitrogen** and maintained at 180 bar to make the turbine rotate.

In Sodium-Gas-Energy Conversion System, heat transfer takes place inside modulus comprising 2 channels networks: one for nitrogen and the other one with larger section for sodium flowing. Each channels are separated by a wall of 2 mm thick for good thermal conductivity. Selected material : AISI- 316 SS grade Working conditions in the modulus:

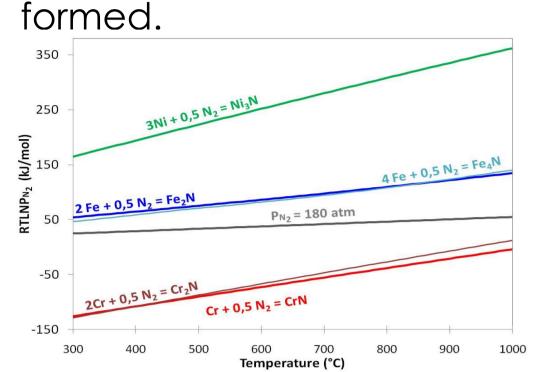
Na: P ~1bar; Inlet  $\theta$ =530°C and Outlet  $\theta$ =330°C N<sub>2</sub>: P=180 bar ; Inlet  $\theta$ =315°C and Outlet  $\theta$ =515°C

## **OBJECTIVES**

Good performance of the ECS has to be guaranteed for **30 years**  $\rightarrow$  Compatibility of the 316L with N<sub>2</sub> environment at 515°C and 180 bar has to be checked.

Stability of main nitrides as a function of  $P_{N_2}$ . Activity values of Fe, Cr, and Ni are the molar fraction in 316L. At 515°C and 180 bar N<sub>2</sub>, CrN and Cr<sub>2</sub>N are potentially If oxygen is present, competition between nitridation and oxidation may occur. **Oxidation susceptibility** to take into account.

Considering that both  $P_{N_2}$  and  $P_{O_2}$  decrease in serial corrosion layers from external to bulk material, thermodynamic diagram suggests 3 scenarios:

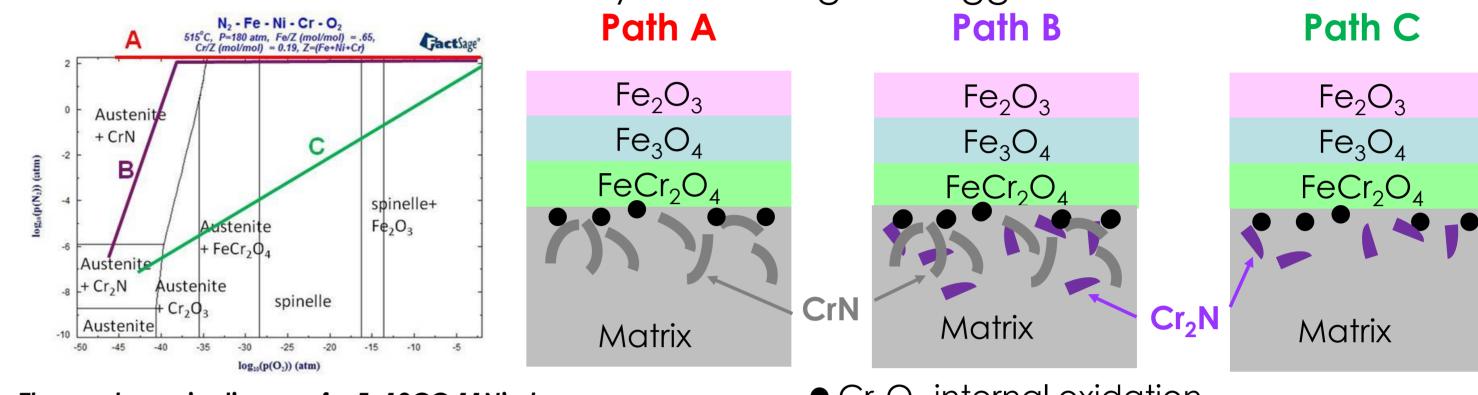


Main nitrides Ellingham diagram Thermodynamic data from HSC database.

Expected phenomenon : •Nitrogen diffusion onto the surface

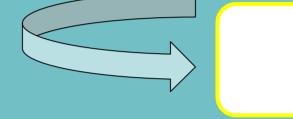
- $\rightarrow$  nitriding layers;
- No continuous layer
- $\rightarrow$  internal nitridation (in the matrix). Severity of damages depends on affected thickness.

 $\rightarrow$  Few relevant data within the ECS conditions : they concern other environment than pure  $N_2$  (NH<sub>3</sub>,  $N_2$ /air or complex atmospheres), other materials (Nibased alloys) and higher temperature.



