



## Manufacturing of $(U,Pu)O_{2-x}$ mixed oxides with high plutonium contents ( $\geq 60$ mol.% Pu)

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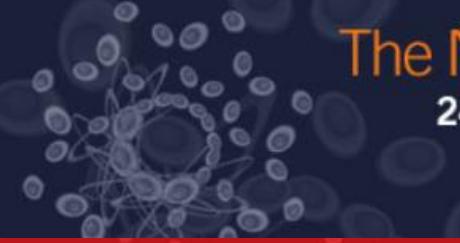
HAL Id: cea-04743910

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## Manufacturing of $(U,Pu)O_{2-x}$ mixed oxides with high plutonium contents ( $\geq 60$ mol.% Pu)

DE LA RECHERCHE À L'INDUSTRIE

M-M. Desagulier<sup>1</sup>, P.M. Martin<sup>1</sup>, J. Martinez<sup>2</sup>, C. Guéneau<sup>3</sup>, N. Clavier<sup>4</sup>

<sup>1</sup> CEA, DES, ISEC, DMRC, SASP, Université Montpellier, Marcoule, France

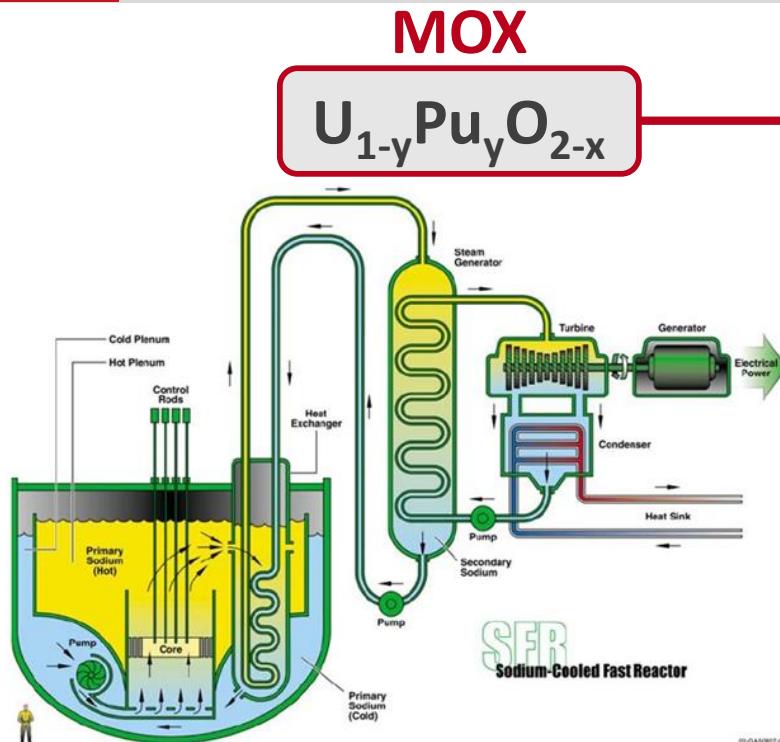
<sup>2</sup> CEA, DES, ISEC, DMRC, SPTC, Université Montpellier, Marcoule, France

<sup>3</sup> Université Paris-Saclay, CEA, SCCME, Gif-sur-Yvette, France

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# Context (1/4) – MOx fuels for Sodium-cooled Fast Reactor



Currently studied as part of the fast reactors development.

	MOX fuel for SFR
Pu content (y)	$0.15 < y < 0.35$
O/M	$1.94 < O/M \leq 1.99$
Porosity (%)	5%
Density	95 % TD
Microstructure heterogeneity	$PuO_2 < 100 \mu m$ $UO_2 < 200 \mu m$

SFR (Sodium Fast Reactor) as ASTRID or Phenix reactor [1]

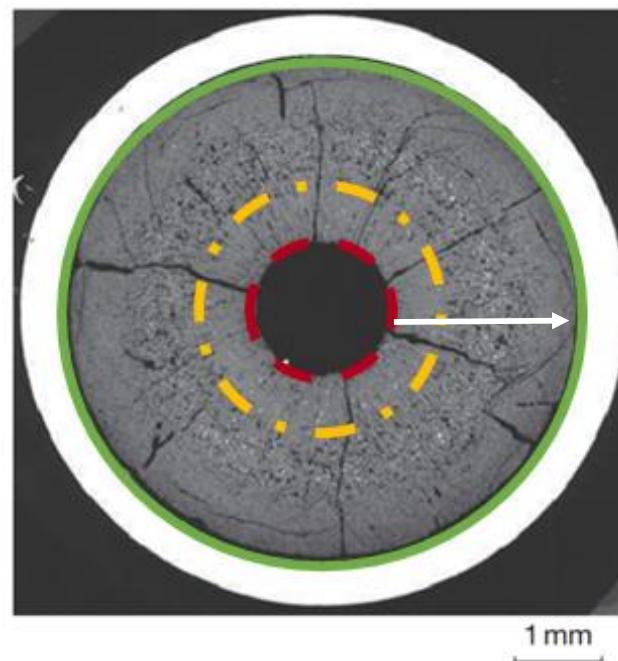
The main phenomena occurring at the beginning of life and high-temperature effects: fuel restructuring, radial redistribution of fuel constituents, and geometrical evolution.

[1] Direction de l'énergie nucléaire, le démonstrateur technologique ASTRID, 2012.

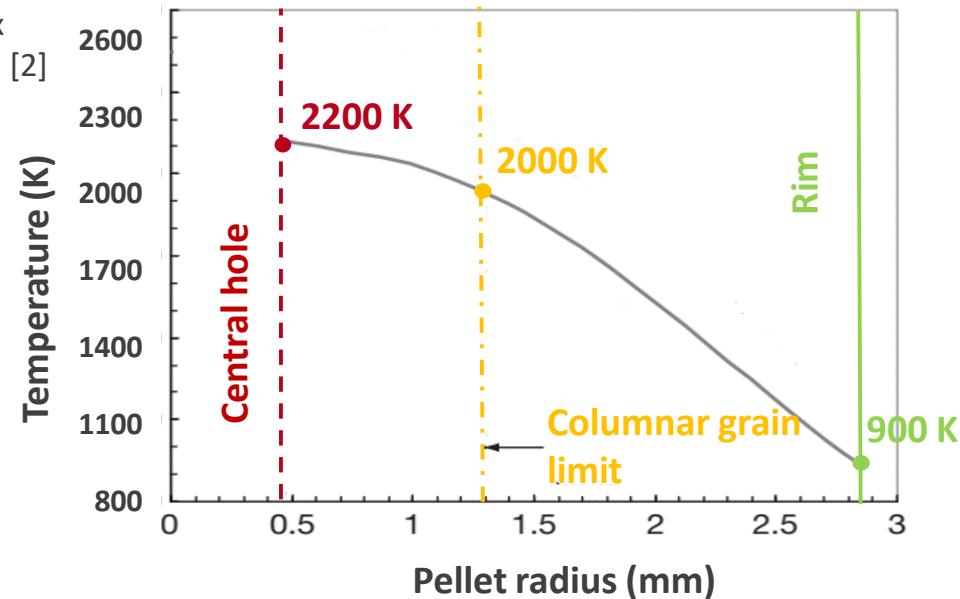
# Context (2/4) – Thermal gradient in MOx fuels

Under irradiation : Linear power 400-500 W.cm<sup>-1</sup>

Thermal Gradient from 900 K to over 2200 K



Micrograph of a Phenix pellet (Max flux plane) [2]  
Pu content :  $y = 0.20$   
 $O/M^* = 1.978$   
Burnup: 13 at. %  
**Central hole**  
**Columnar grain limit**  
**Rim**



