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Pellet core fueling in tokamaks, stellerators and reversed field pinches

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DE LA RECHERCHE À L'INDUSTRIE



Pellet core fueling in tokamaks, stellerators and reversed field pinches

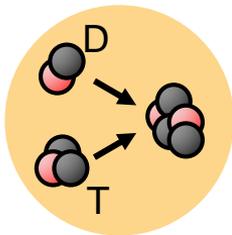
Eleonore Geulin, Bernard Pégourié



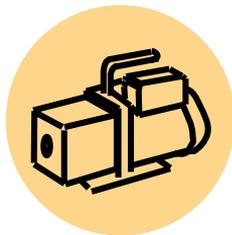
www.cea.fr

10/11/2022 - AAPPS conference

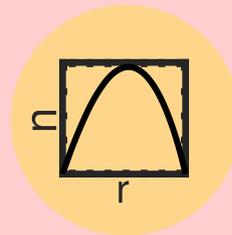
We need to fuel to compensate :



Fusion reactions



Ash pumping



Keep core
density
→ balancing
outgoing flows

Gaz puff injection



easy to use



Fuel only the edge of the plasma

→ Screening of neutrals in the SOL

Neutral beam injection



Deep penetration



- Power & Matter injection

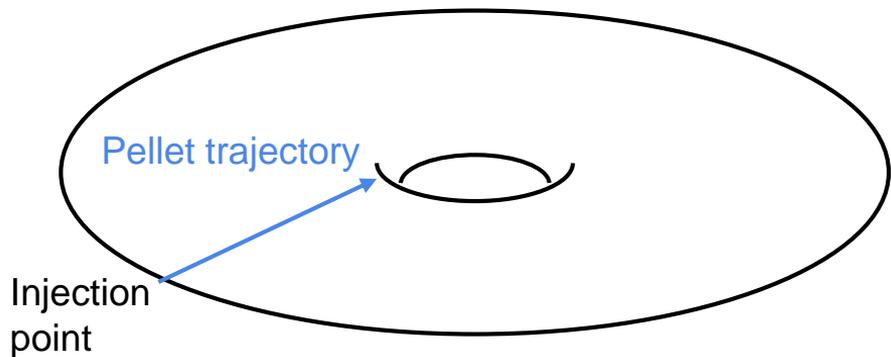
- Not enough fuelling for required power

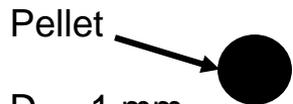
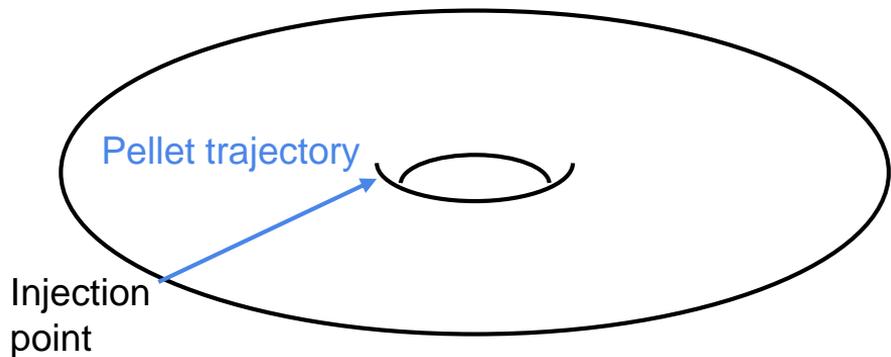
Pellet injection



Deep penetration

Efficient fuelling with no momentum or power injection

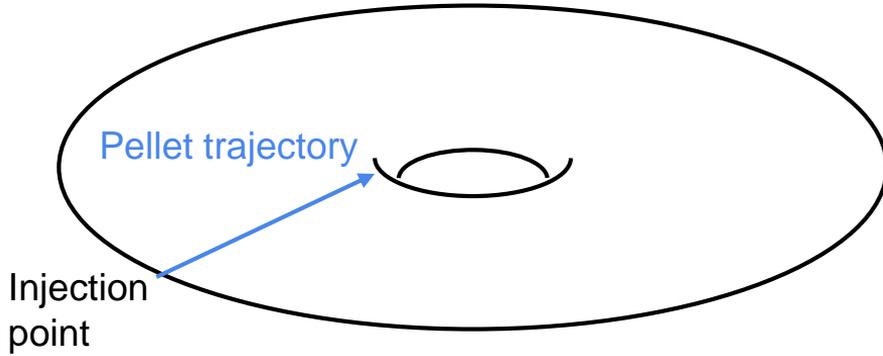




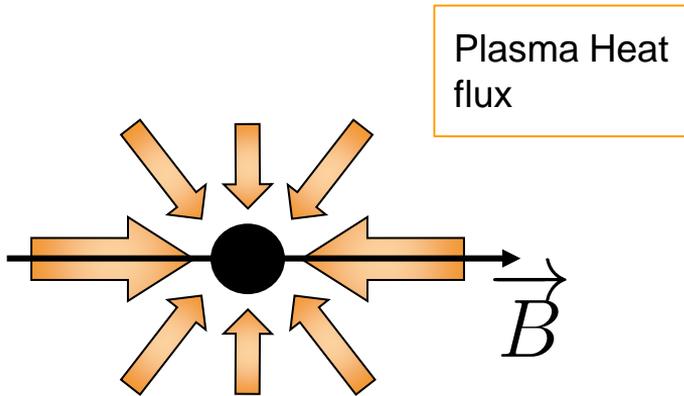
$D \sim 1 \text{ mm}$

$T^\circ \sim 15\text{K}$

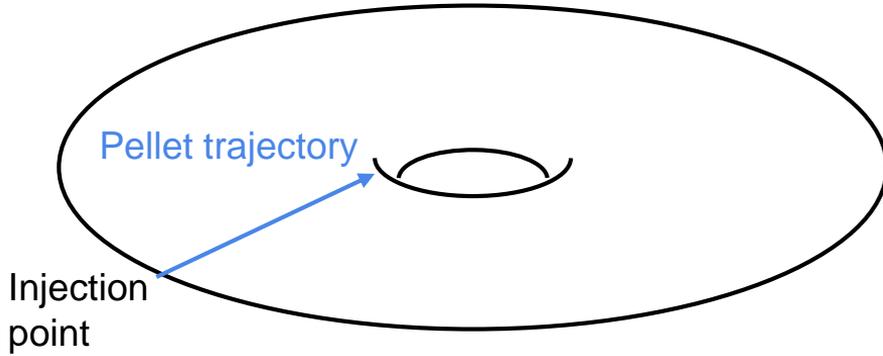
$V \sim 200 \text{ m/s to a few km/s}$



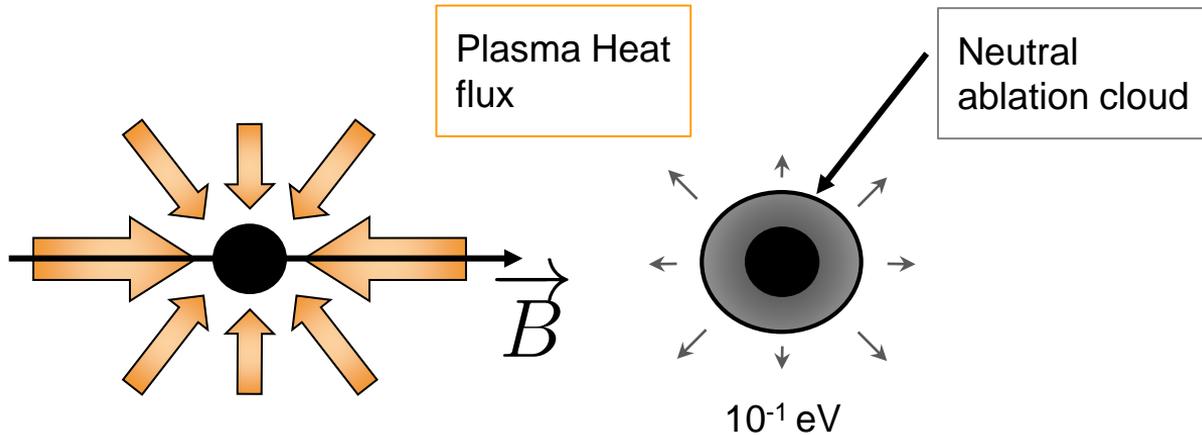
- By heating the pellet,

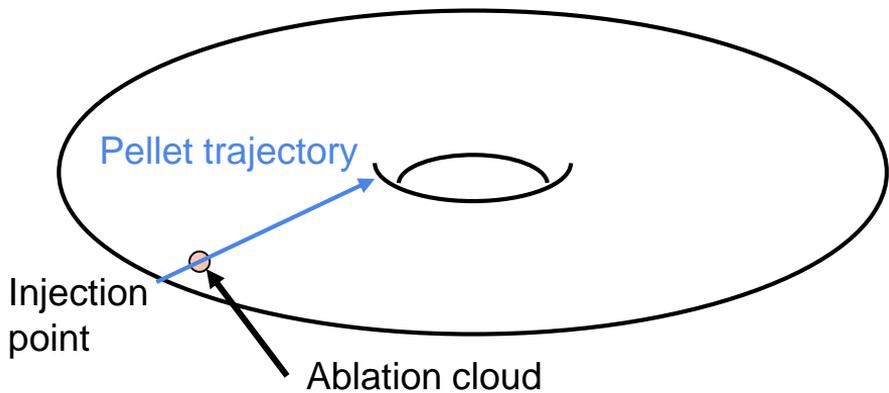


ablation : Loss of a material caused by vaporization

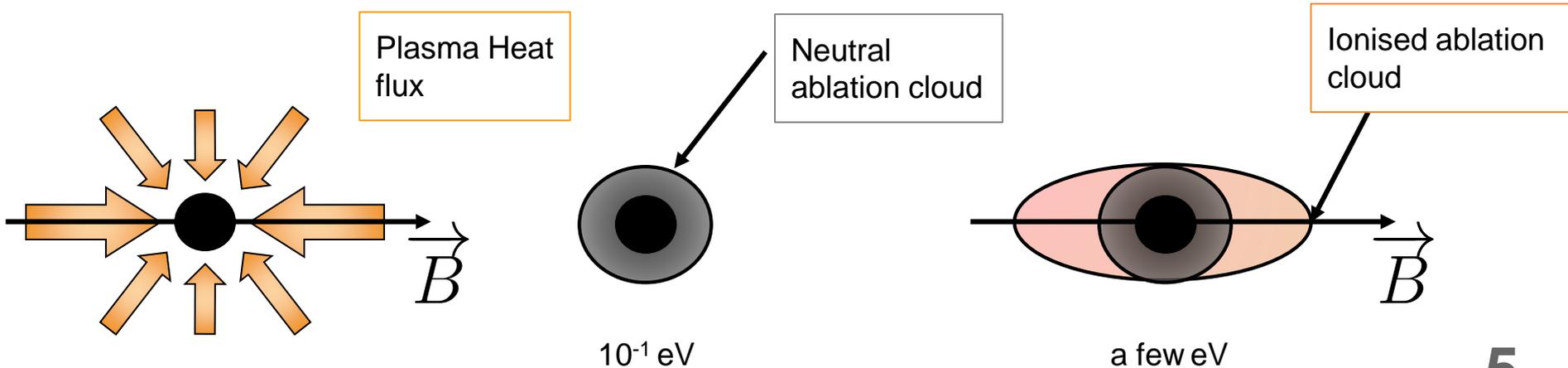
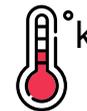


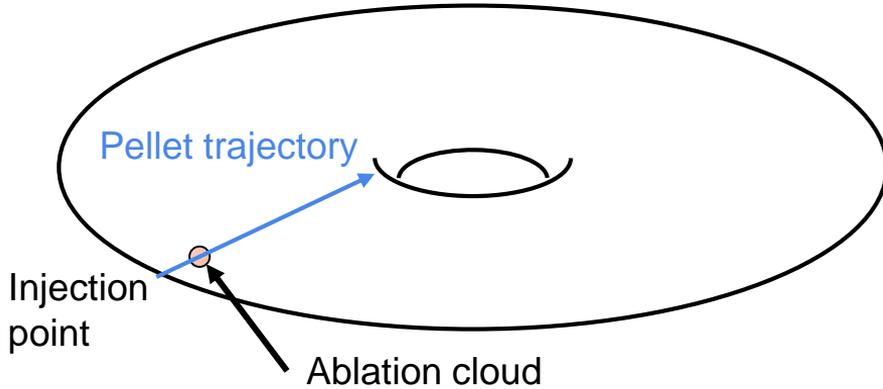
- By heating the pellet,
⇒ Neutral ablation cloud