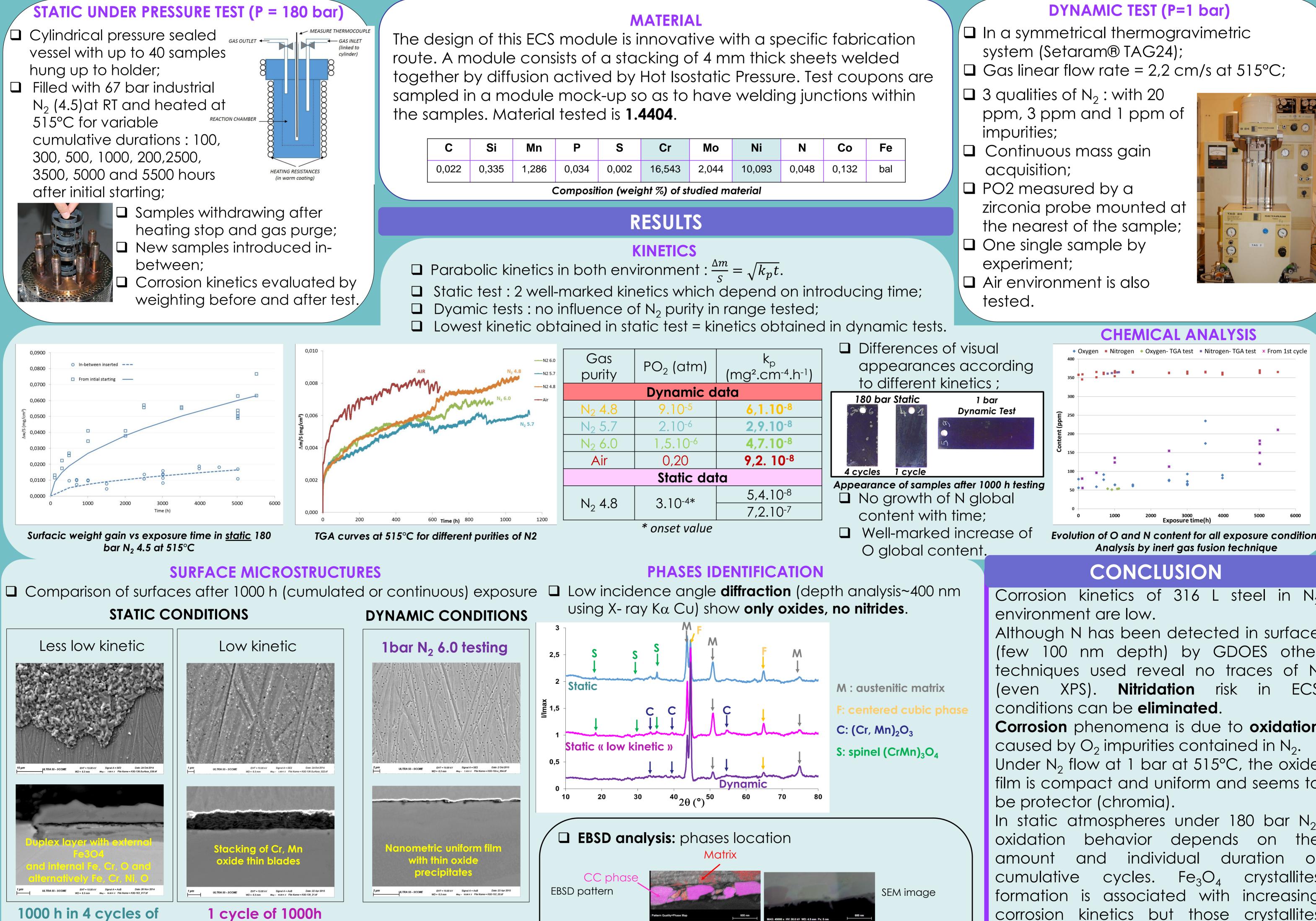
Thermodynamic diagram for Fe19CCr11Ni at 515°C and 180 bar. Obtained with FactSage.