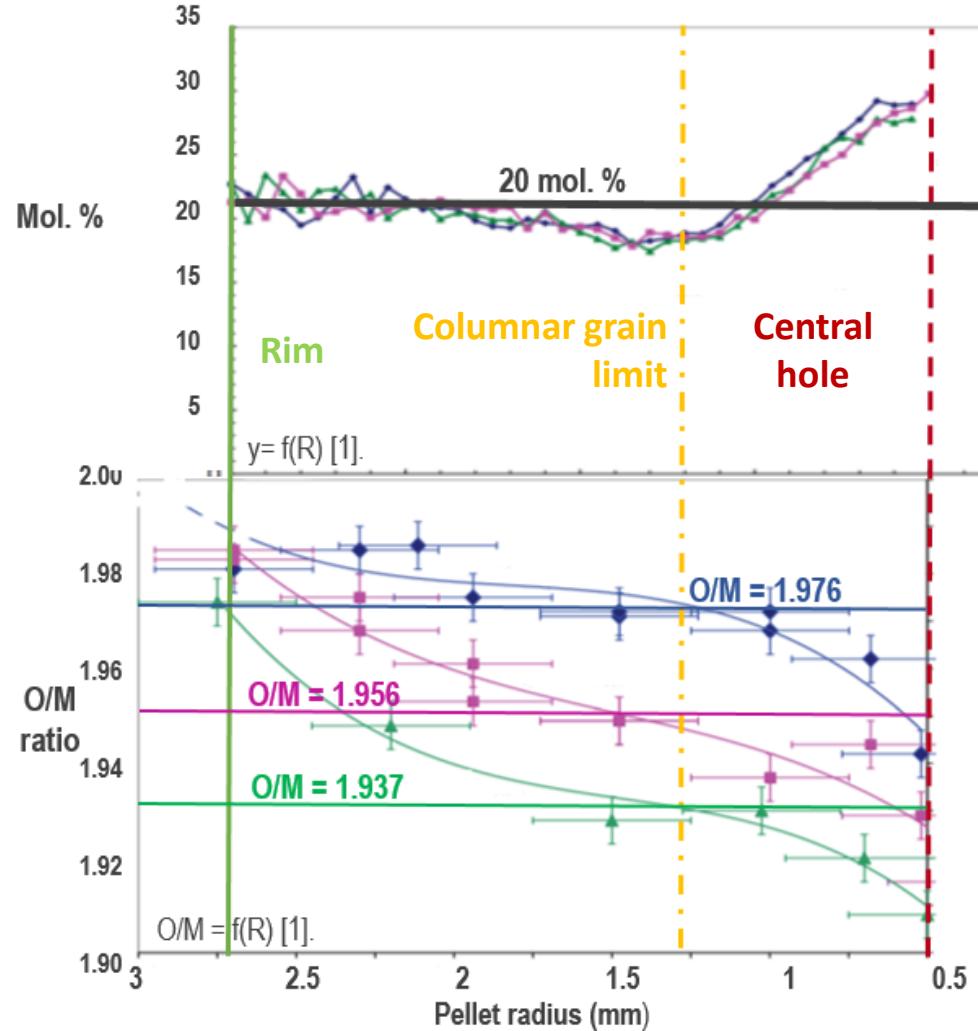
A 1300 K thermal gradient along the pellet radius is observed

\* with  $M = U + Pu$

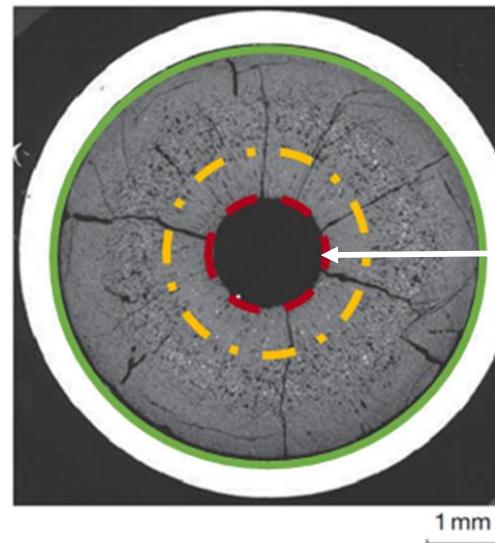
[2] Y. Guerin, C. Nucl. Mat., edited by Rudy J.M. Konings, (2012) 547-78.

# Context (3/4) – Redistribution of Pu and O atoms

Variation of the Pu content and the O/M ratio along the pellet radius for 3 different initial O/M ratios



Pu content ( $y$ )	$0.15 < y < 0.35$
O/M	$1.94 < \text{O/M} \leq 1.99$



Micrograph of a Phenix pellet (Max flux plane) [2]  
Pu content :  $y = 0.20$   
 $\text{O/M}^* = 1.978$   
Burnup : 13 at. %  
Central hole  
Columnar grain limit  
Rim

At max flux plane

	%Pu	O/M
Rim	==	green arrow
Columnar grain limit	yellow arrow	==
Central hole	red arrow	red arrow

%Pu can locally reach up to 70 %

\* with  $M = U + Pu$

[2] Y. Guerin, C. Nucl. Mat., edited by Rudy J.M. Konings, (2012) 547-78.

## Impact on the structural, microstructural and thermodynamic properties

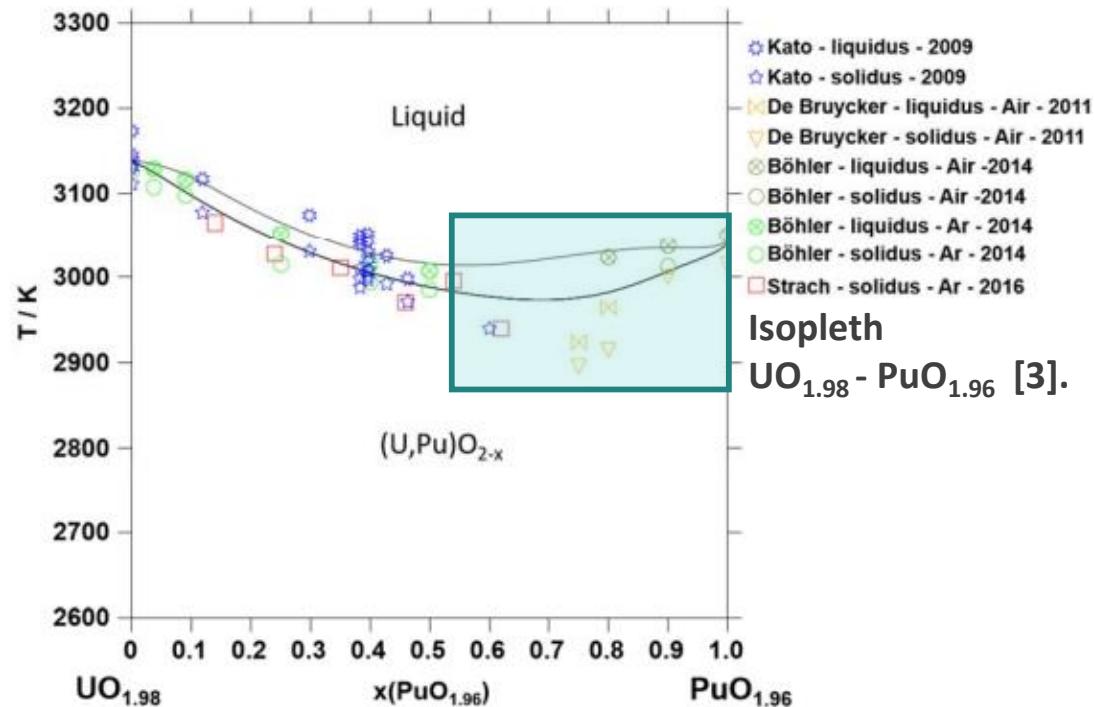
### Example of the melting point

The local melting point depends upon both the O/M ratio and the Pu content



$T_{melt}$  as Pu content  
(for  $y < 0.75$ )