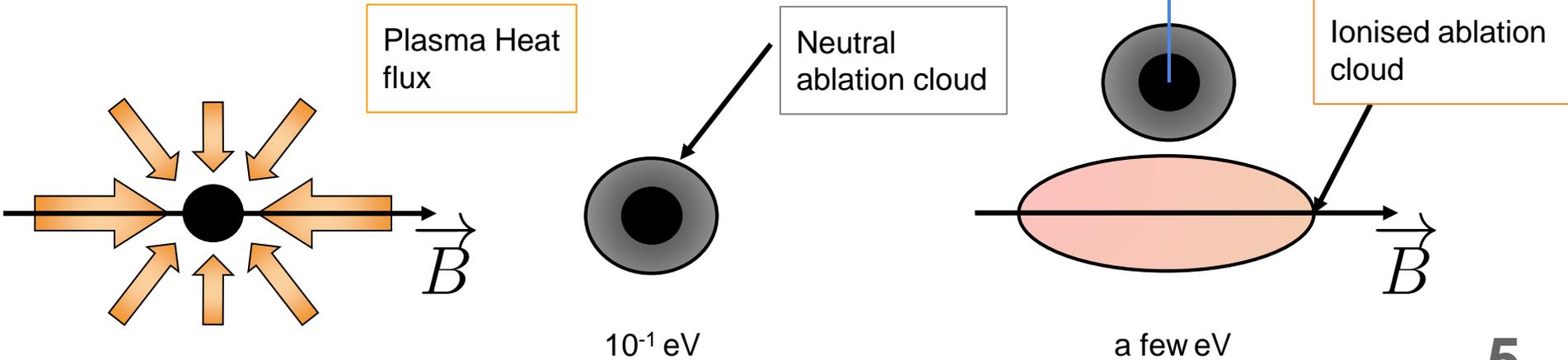
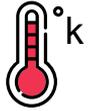


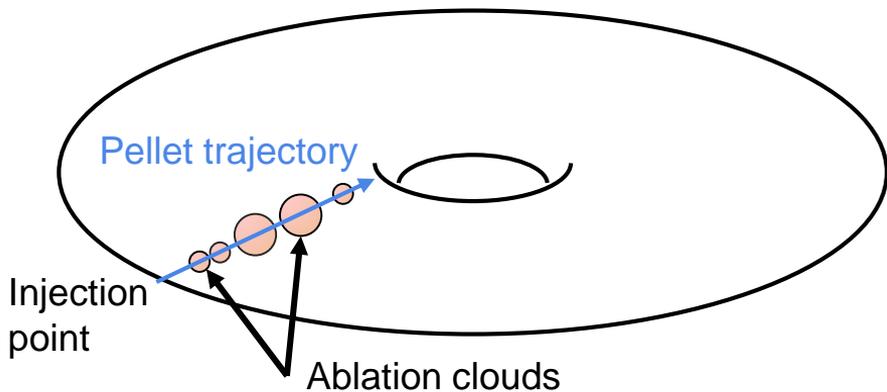
- By heating the pellet,
 ⇒ Neutral ablation cloud
 ⇒ Ionized ablation cloud



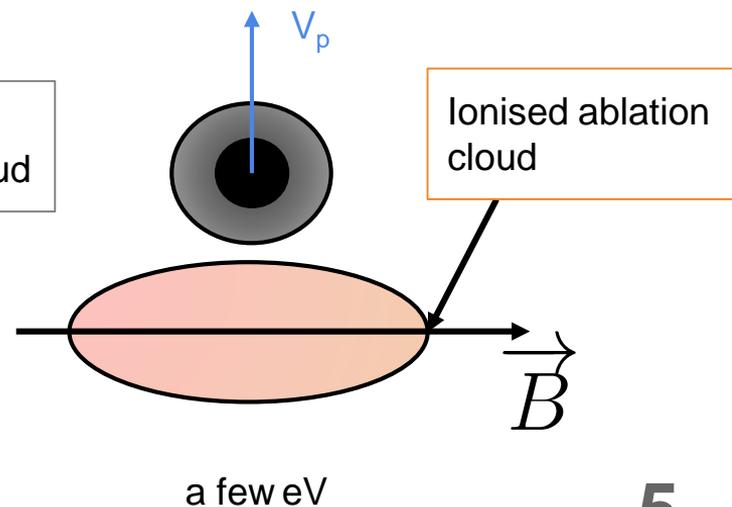
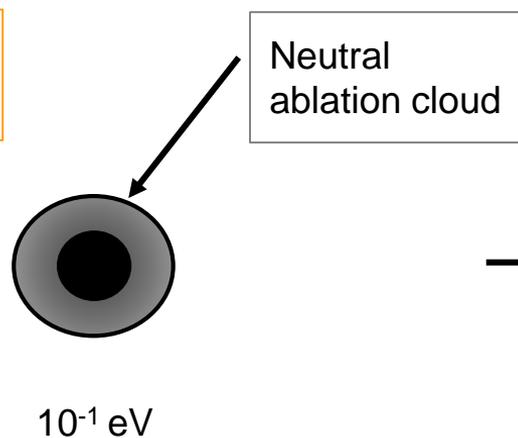
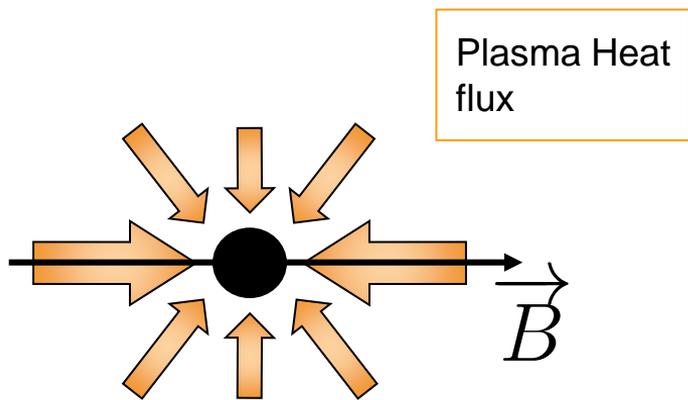
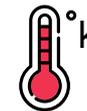


- By heating the pellet,
 ⇒ Neutral ablation cloud
 ⇒ Ionised ablation cloud
- Ionised ablation cloud separate from neutral part (cloud + pellet),





- By heating the pellet,
 ⇒ Neutral ablation cloud
 ⇒ Ionised ablation cloud
- Ionised ablation cloud separate from neutral part (cloud + pellet),
 ⇒ Happens all along the pellet path



Pellet penetration length :

$$L_p \propto V_{\text{pellet}} N_{\text{pellet}}^{1/2} n_{\text{plasma}}^{-1/3} T_{\text{plasma}}^{-5/3}$$

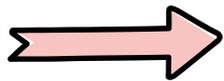
Plasma density / temperature

Pellet velocity / particle contents

2 conclusions :

⇒ Temperature dependance is the more limiting for penetration

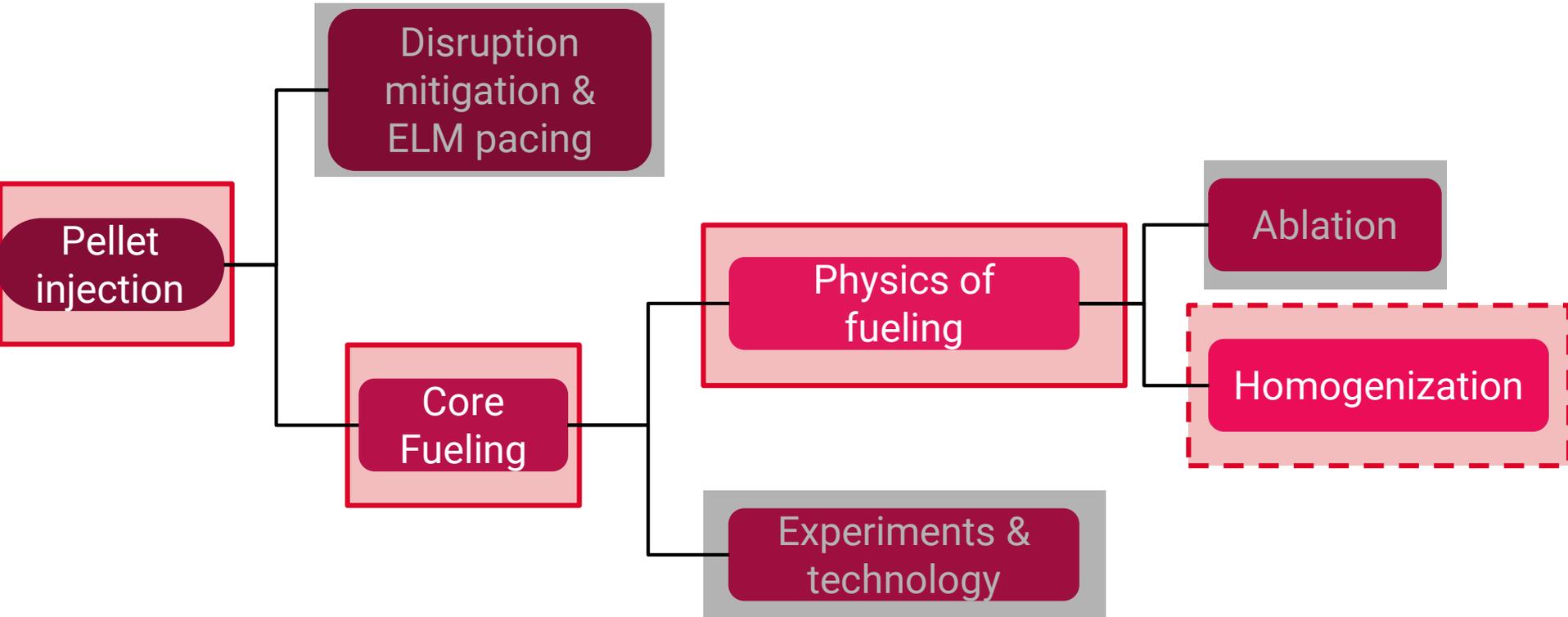
⇒ Increase V_p more efficient than N_p to increase L_p

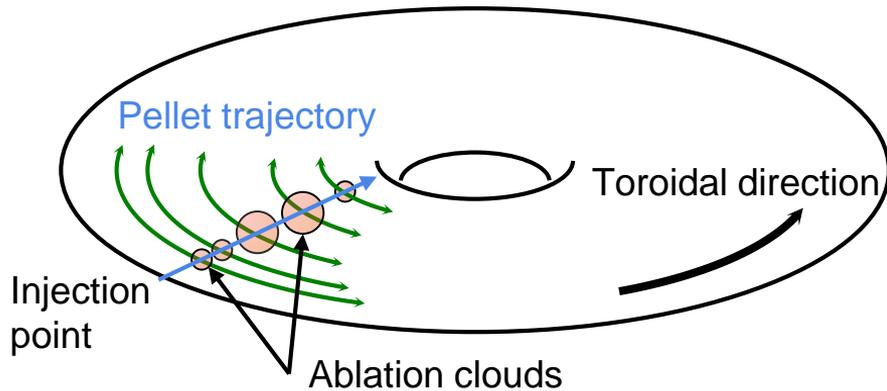


Pellet L_p : from 20% to >50% plasma radius in present day tokamaks

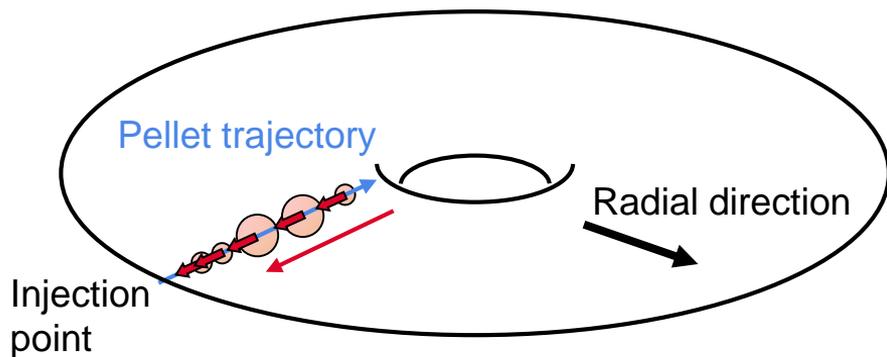
Fast ions (ICRH,NBI) moderate ablation increase

Fast electrons (ECRH) significant ablation increase; (LHCD) pellet mass sublimation



