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CFD SIMULATIONS OF BOILING FLOWS IN NUCLEAR REACTOR CONDITIONS



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Context and Objective

Prediction of flow boiling in nuclear reactor condition using multiphase CFD is very sensitive to the modeling of Interfacial heat transfer, forces, and area [1]. These parameters are interdependent.

Standard approach [2, 3]:

- 1. Build an Interfacial Area Equation or population balance model to determine **bubble diameter**
- 2. Validate model on **adiabatic flows** using force closure terms

3. Add condensation and boiling terms to simulate complete system

Debora: a reactor-similarity experiment

The Debora loop is a vertical heated Freon-12 pipe that fills **similarity criteria with nuclear reactor conditions** [15]. Density ratio, Weber number and Boiling number are respected.



Liquid temperatures, void fractions, gas velocities and Sauter mean diameters are measured at different altitudes and radial positions.

Run number	1	2	3
Pressure	Boiling Water	Pressurized	Pressurized

Our approach:

- 1. Select heat transfer and force terms
- 2. Enforce 3D **experimental diameter** measurements in the flow
- 3. Validate models on **reactor similarity** experiment
- 4. Future work: model bubble diameter in reactor conditions

Numerical Toolkit

 $k - \omega$ turbulence model [6]

TrioCFD open-source CFD code developed at CEA [4]. **Euler-Euler** approach [5]:

```
\frac{\partial(\alpha_k \rho_k)}{\partial t} + \nabla \cdot (\alpha_k \rho_k \vec{u_k}) = \Gamma_k
```

 $\frac{\partial(\alpha_k\rho_k\vec{u_k})}{\partial t} + \nabla \cdot (\alpha_k\rho_k\vec{u_k}\otimes\vec{u_k}) = -\alpha_k\nabla P + \nabla \cdot [\alpha_k\mu_k\nabla\vec{u_k} - \alpha_k\rho_k\overline{u_i'u_j'}] + \vec{F}_{ki} + \alpha_k\rho_k\vec{g}$

```
\frac{\partial(\alpha_k\rho_k e_k)}{\partial t} + \nabla \cdot (\alpha_k\rho_k e_k \vec{u_k}) = -P\left(\partial_t \alpha_k + \nabla \cdot (\alpha_k \vec{u_k})\right) + \nabla \cdot [\alpha_k \lambda_k \nabla T_k - \alpha_k \rho_k \overline{u'_i e'_k}] + q_{ki} + q_{kw}
```

similarity	Reactor	Water Reactor	Water Reactor
Liquid	Maintenance	Maintenance	Normal operation
velocity	$\sim 2 { m m/s}$	$\sim 1 \mathrm{m/s}$	$\sim 3 { m m/s}$

Boiling flow simulations



Tomiyama drag force [7], Burns turbulent dispersion [8], Sugrue lift force [9], Lubchenko wall lubrication [10]. Zeitoun condensation [11], Kurul-Podowski boiling [12].

Air-water adiabatic validation

Upwards, downwards and micro-gravity flow experiments in pipes at atmospheric pressure [13, 14]. Steady-state radially-dependent experimental diameter is enforced in the simulations.



Conclusions and perspectives

• Interfacial forces for isolated bubbles must be modified to simulate high void fraction, high pressure reactor flows

• Next step: build a **unique set of closures for all runs**

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