=> diminution of the margin to fuel melting



### Goals

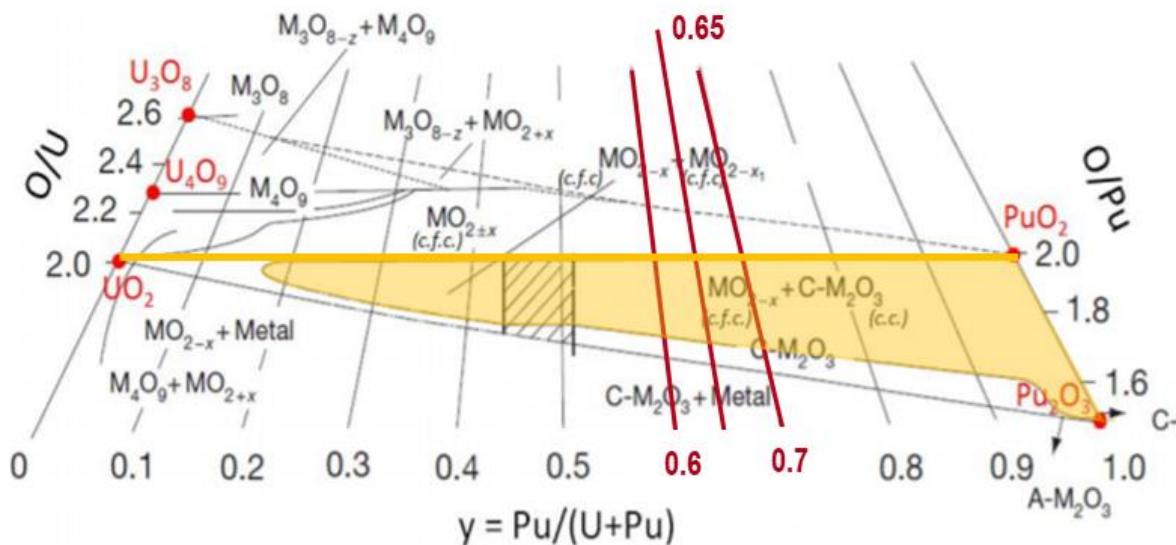
Fill the lack of data (structural, microstructural, thermal and thermodynamic) for MOX with Pu content greater than 0.45 and more specifically for Pu > 0.60



Feed the database for the fuel performance codes (GERMINAL) and enhance the modelling of the U-Pu-O phase diagram by the CALPHAD method.

## Required properties for thermodynamic properties measurement

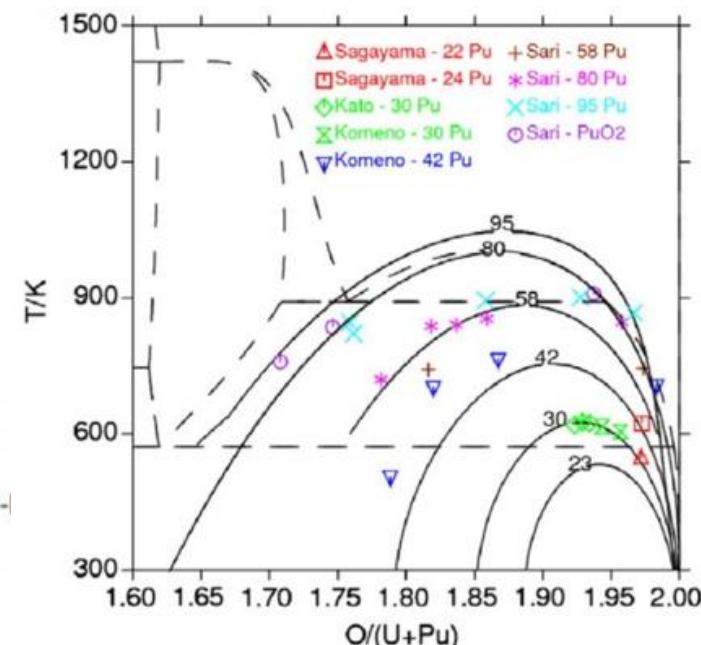
- Density after sintering > 94% TD
- Homogeneous chemical distribution of cations and oxygen (O/M ratio)
- Monophasic (solid solution) and stoichiometric (O/M = 2.00) material



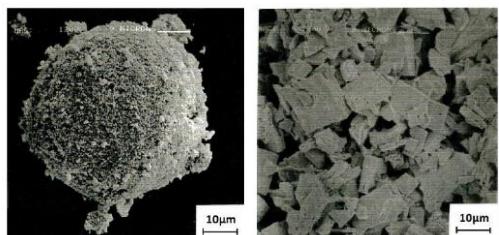
Ternary phase diagram U-Pu-O at **room temperature** for an O/M ratio between 1.5 and 2.7 [4]

[4] C. Guéneau *et al.*, *J. Nuc. Mat.* (2012) 21-59.

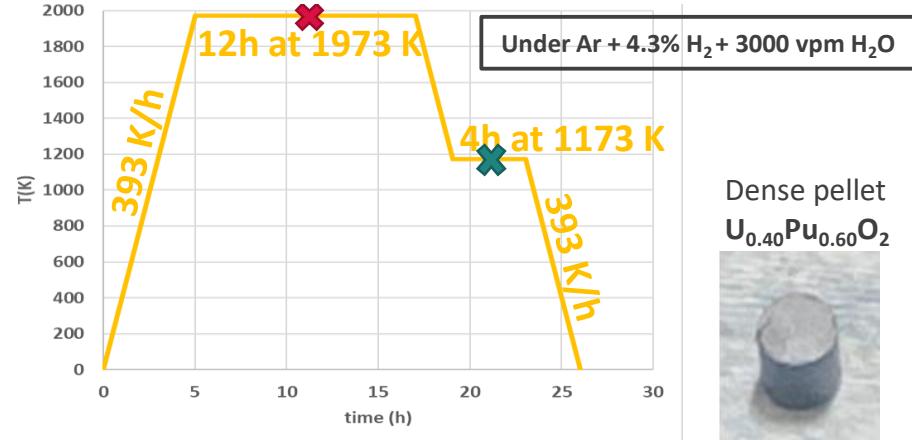
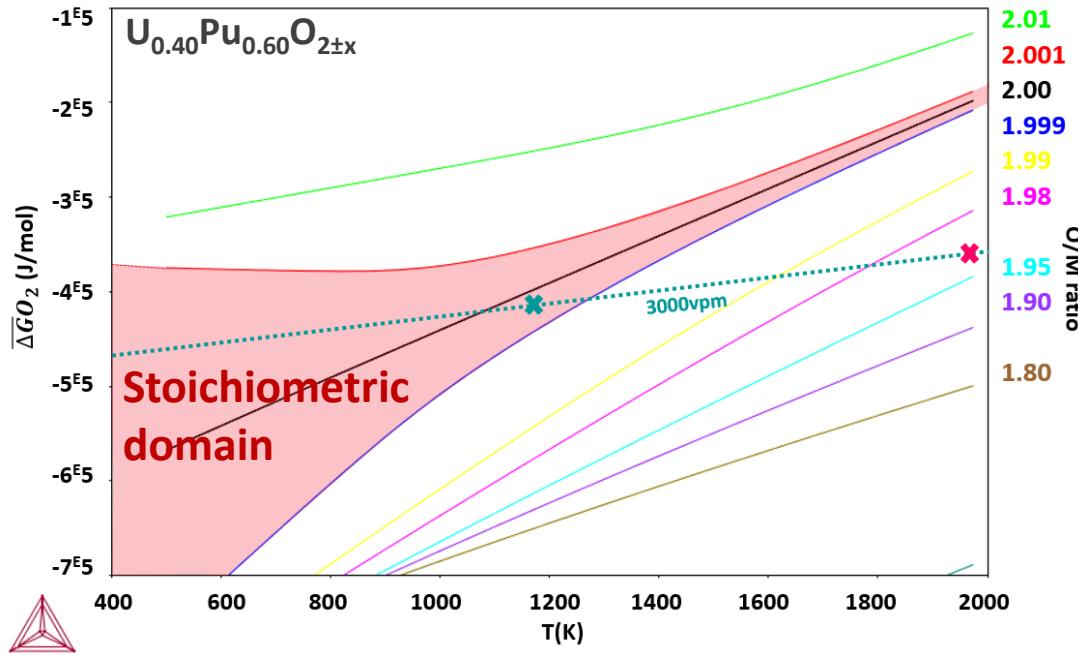
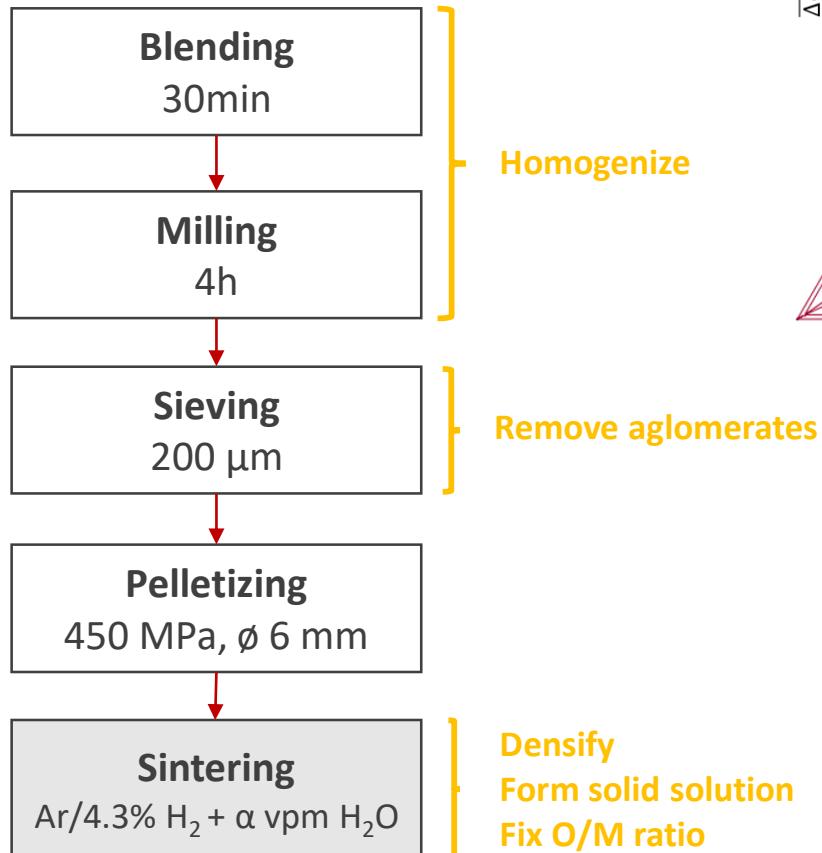
[5] C. Guéneau *et al.*, *J. Nuc. Mat.* 419 (2011) 145-167.