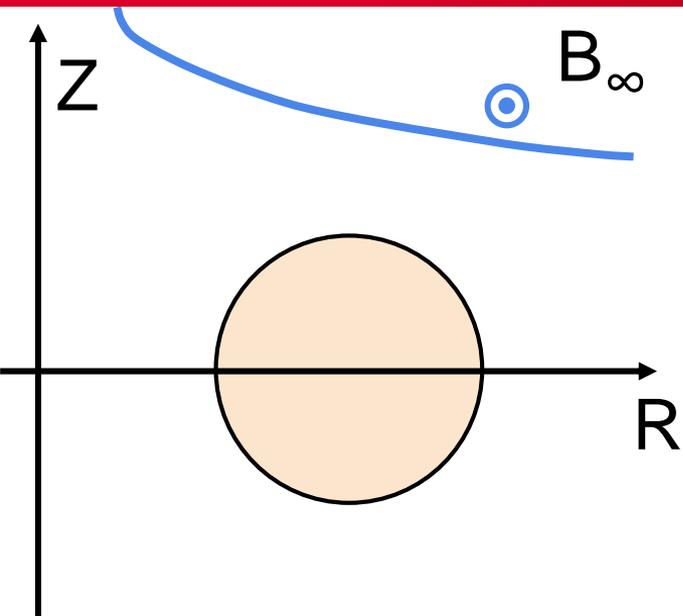


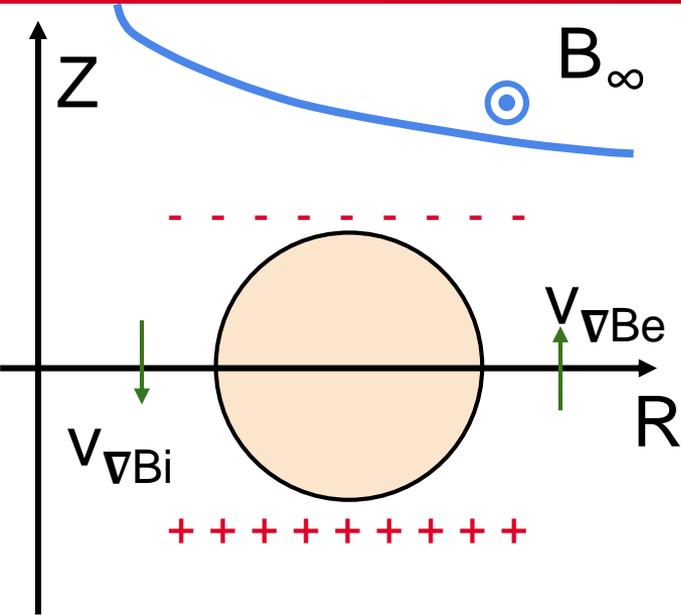
✦ Homogenization : deposited matter leads to a new axisymmetric density and temperature profiles



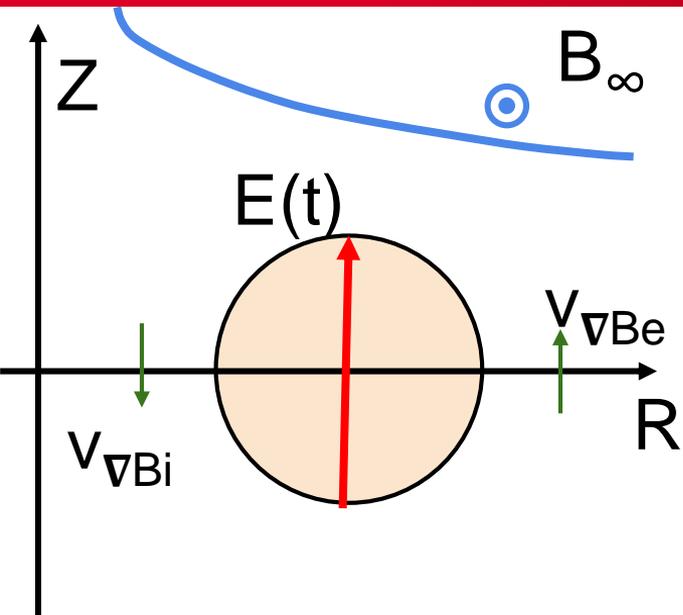
✦ Deposited matter displacement :

- ⇒ Parallel expansion
- ⇒ **Radial drift** (down ∇B direction)

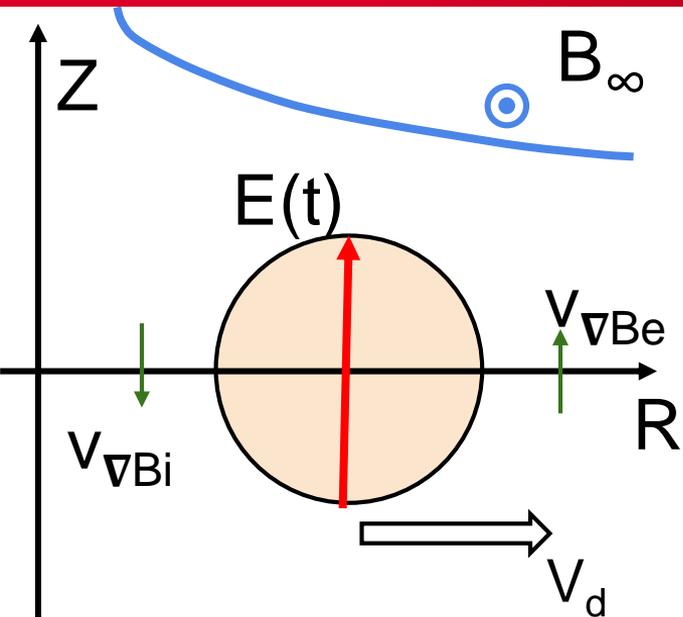




$V_{\nabla B_{e,i}}$: Vertical e^- , i^+ drift

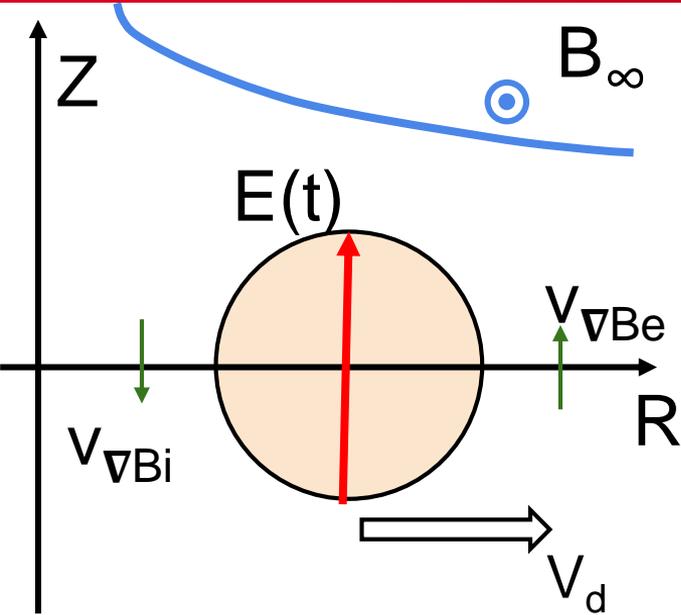


$V_{\nabla B_{e,i}}$: Vertical e^- , i^+ drift



$\mathbf{v}_{\nabla B_{e,i}}$: Vertical e^- , i^+ drift

$$V_d = \frac{\mathbf{E} \times \mathbf{B}_\infty}{B_\infty^2}$$



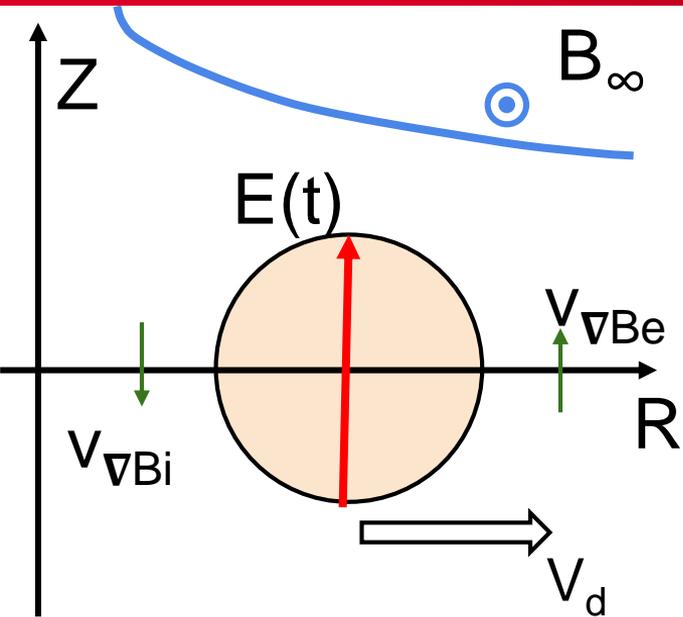
$\mathbf{V}_{\nabla B_{e,i}}$: Vertical e^- , i^+ drift

$$V_d = \frac{\mathbf{E} \times \mathbf{B}_\infty}{B_\infty^2}$$

We can calculate the drift acceleration :

$$\frac{dV_d}{dt} = \frac{2(p_0 - p_\infty)}{n_0 m_0 R_c}$$

- p_0 : Ionised cloud pressure
- p_∞ : Background plasma pressure
- n_0 : Ionised cloud density
- m_0 : Ionised cloud mass
- R_c : Curvature radius

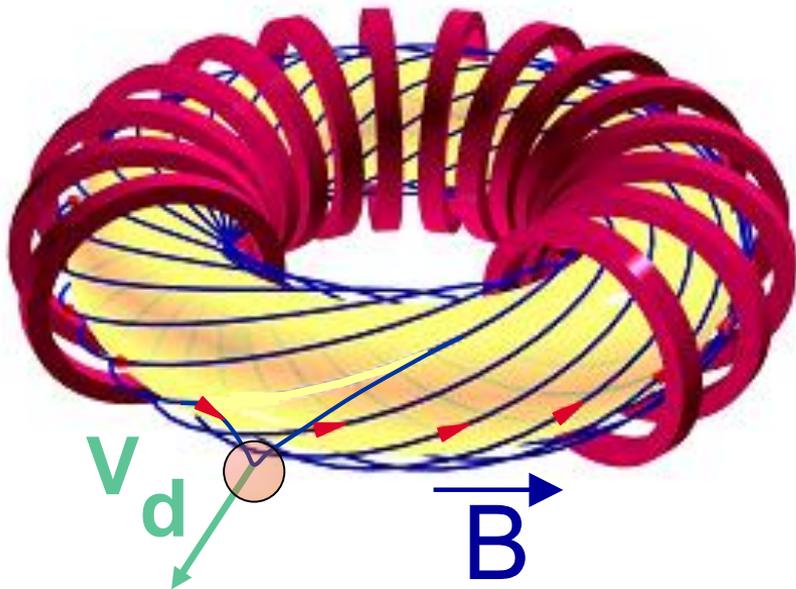


$\mathbf{V}_{\nabla B_{e,i}}$: Vertical e^- , i^+ drift

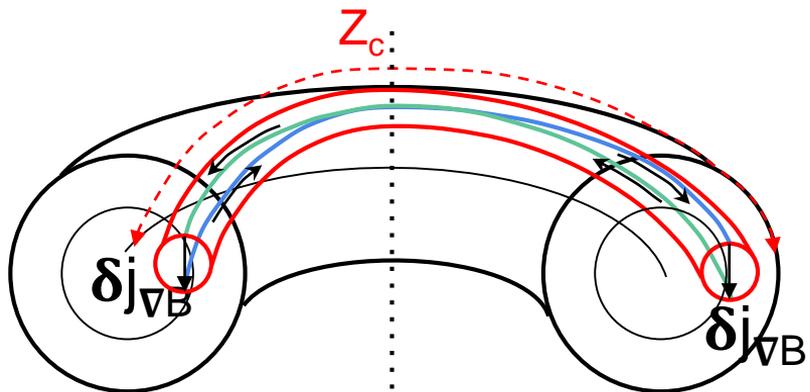
$$V_d = \frac{\mathbf{E} \times \mathbf{B}_\infty}{B_\infty^2}$$

We can calculate the drift acceleration :

$$\frac{dV_d}{dt} = A_{\nabla B}$$

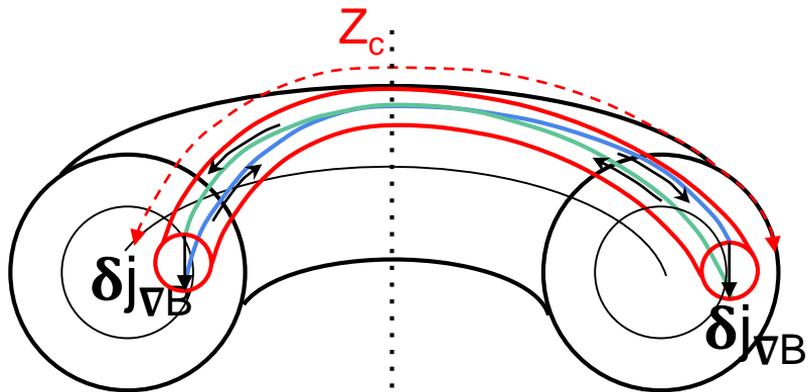


- ✦ Ideal MHD :
Cloud drags magnetic flux tube
- ✦ Rotational transform, winding of the field line
⇒ Drift damping by 2 phenomena