•  $Cr_2O_3$  internal oxidation

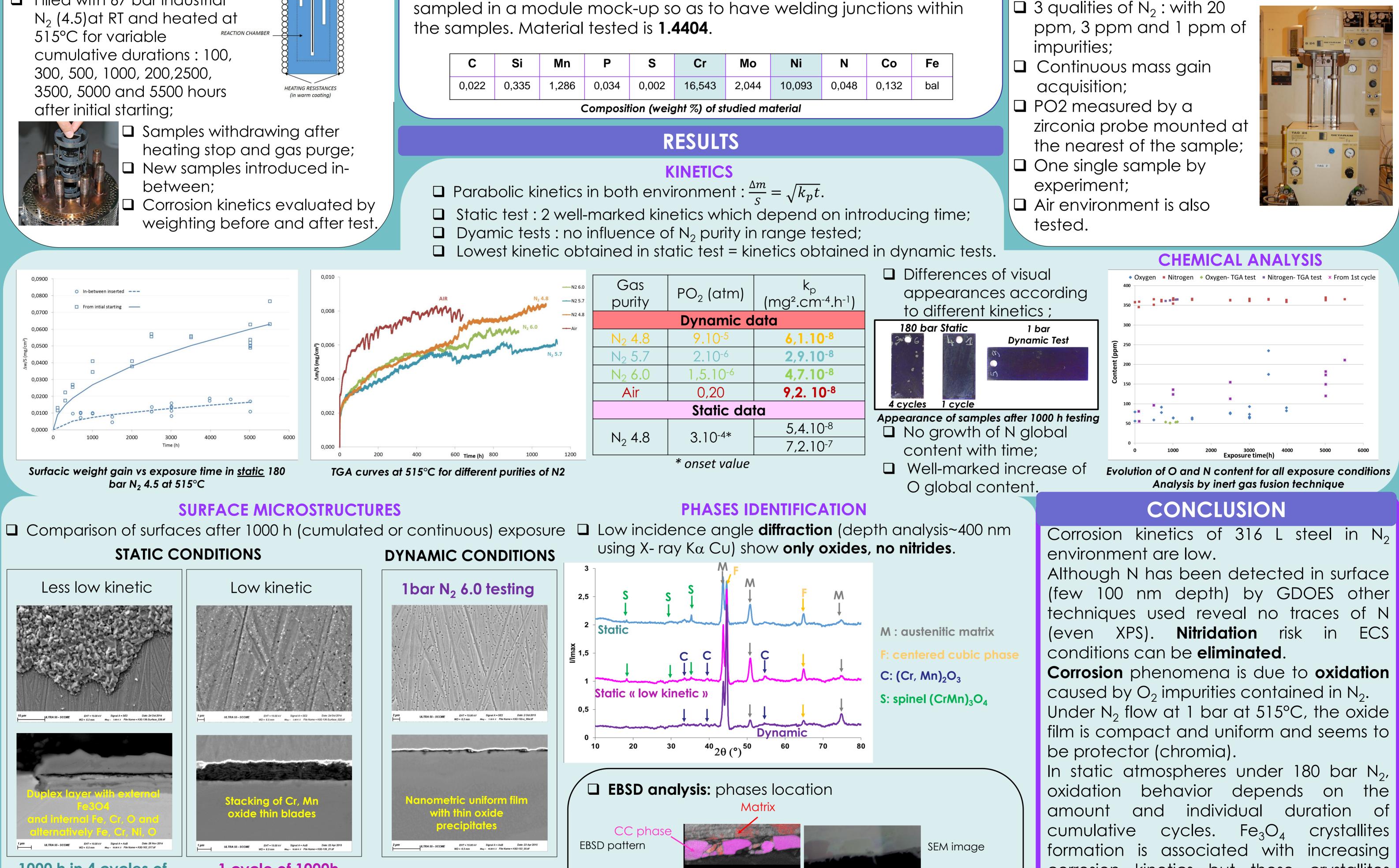


Literature do not rule on the absence of damaging on 316L in ECS conditions. Experimental program set up to acquire long term corrosion kinetics (up to 5000 hours)

# **EXPERIMENTAL**



С	Si	Mn	Р	S	Cr	Мо	Ni	N	Со	Fe
0,022	0,335	1,286	0,034	0,002	16,543	2,044	10,093	0,048	0,132	bal



## 1000 h in 4 cycles of 100+200+200+500 hours

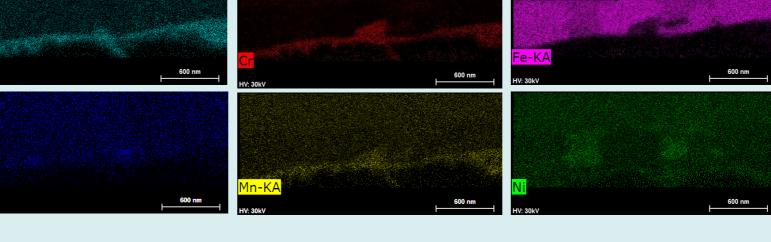
- After static under pressure tests, surfaces are heterogeneous : nanometric films and micrometric layers (with different morphology depending on the number of cycles). They are homogeneous for all dynamic tests.
- 2 kinds of oxides form on surface during static test : spinel and chromia containing Mn while main chromia in dynamic test.
- In both cases a new c.c phase in underlying metal (with Fe and Mo).

**Corrosion** phenomena is due to **oxidation** Under N<sub>2</sub> flow at 1 bar at 515°C, the oxide film is compact and uniform and seems to

In static atmospheres under 180 bar  $N_2$ , the individual duration of crystallites increasing corrosion kinetics but those crystallites change with long period cycles.

# PROSPECTS

In static conditions, gas content is gradually  $O_2$  depleted and the consequences of this depletion will be studied to understand mechanisms in **non-stationary environment**.



600 nm

Elemental EDS- X mapping