

A 3D spectral finite element solution to simulate ultrasonic inspection of austenitic welds

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VIRTUAL CONFERENCE JULY 28-30, 2021





FROM RESEARCH TO INDUSTRY

A 3D spectral finite element solution to simulate ultrasonic inspection of austenitic welds

July 28-30, 2021 – Annual Review of Progress in Quantitative Nondestructive Evaluation

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The ADVISE Project

About the project

- Funded by the European Commission's EURATOM programme under the Horizon 2020 framework programme for Research and Innovation
- 13 partners
- Started in September 2017 and lasting 4 years

Overall objective

- enhance the ultrasonic inspection of complex structures materials in order to **improve confidence and reliability**



Our goal in WP1:

- propose **UT modelling tools** well-adapted to parametric study for UT technique design and data analysis for complex microstructure materials in welds
 - \Rightarrow "seek a compromise between weld description accuracy and computational cost"

Euratom

Horizon 2020

ba

London

Imperial College

cea

Macroscale modelling

effective material consideration

P

Eddyfi Technologies

framatome

University of BRISTOL

Arttic



Phenomenological aspect for UT inspection and effective material consideration

NDT in microstructured material (λ/D >>1, D grain size)



Effective material properties for coherent wave propagation

- Equiaxed grain with random crystal orientations



 \Rightarrow isotropic damped material

- austenitic welds: **elongated grains** with preferential texture <100> around grain elongation axis



⇒ anisotropic (quasi-hexagonal) damped material whose symmetry axis is correlated with elongation axis



Inputs for weld material using macroscale approach

Properties of the effective media

- Anisotropic viscoelastic constitutive law
- Definition of complex stiffnesses to fit wave velocities and attenuation variations w.r.t. wavefront directions

 $\Rightarrow C_{ij}(\omega_0) = C'_{ij}(\omega_0) + iC''_{ij}(\omega_0)$



						. CIV N·D·Ξ
Sti	iffness matrix <mark>(</mark> GPa)) - elastic properties				
	220	135	135	0	0	0
	135	245	110	0	0	0
,	135	110	245	0	0	0
j 🛛	0	0	0	80	0	0
	0	0	0	0	110	0
	0	0	0	0	0	110
Vi	iscosity matrix (GPa)				
	1.6	2	2	0	0	(
	2	12	2.5	0	0	C
!!	2	2.5	12	0	0	C
J	0	0	0	2.7	0	C
	0	0	0	0	4.3	C
	0	0	0	0	0	4.3

Typical values for the stiffnesses of an effective material consisting of a set of elongated grains mainly oriented along the **1** axis

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Inputs for weld material using macroscale approach

- ► Grain orientation mapping in the bevel
 - Local definition of the main elongation axis





A complementary solution to ray models in order to provide reference results





Mapping

- Efficient ray model but limitations on various cases (caustics, surface wave, diffraction...)
- In practice difficult to anticipate these issues
- \Rightarrow Need 2D/3D FEM simulation as references





A dedicated Spectral Finite Element Method (SFEM)

- ► High-order mass-lumped FEM:
 - full explicit time-transient solver with diagonal mass matrix
- Parametric hyper mesh structure of the UT scene:
 - domain decomposition into macro-elements (MEs) containing material and geometrical inputs
- Mortar element method used for MEs interactions
- **Each ME carries a structured refinement w.r.t.** λ
- Optimal data structure for parallelization and memory load



<u>A. Imperiale et al., Int. J. Numer. Methods Eng., 2019</u> DOI: 10.1002/nme.6080



Objective: to enable macroscale FE simulations for 3D cases on PC for realistic configuration sizes





Features already using SFEM code in CIVA

FE Grid Defect (CIVA 2020) – UT inspection



► CIVA SHM (CIVA 2020 SP3)



Composite inspection (dev only)



 FE BEAM UT (available in the CIVA project version, planned 2022 for commercial release)
FE solution for 3D field computation in welds







FE BEAM UT: PRINCIPLE

Weld-oriented hybrid technique coupling ray model and SFEM

- Ray-based calculation of the source field in the coupling above the specimen
- Automated build-up of the high-order SFEM hexahedron mesh