- ✦ Critical length Z_c reach
→ drift current circuit is closed inside the cloud

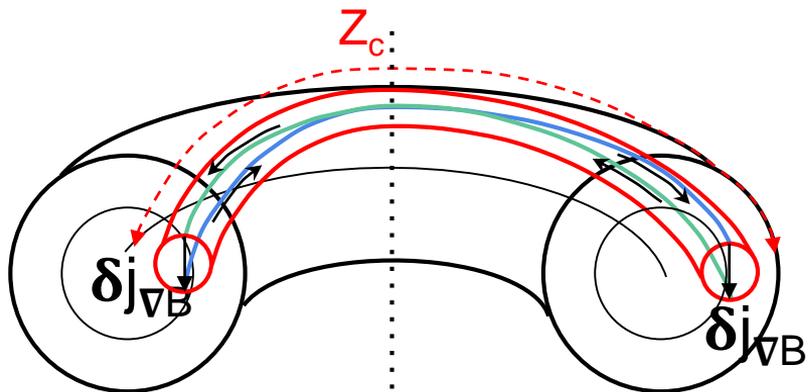
[Rozhansky 2005]



[Rozhansky 2005]

$$\frac{d\mathbf{V}_d}{dt} = A_{\nabla B} D_{IC}$$

 1st damping term
 → Internal **C**onnection



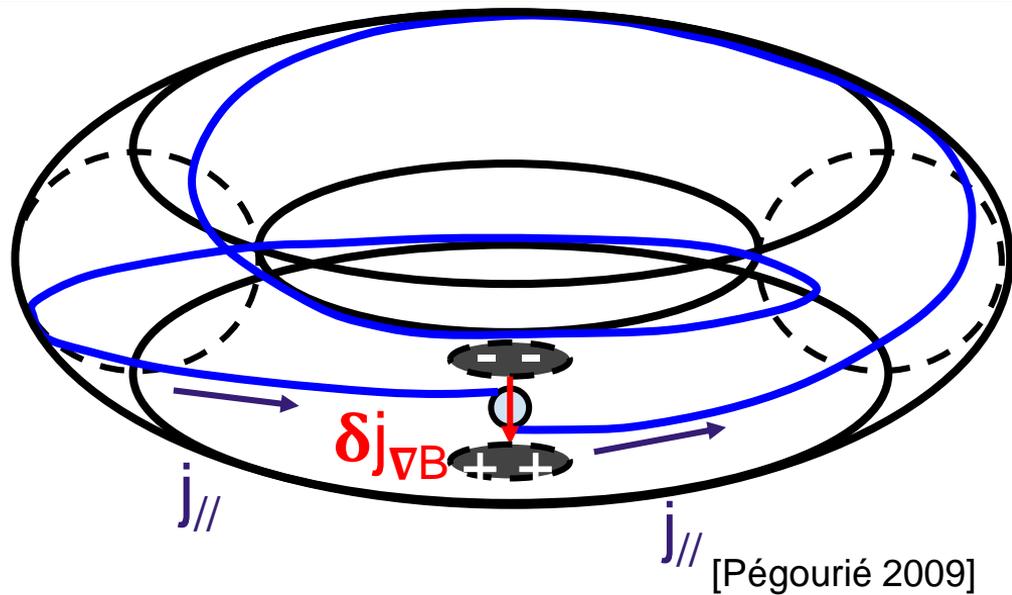
[Rozhansky 2005]

$$\frac{d\mathbf{V}_d}{dt} = A_{\nabla B} \mathbf{D}_{IC} \propto \mathcal{H}(Z_c - Z_0)$$

● 1st damping term
→ Internal **C**onnection

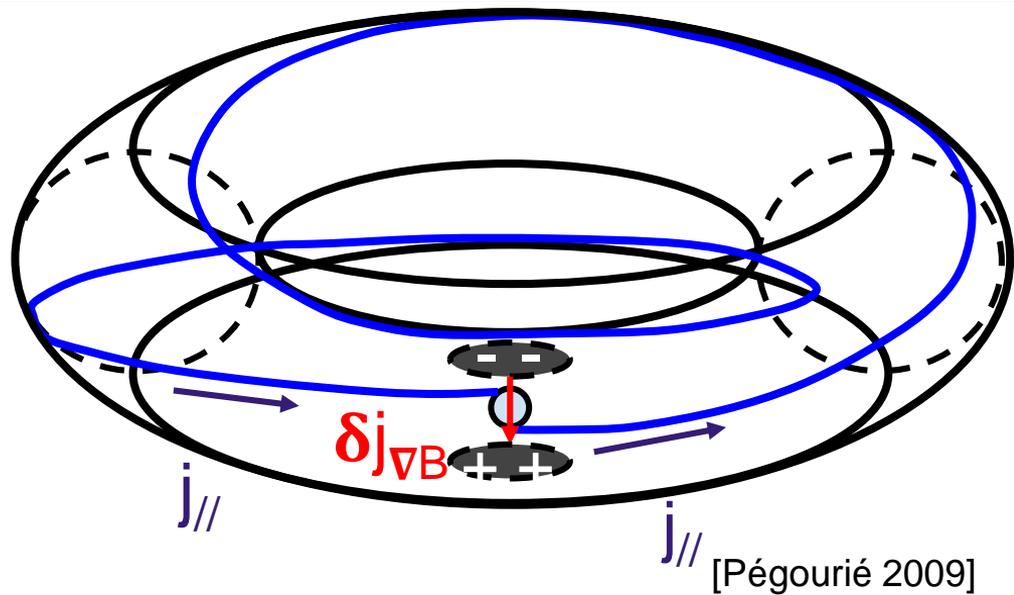
Z_c : Critical length where the relative current are inverted
 Z_0 : Cloud length

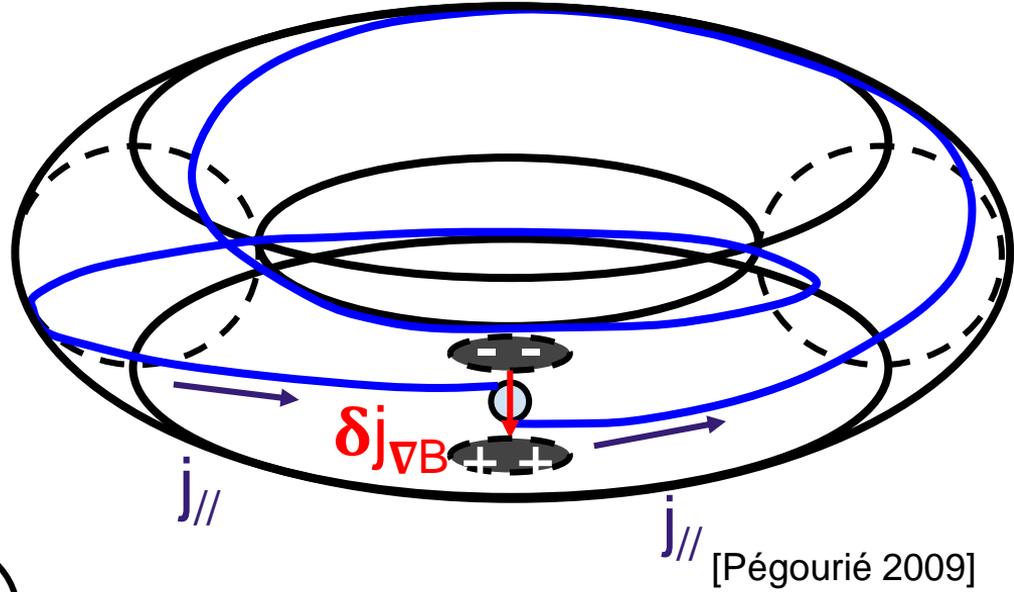
Parallel currents flow along field lines
→ closing drift current



$$\frac{d\mathbf{V}_d}{dt} = A_{\nabla B} D_{IC} - D_{EC}$$

- 2nd damping term
- **External Connection**





σ_{∞} : Parallel conductivity
 Z_{∞} : Length of the connecting flux tube

$$\frac{d\mathbf{V}_d}{dt} = A_{\nabla B} D_{IC} - \textcircled{D_{EC}} \propto V_d \frac{\sigma_{\infty} B_{\infty}^2}{Z_{\infty}}$$

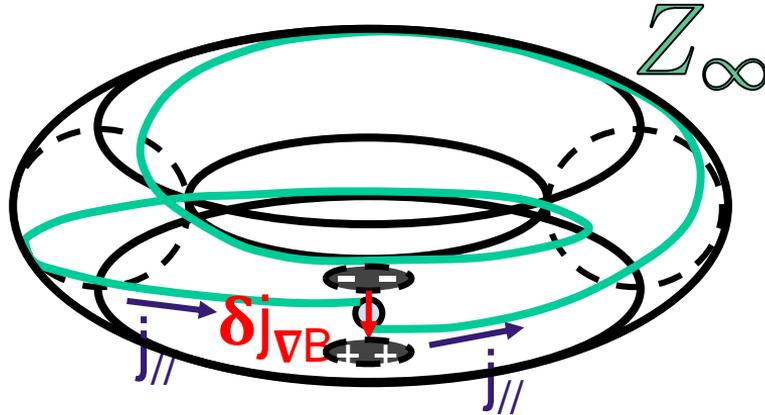
 2nd damping term
 → **External Connection**

$$\frac{d\mathbf{V}_d}{dt} = A_{\nabla B} D_{IC} - D_{EC}$$

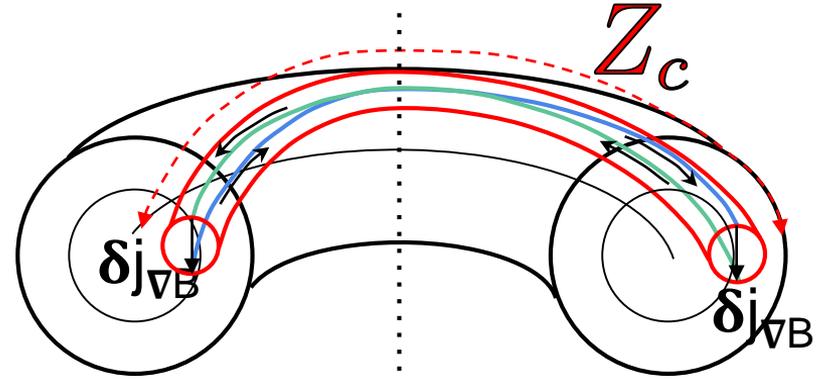
$$\frac{d\mathbf{V}_d}{dt} = A_{\nabla B} D_{IC} - D_{EC}$$

How D_{EC} & D_{IC} influence the deposition profile for different magnetic configuration ? (tokamak/Stellarator/RFP)

Competition between D_{EC} & D_{IC} - in a tokamak the external connection is the dominant effect



$$\tau_{EC} \sim \frac{Z_\infty}{C_A}$$



$$\tau_{IC} \sim \frac{Z_c}{C_s}$$

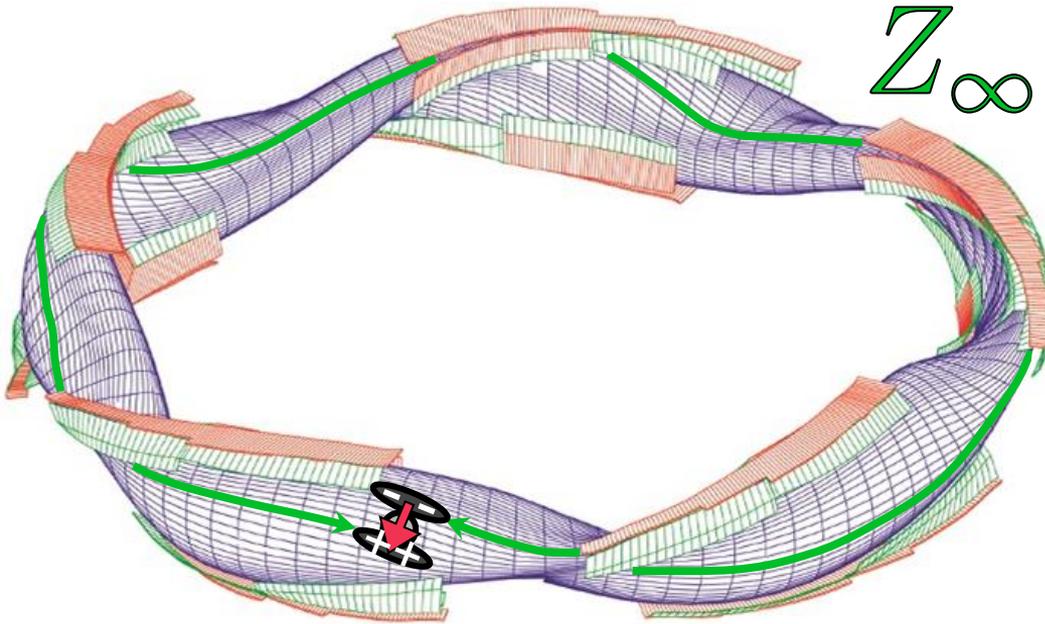
τ : efficient time
 $C_A \gg C_s$
 $Z_\infty > Z_c$