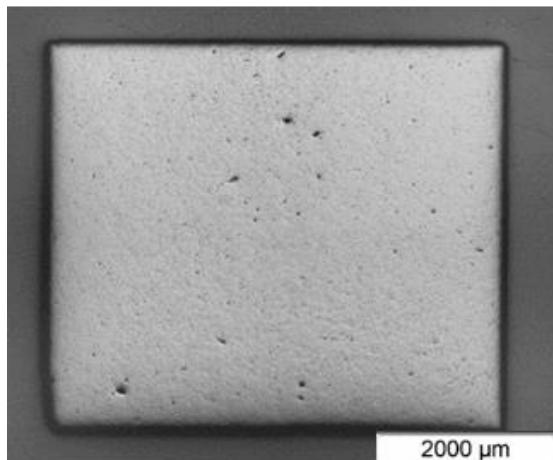
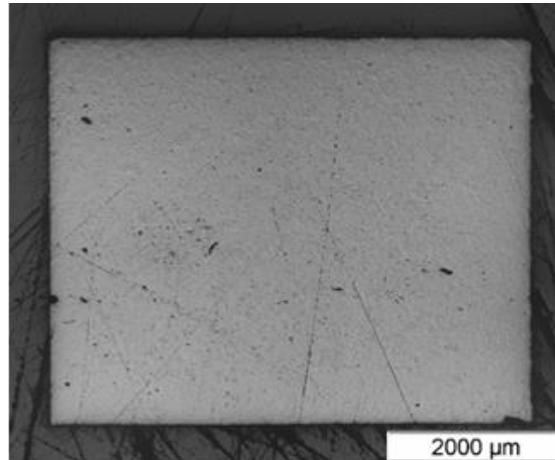
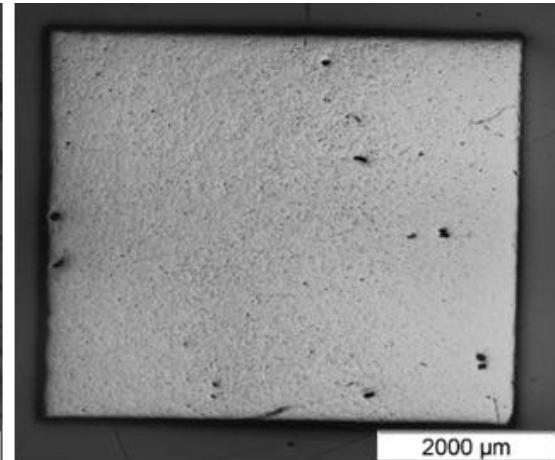
Phase separation temperature calculated as a function of the O/M ratio [5].



$\text{UO}_2$        $\text{PuO}_2$



- [6] T. Truphemus, Thèse de doctorat (2013), University of Aix-Marseille.
- [7] R. Vauchy et al., Ceramics international 40 (2014), 109991-10999.

$\text{U}_{0.40}\text{Pu}_{0.60}\text{O}_2$  $\text{U}_{0.35}\text{Pu}_{0.65}\text{O}_2$  $\text{U}_{0.30}\text{Pu}_{0.70}\text{O}_2$ 

$y$	0.60	0.65	0.70
Density <sup>1</sup>	$97.0 \pm 0.1\% \text{ TD}$	$96.0 \pm 0.1\% \text{ TD}$	$95.8 \pm 0.1\% \text{ TD}$
Density (Image analysis)	$96.6 \pm 1.1\%$	$96.5 \pm 1.0\%$	$95.1 \pm 1.4\%$
Chemical analysis y (TIMS <sup>2</sup> )	$0.59 \pm 0.02$	$0.63 \pm 0.02$	$0.69 \pm 0.02$
Optical microscopy	OK	OK	OK