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A FEM code including anisotropic damping effects of the weld material

- Consideration of coherent wave energy losses from scattering by the microstructure: anisotropic viscoelastic constitutive law
- Different schemes proposed:
 - Maxwell (constant attenuation w.r.t. frequency)
 - Zener (linear attenuation w.r.t. frequency)
 - Kelvin-Voigt (quadratic attenuation w.r.t. frequency)



Inviscid O(h)O(1) $3 \times N_h$ 1 $O(h^2)$ Kelvin-Voigt $O(Q_{\star})$ $3 \times N_h$ 2 $O\left((I + Q_{\star}^{-2})^{-\frac{1}{2}}\right)$ O(h) $3 \times N_h + 2 \times N'_h$ Maxwell 1 $O\left((I+Q_{+}^{-1})^{-\frac{1}{2}}\right)$ O(h)2 $3 \times N_h + 2 \times N'_h$ Zener TABLE 1 Qualitative A. Imperiale et al., Int. J. Numer. Methods Eng., 2020 comparison of fully discrete DOI: 10.1002/nme.6359 explicit viscoelastic propagators

Cross-validation with ray-based computation using Maxwell scheme with calibration procedure at the main frequency

CFL vs Q*

CFL vs h

= main grain orientations

- Validation in homogenous cases for various grain orientations (L0 – 2MHz)
- Very good agreement for simulating anisotropic damping and beam deviation





Nb. of stiffnesses

Memory cost

FE BEAM UT: FEATURES

Other advantages

► Applicable to the main probe classes handled in CIVA

- immersion and wedge contact probes (rectangular, circular or elliptical shapes and focus settings)
- single element or any phased array patterns (linear, matrix, dual probe...)

Field extraction in a 2D or 3D region of interest using CIVA analysis panels

ROI dimensions: $20\lambda_T \ge 20\lambda_T \ge 50\lambda_T$ at 2MHz

Macroscale description with low-memory requirements

- e.g. for the current use case at 2MHz
 - Homogeneous Isotropic < 1 GB
 - Heterogeneous anisotropic < 6 GB

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150 Pacific Pacific

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3D field computation on the backwall of a cylindrical welding component

PA probe with focusing law on the backwall

- 2MHz wedge probe (nominal L45) linear 48 elements point focusing law
- Ogilvy description using anisotropic damped material properties
- Simulated time for wave propagation to the bottom: 20 µs

Point focusing law computation considering an isotropic metal

Superposed SFEM results with ray tracing analysis

3D field computation on the backwall of a cylindrical welding component

- Quantification of weld material properties
 - Beam deviation
 - Beam damping

3D field computation on the backwall of a cylindrical welding component

- Performances obtained on
 - Single workstation using Intel[®] Xeon[®] W-2155 Processor (13.75M Cache, 3.30 GHz)
 - # of Cores 10 (# of Threads 20)

°							
	20 μs at 2MHz	Time step and # of iterations	Computation Time FE BEAM 3D	Computation Time FE BEAM 2D			
	Isotropic	1.2e-2 μs 1650 iterations	≈25 min	< 3s			
	Weld (no damping)	4e-3 μs 5000 iterations	≈75 min	< 10s			
	Weld (with damping)	4e-3 μs 5000 iterations	≈85 min	< 10s			

Summary of the present work

- An hybrid ray/SFEM technique
 - Ray model used for radiated beam definition at the surface of the sample
 - SFEM used for wave propagation into the whole sample reduced to a ROI
- Simulation tool fully integrated into the CIVA platform environment
- ► A complementary FEM solution to ray-based simulations in weld
 - Provide FE reference solution
 - Very efficient in 2D allowing intensive parametric studies
 - Low memory and computational cost in 3D (several GB and of the order of a few hours)

Next challenges within the FEM in welds

- Geometric distortion and variation of the weld bevel
- Taking into account the geometry of the passes according to a MINA technical description
- Introduction of a 3D flaw-area and propose echo response synthesis
- Adding structural noise in the FEM propagator

Cea

Thank you for your attention

Please feel free to send any questions and more details after this short presentation!

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