More efficient close to a rational q

$$\tau_{EC} \sim \frac{Z_{\infty}}{C_A} < \tau_{IC} \sim \frac{Z_c}{C_s}$$

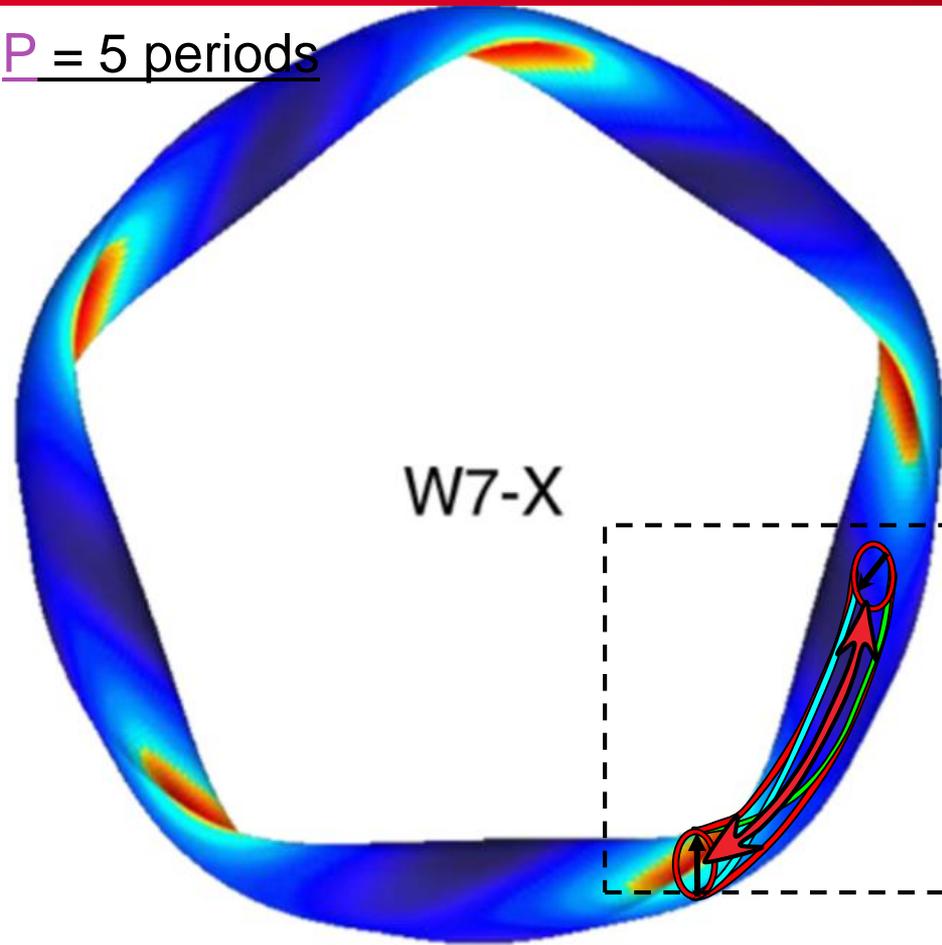
[Sakamoto 2013]

⇒ External Connection
more efficient for tokamak

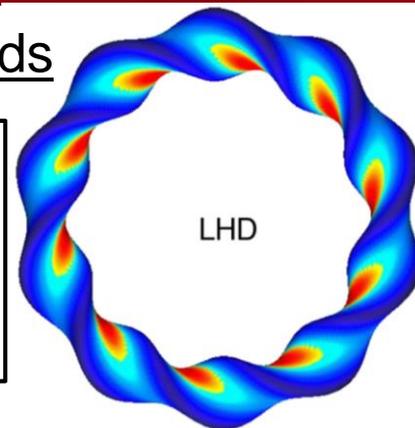


$$\tau_{EC} \sim \frac{Z_\infty}{C_A}$$

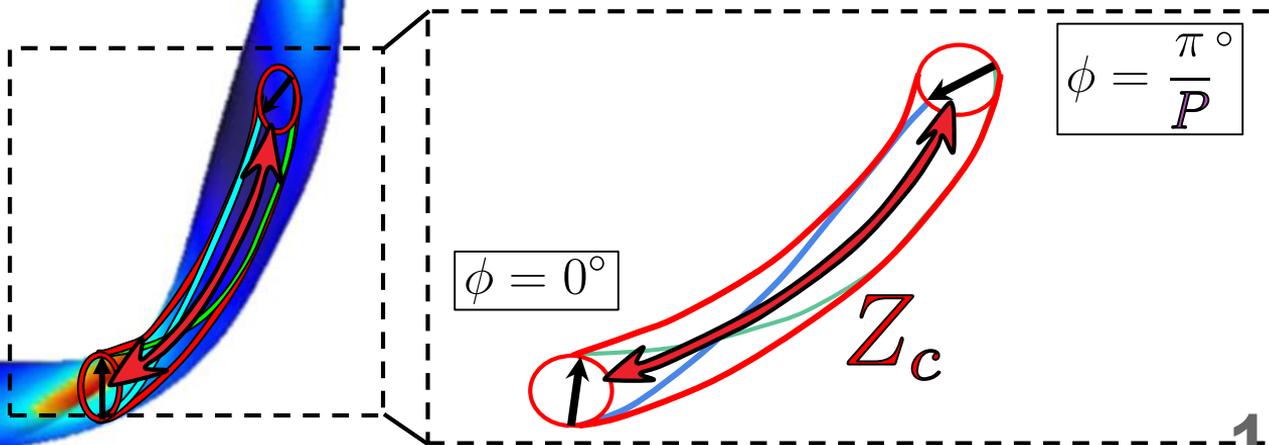
$P = 5$ periods



$P = 10$ periods



$$\tau_{IC} \sim \frac{Z_c(P)}{C_s}$$



$$\tau_{EC} \sim \frac{Z_{\infty}}{C_A} > \tau_{IC} \sim \frac{Z_c(P)}{C_s}$$

[Matsuyama 2012]

⇒ **Internal Connection** more efficient for stellarator

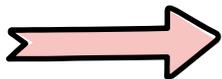
We have :

$$\star \tau_{EC} \text{ tokamak} \sim \tau_{EC} \text{ stellarator}$$

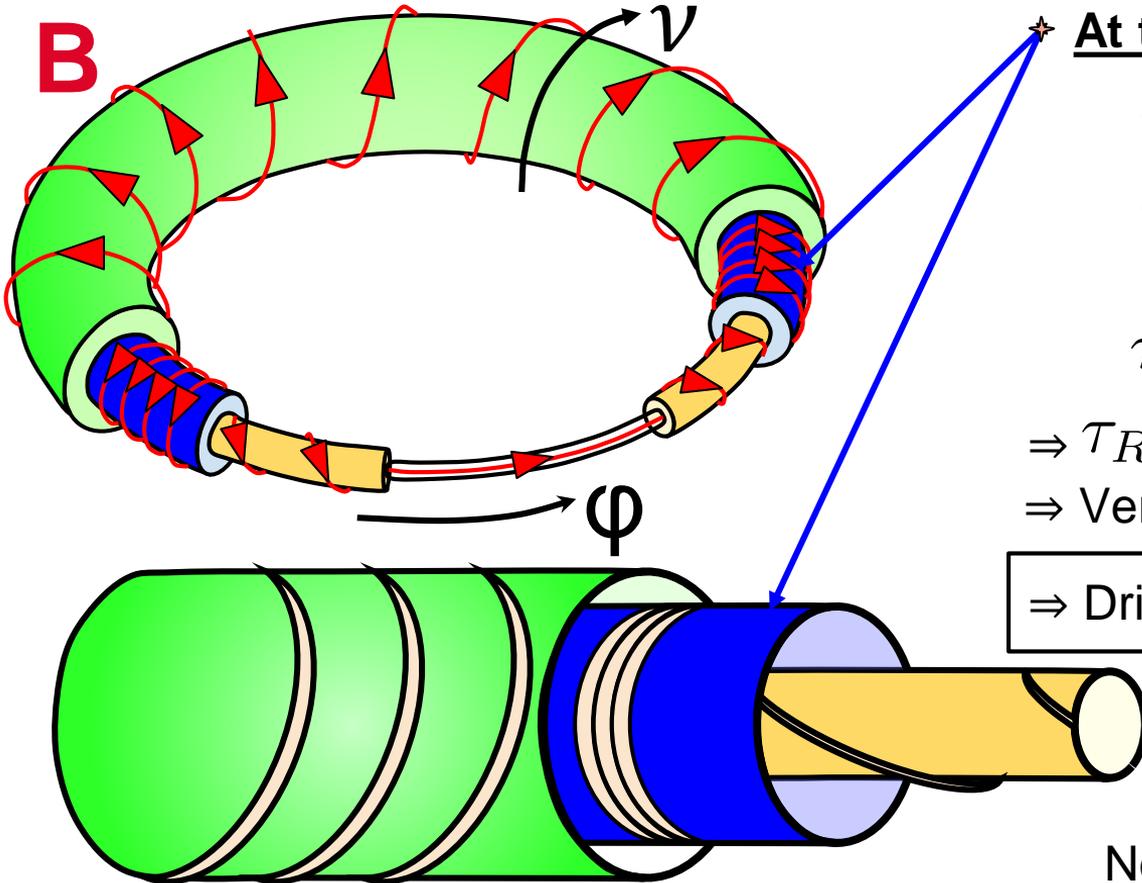
$$\star \tau_{EC} \text{ tokamak} < \tau_{IC} \text{ tokamak} \quad \& \quad \tau_{EC} \text{ stellarator} > \tau_{IC} \text{ stellarator}$$

Then :

$$\Rightarrow \tau_{EC} \text{ tokamak} > \tau_{IC} \text{ stellarator}$$



Drift displacement is smaller in a stellarator than in tokamak



At the reversal radius :

$$\left. \begin{aligned} \tau_{Ec} &= \frac{2\pi a}{C_A} \\ \tau_{IC} &= \frac{\pi a}{C_s} \end{aligned} \right\} \tau_{RFP} \propto a$$