**Dense pellets with the microstructure and Pu content targeted**

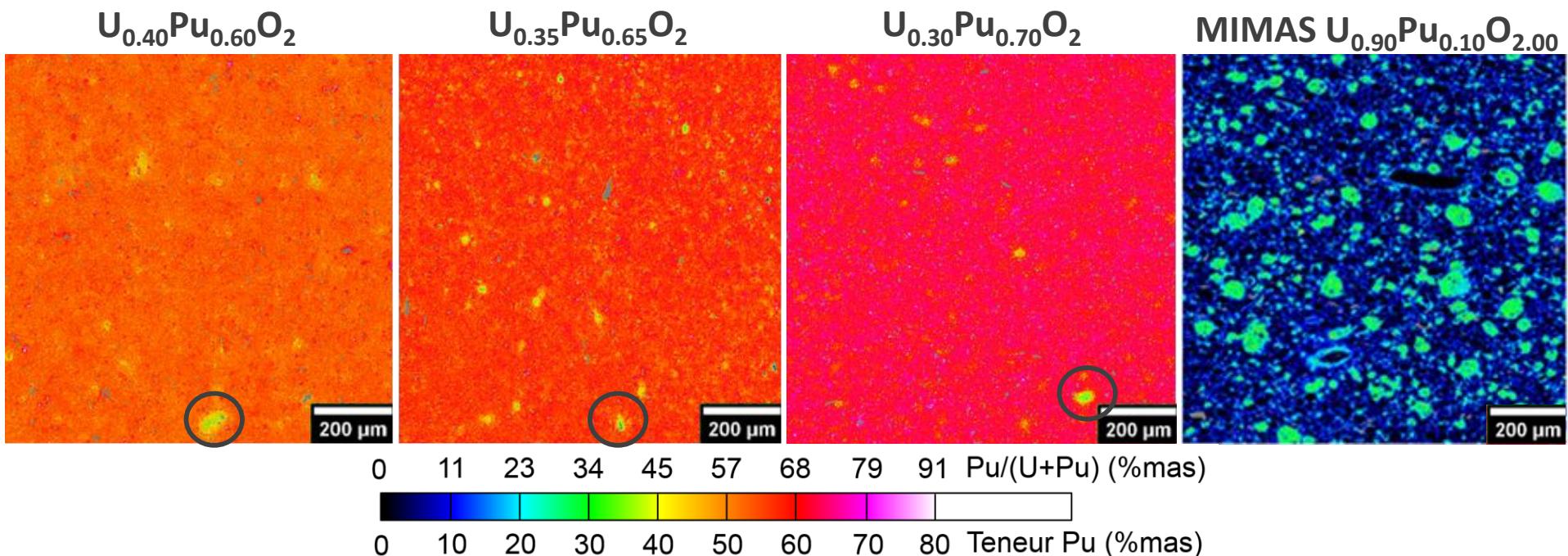
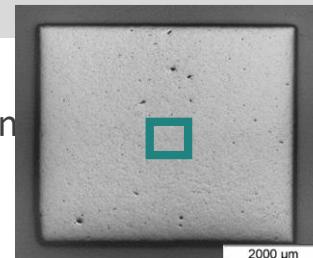
<sup>1</sup> Hydrostatic density by immersion

<sup>2</sup> Thermal Ionization Mass Spectroscopy

# Characterization (2/4) – EPMA (global composition)

**Setting:** Map of 1024x1024 pixels =  $1 \mu\text{m}^2$  / - 20kV electron accelerating voltage - 20 ms. pixel $^{-1}$

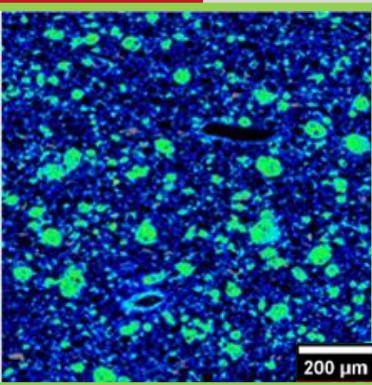
**MIMAS ( $\text{U}_{0.90}\text{Pu}_{0.10}\text{O}_{2.00}$ ) [8]:** Dosage, first blending, dosage, blending-dilution, pelletizing, sintering, grinding, inspection.



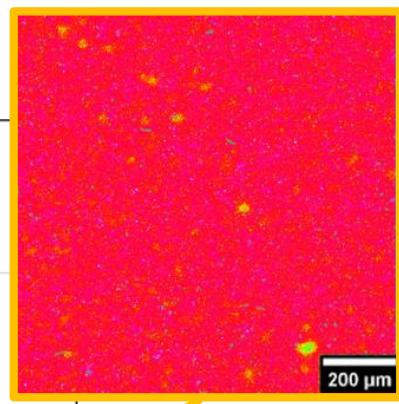
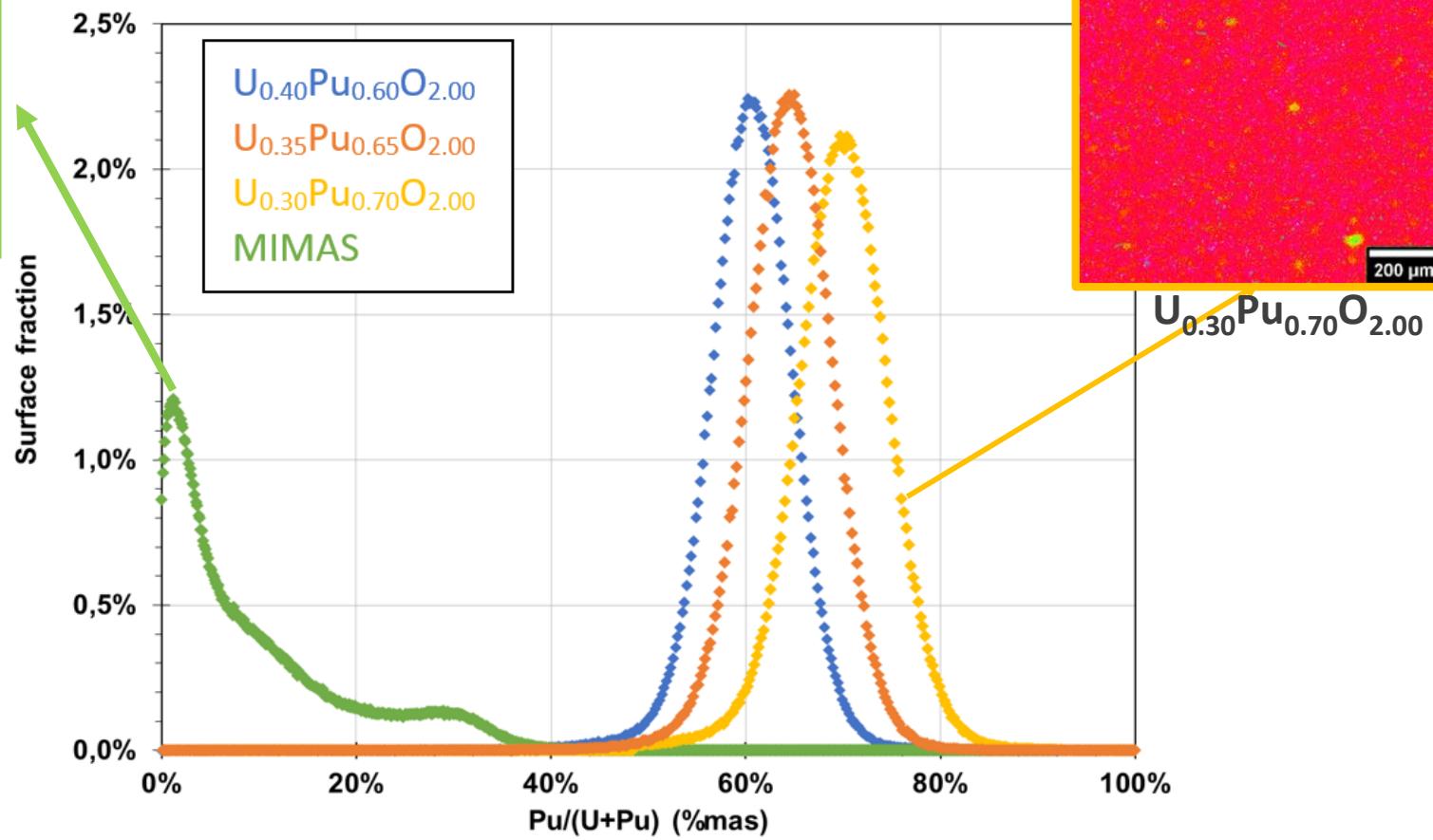
$y$	0.60	0.65	0.70
Electron Probe Micro-Analysis (EPMA)	$y = 0.595 \pm 0.048$ Homogeneous distribution of cations	$y = 0.629 \pm 0.039$ Homogeneous distribution of cations	$y = 0.704 \pm 0.056$ Homogeneous distribution of cations

[8] O. Kahraman *et al.*, *J. App. Phys.* 132 (2022) 115106.