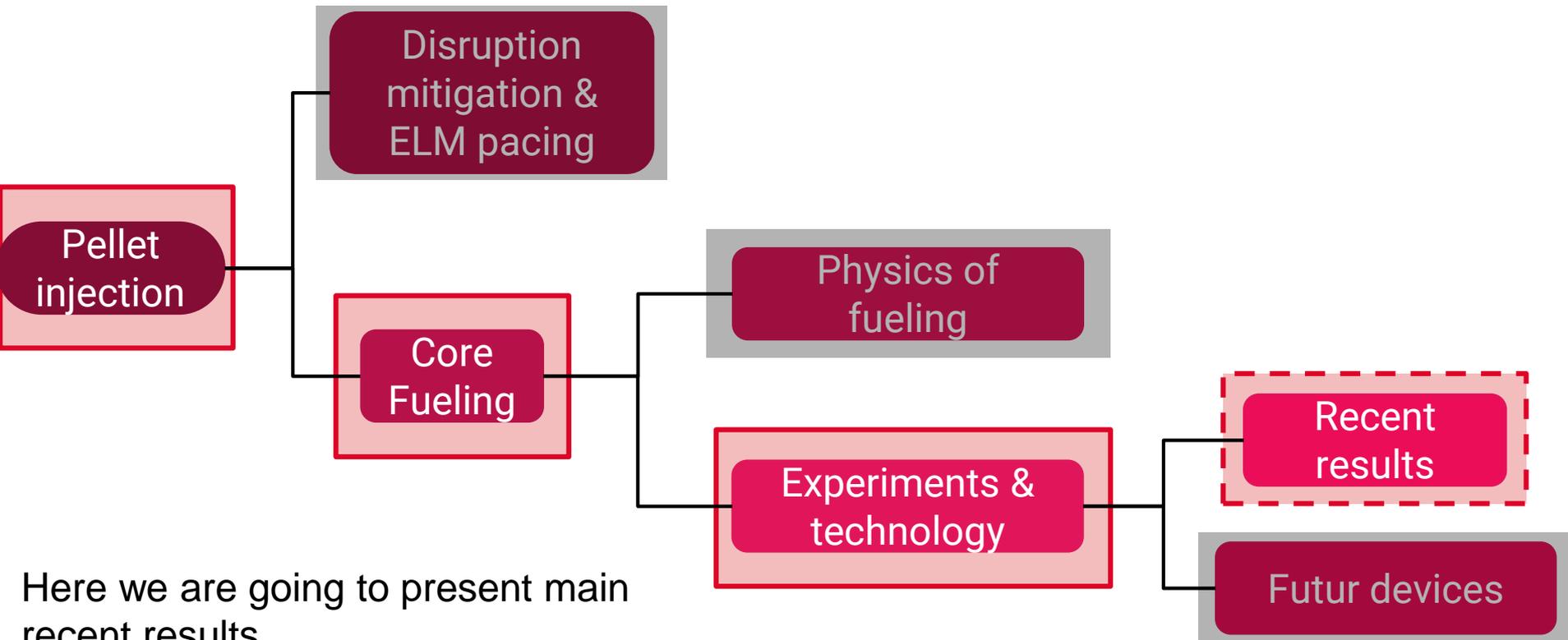
$$\neq \tau_{\text{tokamak, stellarator}} \propto R$$

$\Rightarrow \tau_{RFP} \ll \tau_{\text{tokamak, stellarator}}$
 \Rightarrow Very short drift time: magnetic shear

\Rightarrow Drift barrier

[Canton 2000]

No experiments made yet



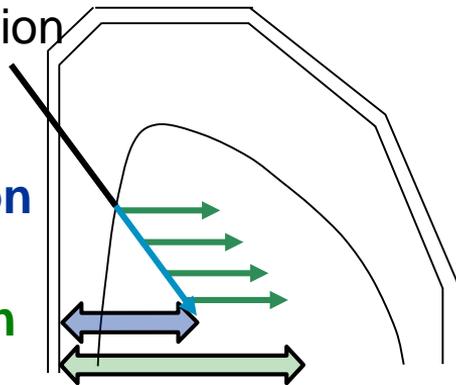
Here we are going to present main recent results
 ⇒ Similar results on other machines also exist

I - Better fueling from High field side in DIII-D due to the drift of the cloud

Pellet injection

Penetration length

Deposition length



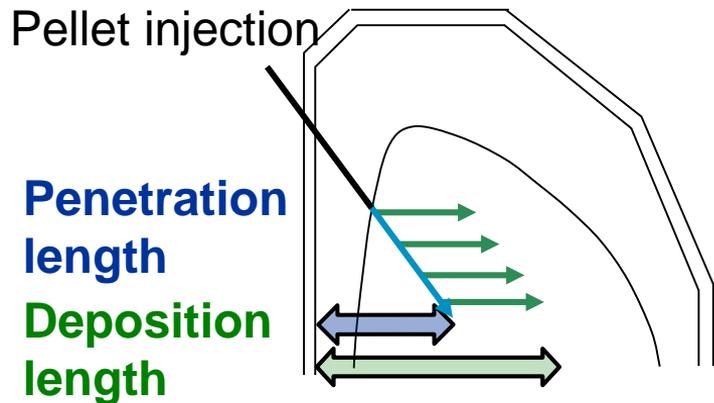
✦ Matter deposition deeper than pellet penetration :
⇒ Drift of the cloud

[Baylor 2007]

(ablation of the pellet)

(drift of the cloud)

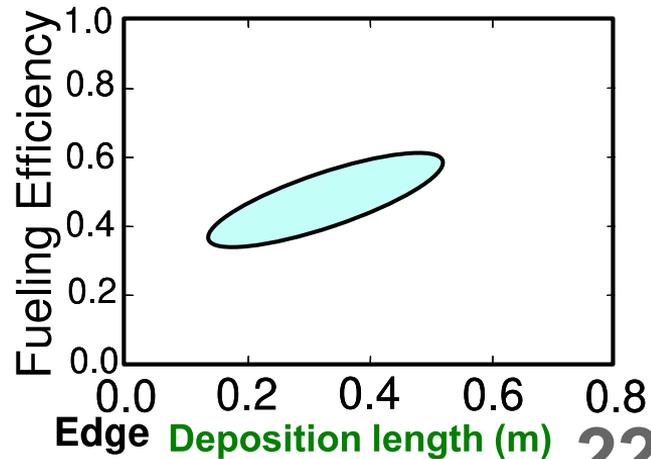
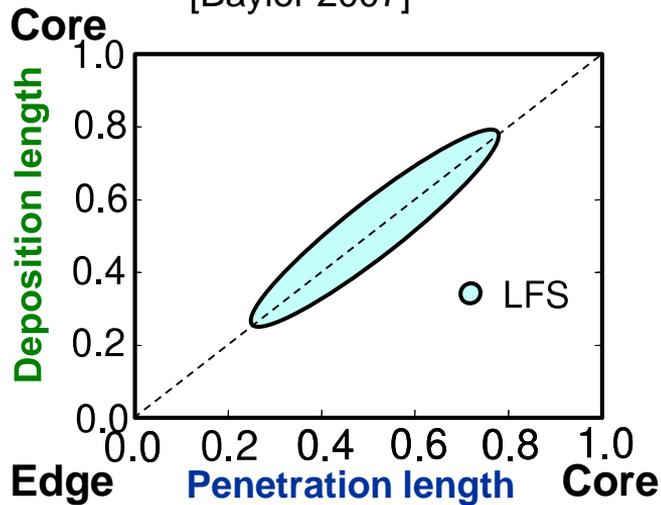
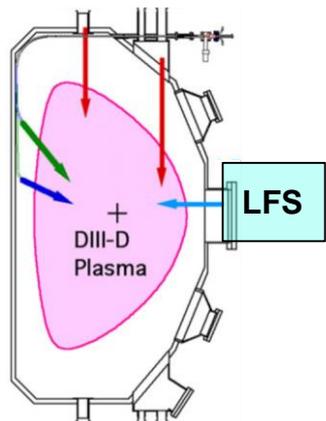
I - Better fueling from High field side in DIII-D due to the drift of the cloud



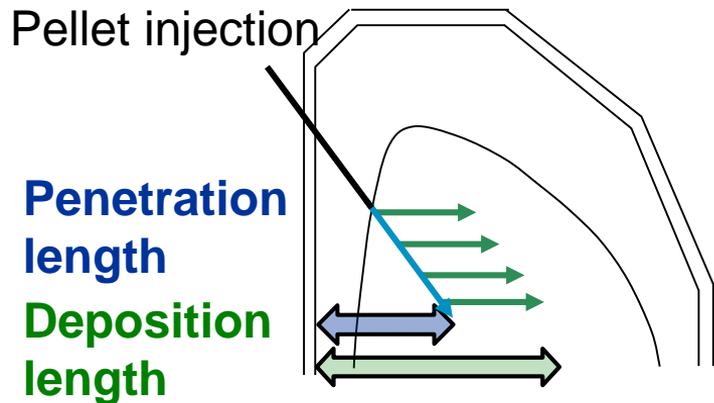
✦ Matter deposition deeper than pellet penetration :
⇒ Drift of the cloud

✦ Test of different injection points :
LFS : Deposition ~ penetration

[Baylor 2007]



I - Better fueling from High field side in DIII-D due to the drift of the cloud

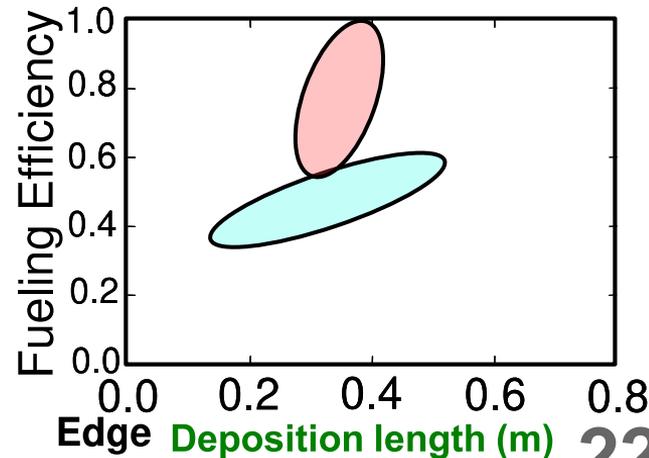
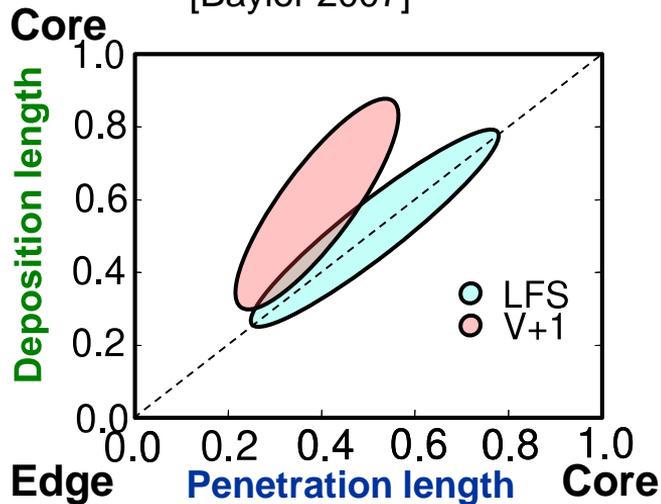
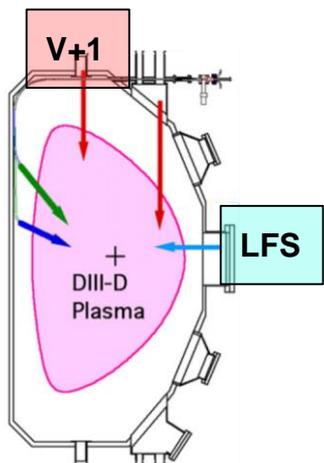


✦ Matter deposition deeper than pellet penetration :
⇒ Drift of the cloud

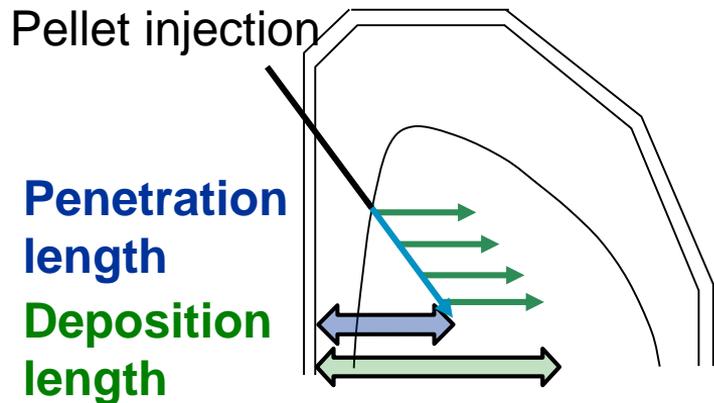
✦ Test of different injection points :

LFS	: Deposition ~ penetration
V+1	: Deposition ~ 2 x deeper than penetration

[Baylor 2007]