# Characterization (2/4) – EPMA (global composition)



MIMAS [8]  
 $\text{U}_{0.90}\text{Pu}_{0.10}\text{O}_{2.00}$

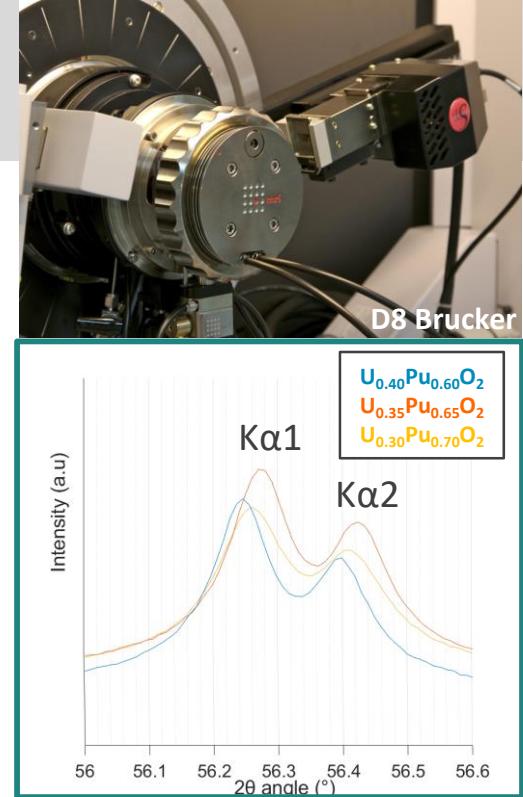
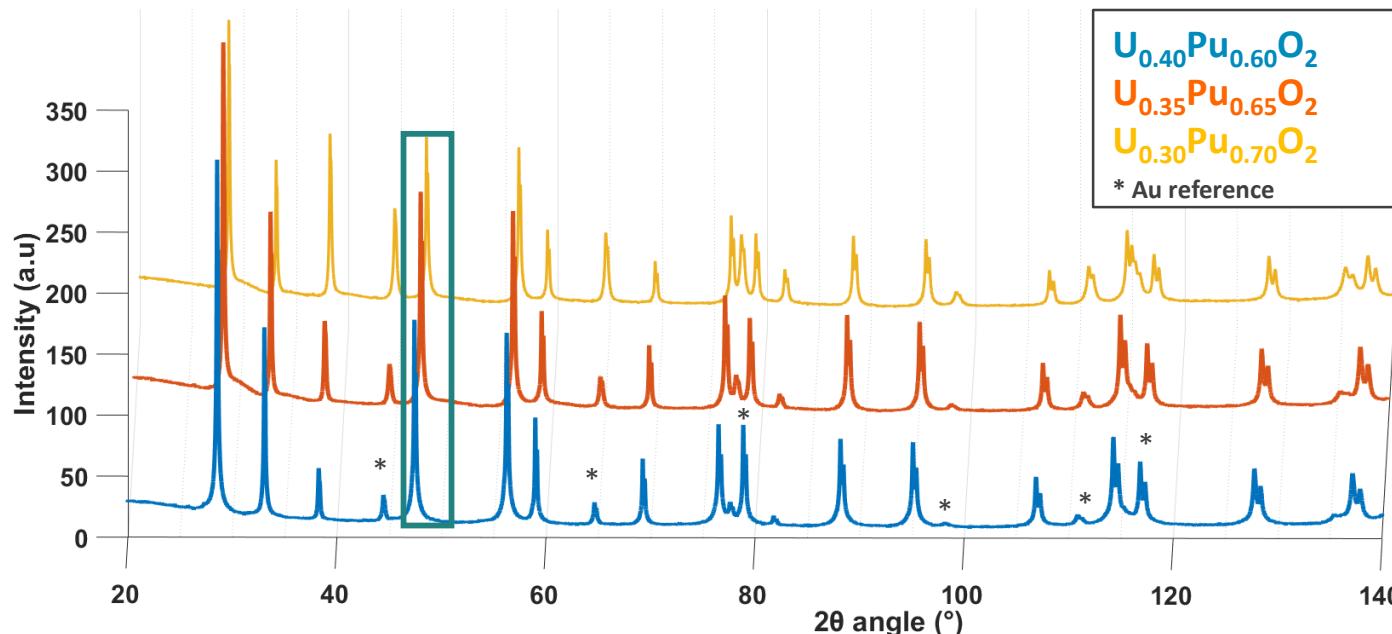


$\text{U}_{0.30}\text{Pu}_{0.70}\text{O}_{2.00}$

**Homogeneous cations distribution in the matrix with U-rich agglomerates surface fraction < 5 % and the Pu content targeted**

# Characterization (3/4) – X-Ray Diffraction

Setting: 0.1 g of powder - angle step 0.1 ° each 5s – 2θ angle 20-140°



Evolution of the (311) pic of the fcc structure function of the Pu content.

Determination of the lattice parameter  
=> Estimation of the matrix O/M ratio

Duriez *et al.* law [4]  
 $a(\text{U}_{1-y}\text{Pu}_y\text{O}_{2-x}) \text{ Å} = 5.470 - 0.074y + 0.34x$

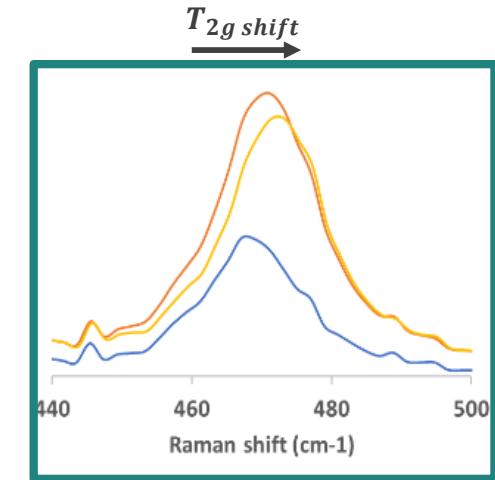
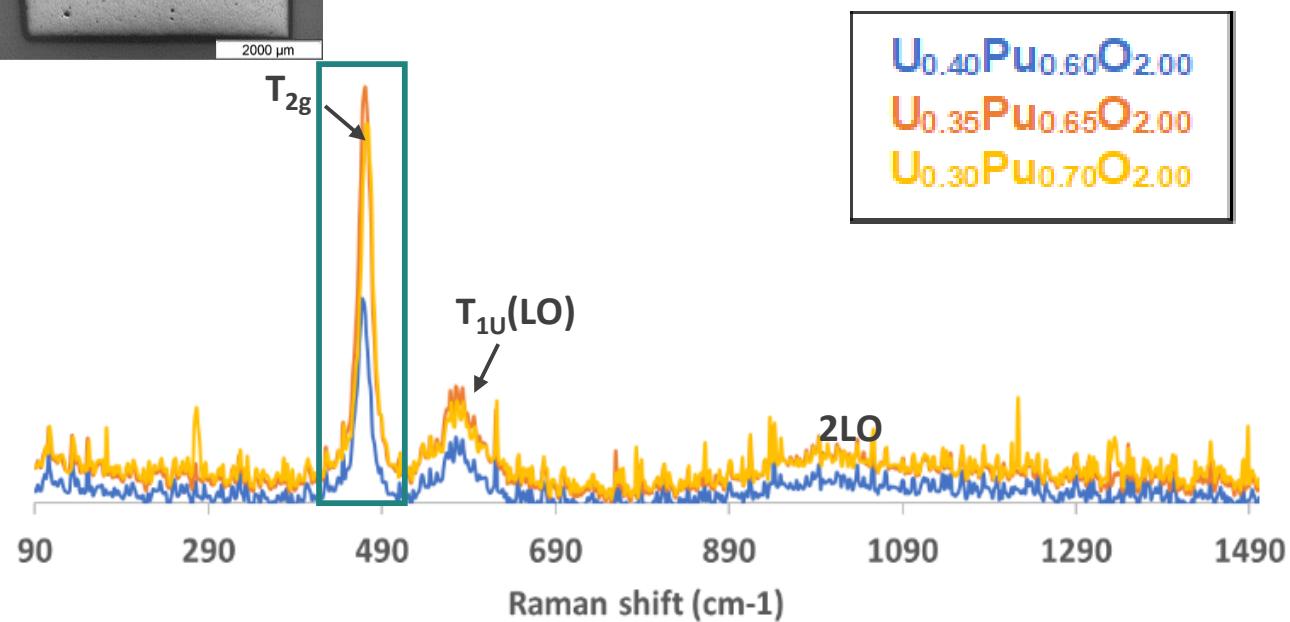
y	0.595	0.629	0.700
X-Ray diffraction	$a = 5.426 \pm 0.001 \text{ Å}$ $\text{O/M} = 2.000 \pm 0.004$	$a = 5.424 \pm 0.001 \text{ Å}$ $\text{O/M} = 1.998 \pm 0.004$	$a = 5.420 \pm 0.001 \text{ Å}$ $\text{O/M} = 1.998 \pm 0.004$