I - Better fueling from High field side in DIII-D due to the drift of the cloud

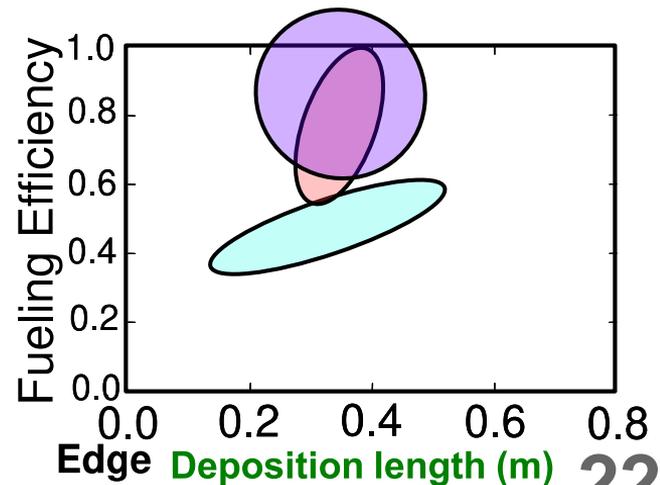
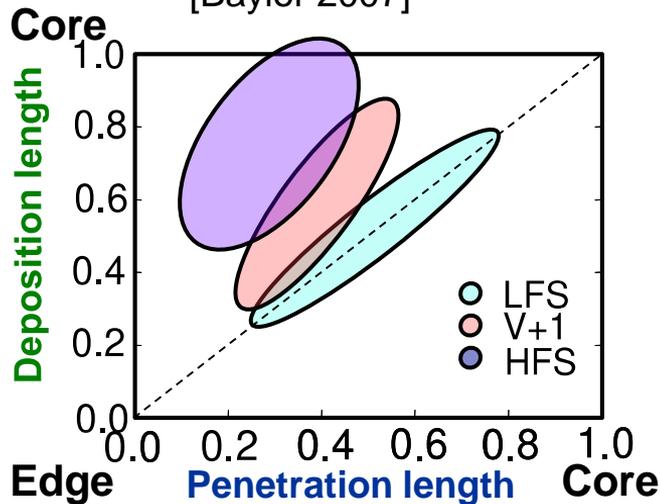
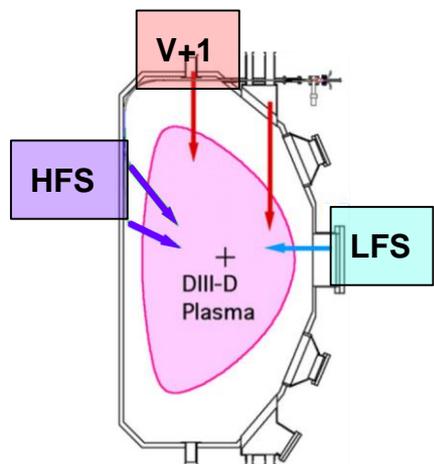


✦ Matter deposition deeper than pellet penetration :
⇒ Drift of the cloud

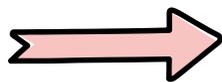
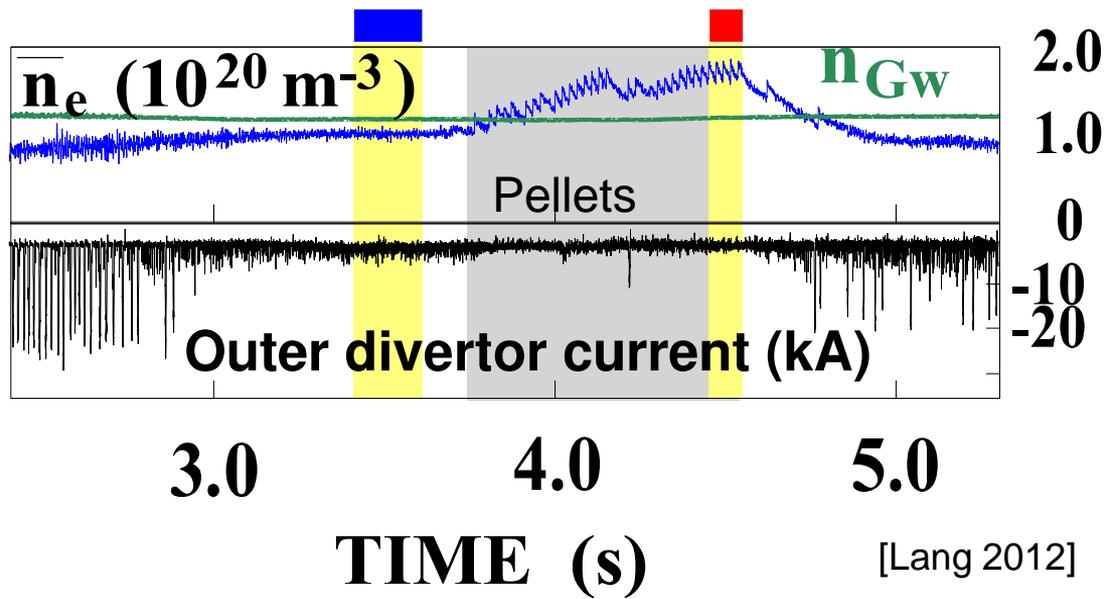
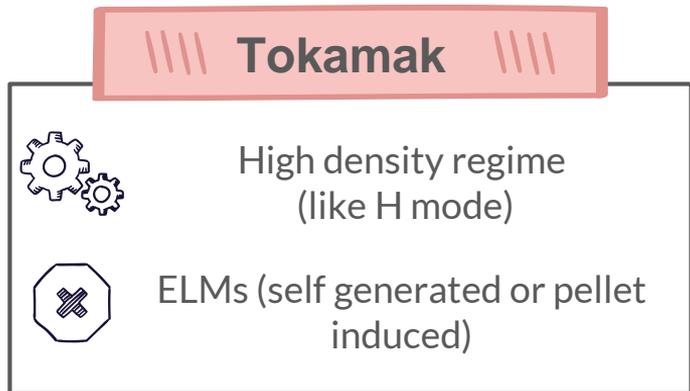
✦ Test of different injection points :

LFS	:	Deposition ~ penetration
V+1	:	Deposition ~ 2 x deeper than penetration
HFS	:	Deposition ~ 4 x deeper than penetration

[Baylor 2007]



II- Pellet fueling allows RMP ELM suppression above Greenwald density in ASDEX-Upgrade



Resonant Magnetic Perturbation (RMP) + Pellet allowed a density $> n_{GW}$ without ELM

Stellarator

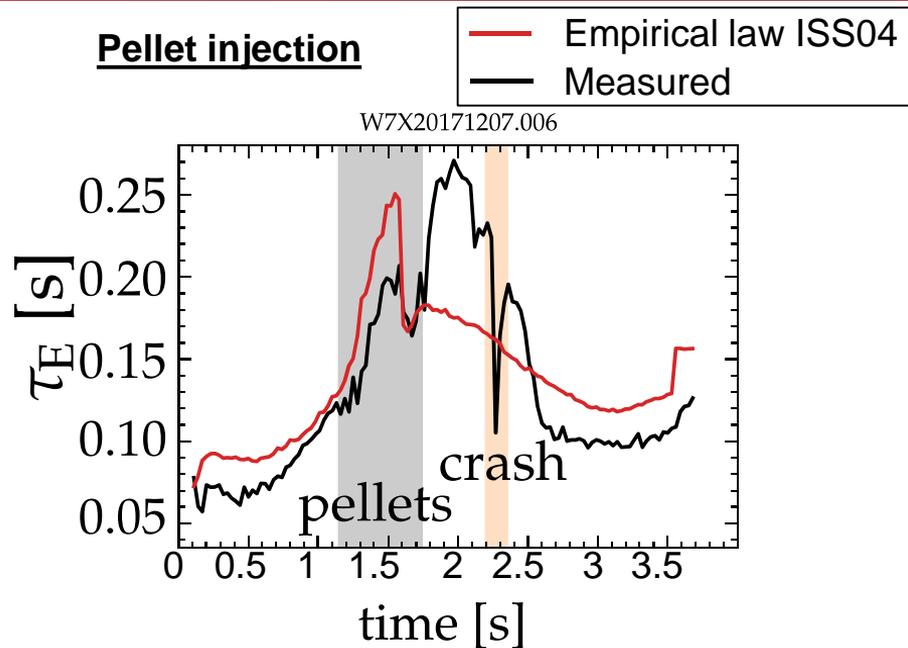


- High density regime
- Large confinement time



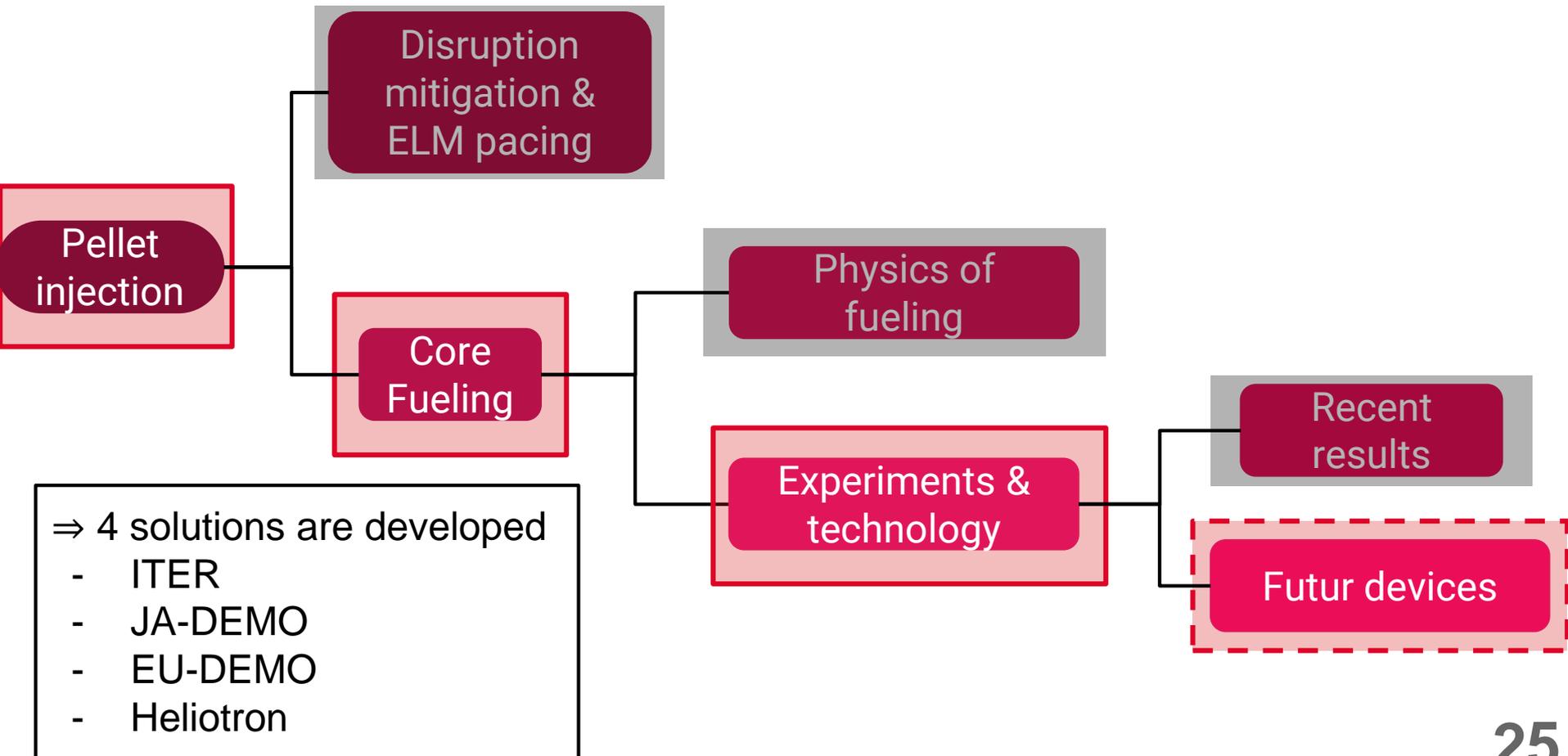
- Hollow density profile

Pellet injection



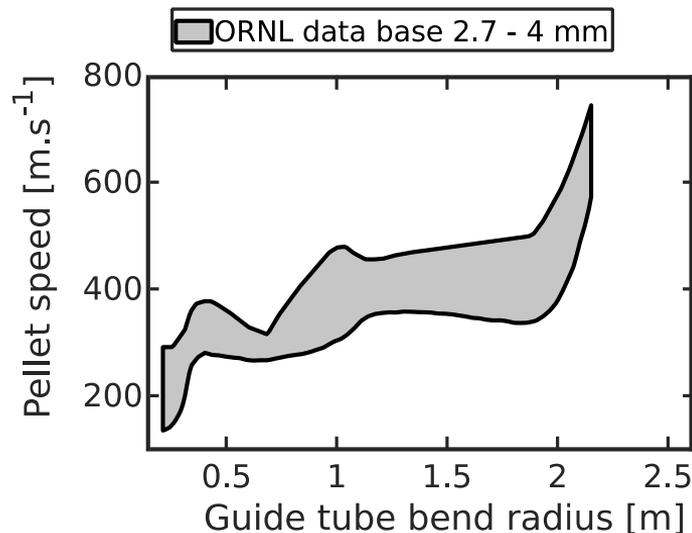
[Balchenkov 2018]

- ✦ Pellet increases core density
- ✦ Pellet increases global energy confinement time



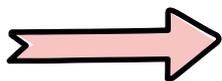
Futur devices will be large

- Large drift
- injection from HFS
- Bended guide tube
- Limited pellet speed V_p^{Max}



R_p (pellet radius) limited by plasma perturbation

[Poeckl 2021]