Monophasic and stoichiometric mixed oxides

# Characterization (4/4) – Raman $\mu$ -Spectroscopy (Local homogeneity)



Line (3000  $\mu\text{m}$ ): 2x30 s/point each 1.5  $\mu\text{m}$   
Average of 2000 spectrums



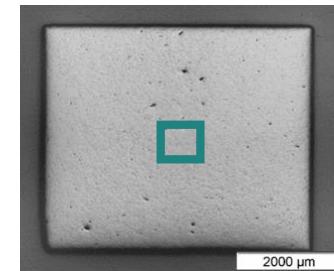
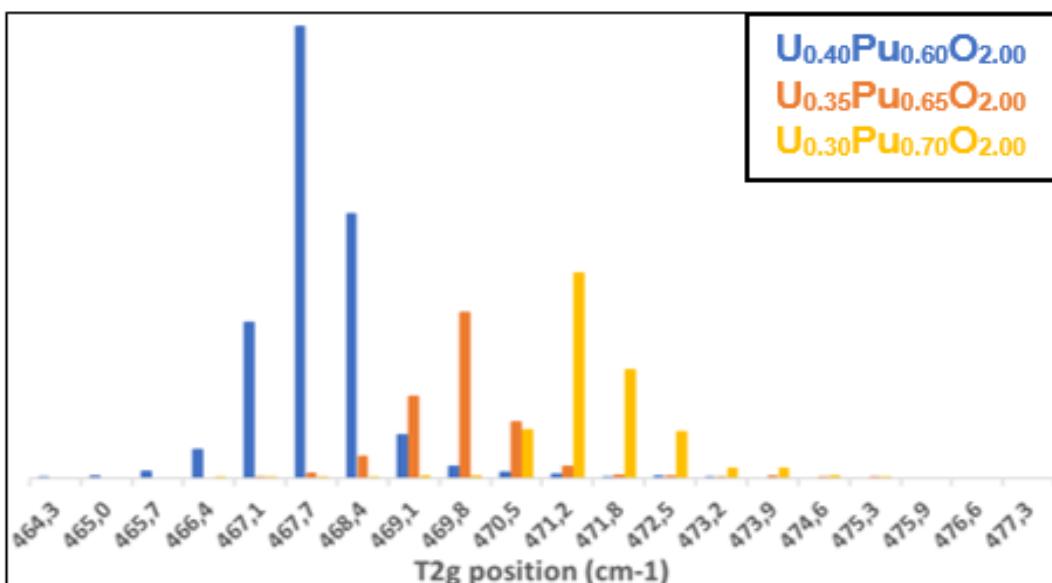
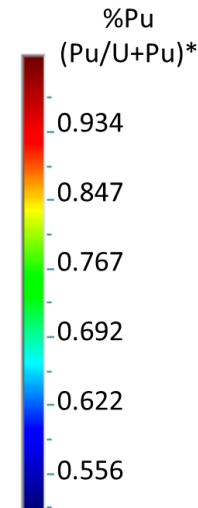
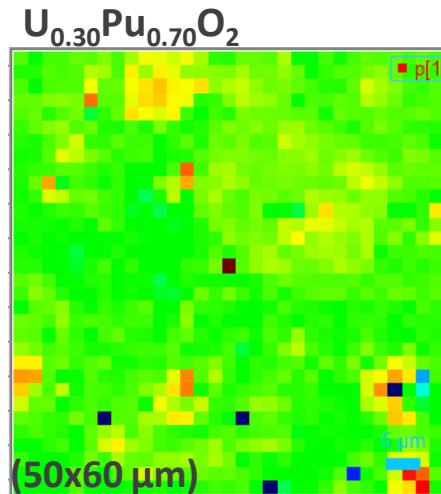
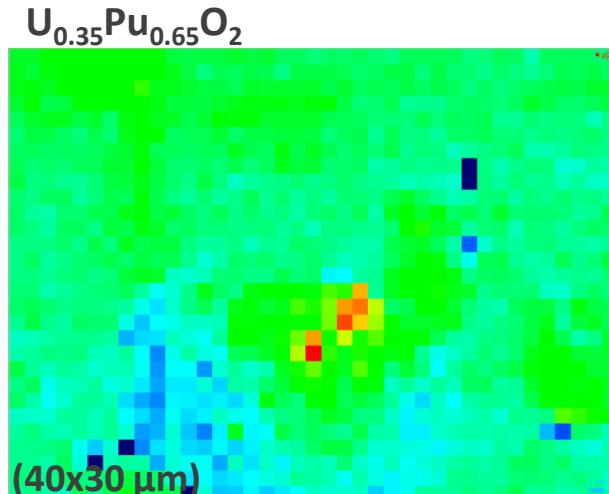
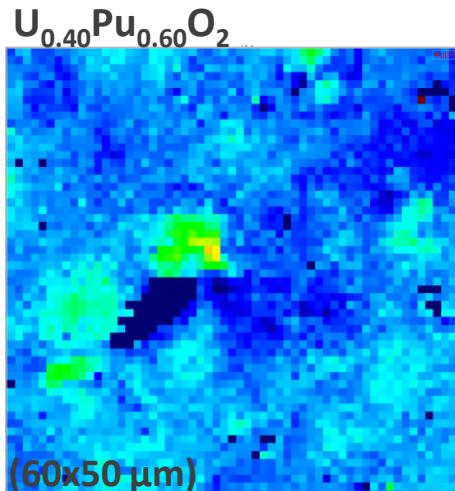
$\gamma$	0.60	0.65	0.70
Raman $\mu$ -spectroscopy	$T_{2g} = 467.5 \text{ cm}^{-1}$ $\rightarrow \gamma = 0.605 \pm 0.003^*$	$T_{2g} = 469.4 \text{ cm}^{-1}$ $\rightarrow \gamma = 0.670 \pm 0.003^*$	$T_{2g} = 471 \text{ cm}^{-1}$ $\rightarrow \gamma = 0.729 \pm 0.003^*$
O/M (XRD)	$2.000 \pm 0.004$	$1.998 \pm 0.004$	$1.998 \pm 0.004$

\* %Pu: Pu/(U+Pu) ratio calculated for O/M = 2.00

[10] L. Medyk et al., J. Nuc. Mat. ,541 (2020) 152439.

# Characterization (4/4) – Raman $\mu$ -Spectroscopy (Local homogeneity)

Maps: 2x30 s/point each 1.5  $\mu\text{m}$



Monophasic solid solution with a local homogeneous cations distribution with surface fraction agglomerates < 5% and the Pu content targeted

\*%Pu: Pu/(U+Pu) content calculated for O/M = 2.00

[10] L. Medyk et al., J. Nuc. Mat., 541 (2020) 152439.



## Conclusions:

### Optimization of the manufacturing process

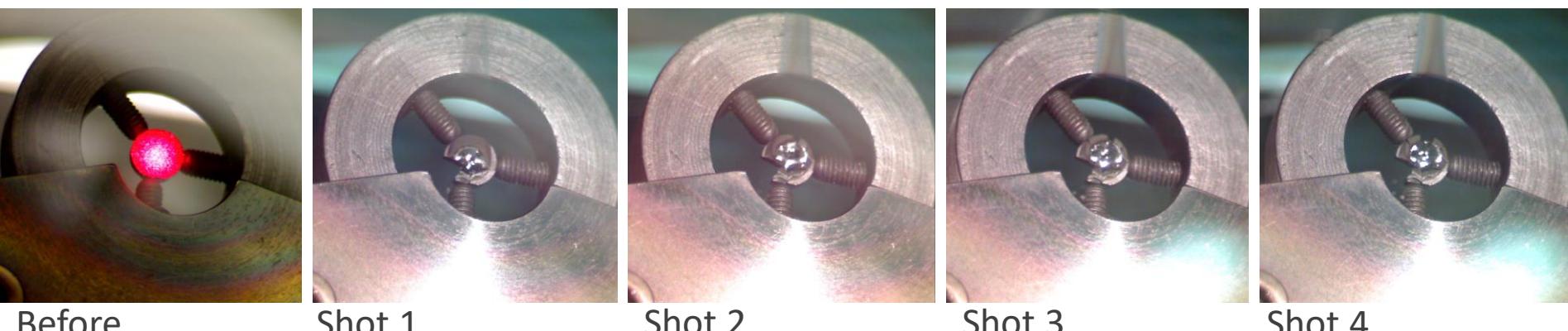
- High density (> 94% TD)
- Microstructure with the required properties
- Homogeneous cationic distribution
- Monophasic and stoichiometric mixed oxides

	$U_{0.40}Pu_{0.60}O_2$	$U_{0.35}Pu_{0.65}O_2$	$U_{0.30}Pu_{0.70}O_2$
Chemical analysis	$0.591 \pm 0.019$	$0.631 \pm 0.020$	$0.689 \pm 0.021$
EPMA	$0.595 \pm 0.048$	$0.629 \pm 0.039$	$0.704 \pm 0.056$
Raman $\mu$ -spectroscopy	$0.605 \pm 0.003$	$0.670 \pm 0.003$	$0.729 \pm 0.003$
O/M (XRD)	$2.000 \pm 0.004$	$1.998 \pm 0.004$	$1.998 \pm 0.004$



## Next steps:

- Thermodynamic properties measurements at JRC-Karlsruhe (melting temperature, enthalpy, heat capacity, conductivity, ...) and at Marcoule (thermal expansion and oxygen potential).



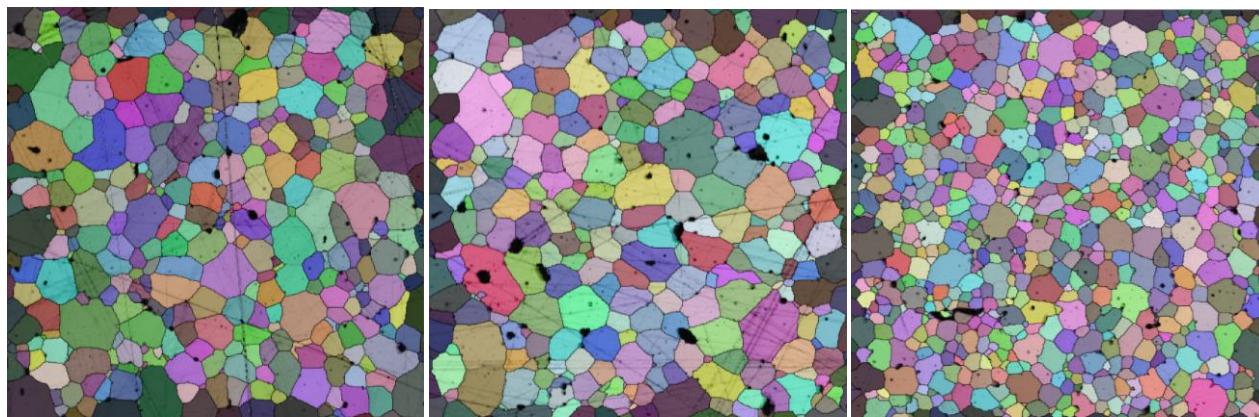


# Thank you for your attention

## Acknowledgments

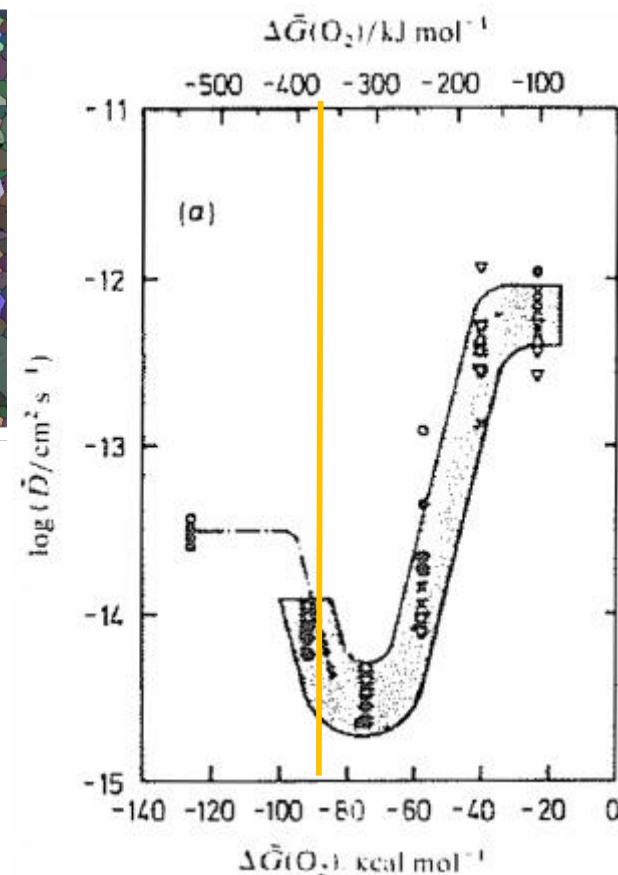
F. Lebreton<sup>1</sup>, M. Alibert<sup>1</sup>, C-M. Aloin<sup>1</sup>, M. Pons<sup>1</sup>, L. Barnouin<sup>1</sup>, G. Gabriel<sup>1</sup>, P. Signoret<sup>1</sup>, J. Lorino<sup>1</sup>, L. Picard<sup>1</sup>, O. Miollan<sup>1</sup>, O. Kahraman<sup>1</sup>.

<sup>1</sup> CEA, DES, ISEC, DMRC, Université Montpellier, Marcoule, France

 $U_{0.40}Pu_{0.60}O_2$  $U_{0.35}Pu_{0.65}O_2$  $U_{0.30}Pu_{0.70}O_2$ 

	$U_{0.40}Pu_{0.60}O_2$	$U_{0.35}Pu_{0.65}O_2$	$U_{0.30}Pu_{0.70}O_2$
SEM/EBSD	$12.3 \pm 1 \mu\text{m}$	$15.8 \pm 1 \mu\text{m}$	$12.1 \pm 1 \mu\text{m}$

Homogenous distribution of the grain size along the pellet.



U-Pu interdiffusion coefficient according to the oxygen potential at 1873 K; circle:  $0.175 \leq y \leq 0.177$ , black circle:  $0.150 \leq y \leq 0.174$ , cross:  $0.110 \leq y \leq 0.140$ , triangle down:  $0.06 \leq y \leq 0.09$  and triangle up:  $0.003 \leq y \leq 0.05$  [6]

[6] S. Mendez, 1995, Etude de l'interdiffusion U-Pu appliquée au combustible MOX, thèse, université d'Aix Marseille III