Balance to find between R_p & V_p^{Max}
Futur machines take into account pellet injector position

5 fueling system dimensioned :

2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

2 as project :

JA-DEMO (tokamak)

EU-DEMO (tokamak)

1 preliminary state :

FFHR (stellarator)

5 fueling system dimensioned :

2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

2 as project :

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1 preliminary state :

FFHR (stellarator)

	JT-60SA	ITER	JA-DEMO	EU-DEMO
Fueling rate	$\leq 62\text{mg/s}$	$\in [20,167]\text{mg/s}$	50mg/s	$\in [42,58]\text{mg/s}$

5 fueling system dimensioned :

2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

2 as project :

JA-DEMO (tokamak)

EU-DEMO (tokamak)

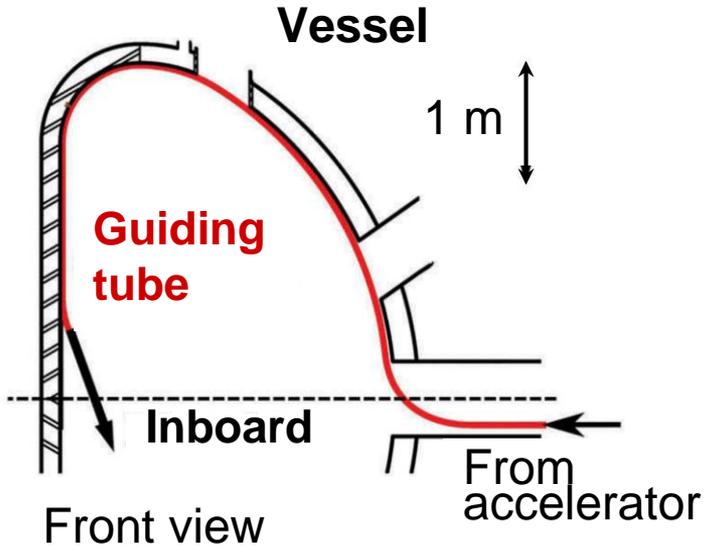
1 preliminary state :

FFHR (stellarator)

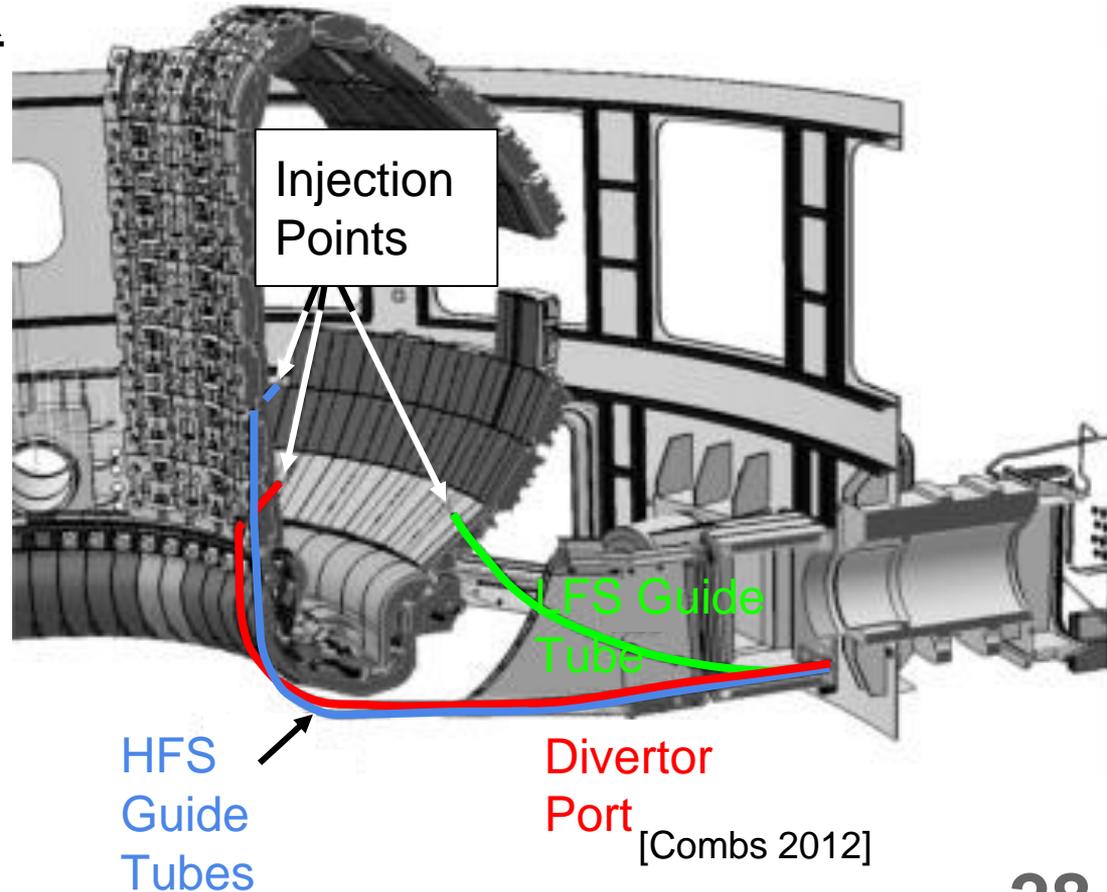
	JT-60SA	ITER	JA-DEMO	EU-DEMO
Fueling rate	$\leq 62\text{mg/s}$	$\in [20,167]\text{mg/s}$	50mg/s	$\in [42,58]\text{mg/s}$
Pellet Size	$\in [1,5]\text{mg}$ $\in [2,3]\text{mm}$	25mg 5mm	17mg 4mm	8mg 3.4mm



JT-60SA



ITER



[Lang 2019]

- Midplane or bottom injector
- strong tube bend

5 fueling system dimensioned :

2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

2 as project :

JA-DEMO (tokamak)

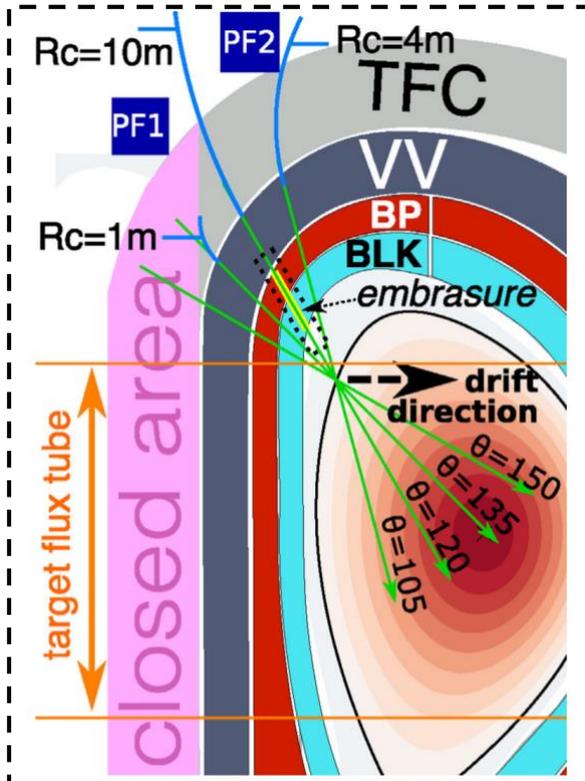
EU-DEMO (tokamak)

1 preliminary state :

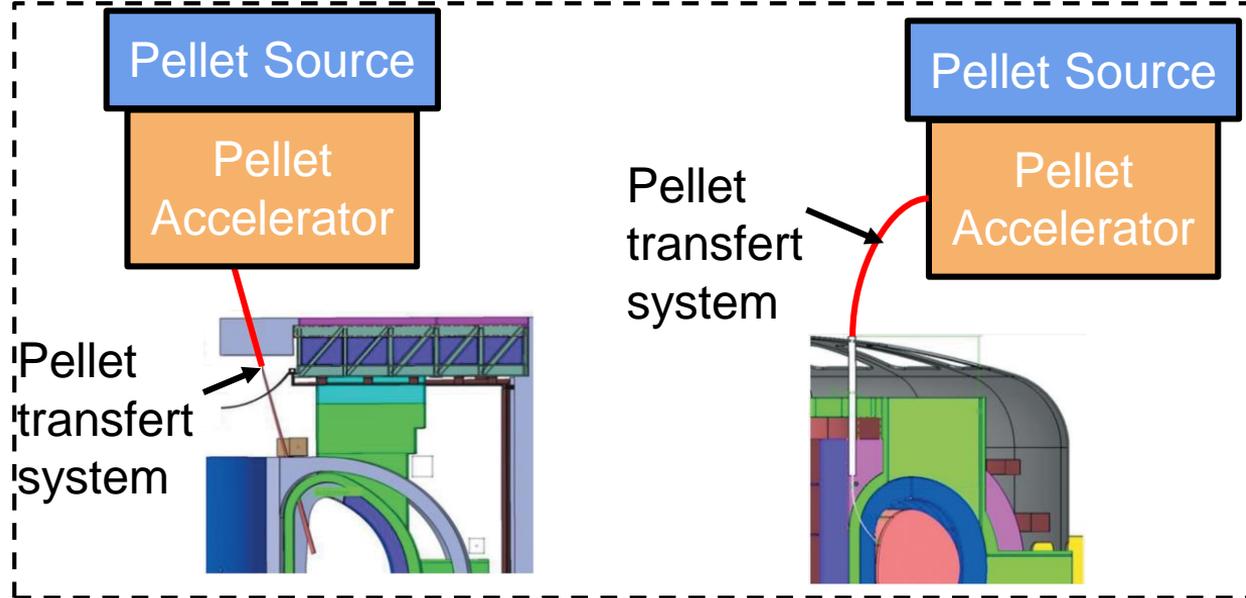
FFHR (stellarator)

	JT-60SA	ITER	JA-DEMO	EU-DEMO
Injector position	midplane	midplane - bottom		
Injection lines	small R_c	small R_c		
V_p^{Max}	470 m/s	300 m/s		
Injector type	centrifuge	1 stage pneumatic		

JA-DEMO



EU-DEMO



[Poeckl 2021]

[Tokugana 2017]

5 fueling system dimensioned :

2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

2 as project :

JA-DEMO (tokamak)

EU-DEMO (tokamak)

1 preliminary state :

FFHR (stellarator)

	JT-60SA	ITER	JA-DEMO	EU-DEMO	
Injector position	midplane	midplane - bottom	top	top	
Injection lines	small R_c	small R_c	Large R_c	Large R_c	
V_p^{Max}	470 m/s	300 m/s	2000m/s	1700m/s	3000m/s
Injector type	centrifuge	1 stage pneumatic	2 stage pneumatic	centrifuge - 1 stage pneumatic	2 stage pneumatic

5 fueling system dimensioned :

2 under manufacturing :

JT-60SA (tokamak)

ITER (tokamak)

2 as project :

JA-DEMO (tokamak)

EU-DEMO (tokamak)

1 preliminary state :

FFHR (stellarator)

	JT-60SA	ITER	JA-DEMO	EU-DEMO		FFHR
Fueling rate	$\leq 62\text{mg/s}$	$\in [20,167]\text{mg/s}$	50mg/s	$\in [42,58]\text{mg/s}$		200 mg/s
Pellet Size	$\in [1,5]\text{mg}$ $\in [2,3]\text{mm}$	25mg 5mm	17mg 4mm	8mg 3.4mm		40-60mg 5.6mm
V_p^{Max}	470 m/s	300 m/s	2000m/s	1700 m/s	3000 m/s	10 000 m/s

Speed not possible to reach yet

	JT-60SA	ITER	JA-DEMO	EU-DEMO		FFHR
Fueling rate	$\leq 62\text{mg/s}$	$\in [20,125]\text{mg/s}$	50mg/s	$\in [42,58]\text{mg/s}$		600 mg/s
Pellet Size	$\in [1,5]\text{mg}$ $\in [2,3]\text{mm}$	25mg 5mm	17mg 4mm	8mg 3.4mm		40-60mg 5.6mm
V_p^{Max}	470 m/s	300 m/s	2000m/s	1700 m/s	3000 m/s	1200 m/s

Not possible to increase pellet size

⇒ unacceptable jumps in fusion power & heat loads of the divertor

- ✦ Understand **Ablation and Homogenization physic** let us understand differences for tokamak/stellarator/RFP



- ✦ Fuelling using pellets allows **high performance discharges**

Tokamak

Stellarator

- $> n_{gw}$ without ELMs

- $\tau_E \nearrow$
- Peak density profil



- ✦ **Pellet injection line** to be considered from **very early stage** of the design of future devices.

- allows better fuelling efficiency
- reduced fuelled circulation