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A self-consistent cross-field transport model for edge tokamak plasma simulations: SOLEDGE modelling and comparison with experiments

DE LA RECHERCHE À L'INDUSTRIE

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# **Outline**





- Brief recall on transport codes and their applications
- Introducing turbulence in mean flow equations
  - The ideas from Computational Fluid Dynamics
  - The derivation for edge plasma transport codes
- Implementation in SOLEDGE code and application to modelling TCV and WEST experiments
- Summary and conclusions

#### G. Ciraolo, EPS 2022

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# CCC2 Tokamak edge plasma modelling with fluid transport codes

- <u>**Transport codes**</u> provide a coarse grained picture of edge plasma properties integrating the many actors at play: main plasma, neutrals, impurities, wall properties
- <u>Architecture</u>:
  - Fluid solver for the quasi-neutral plasma (main species + impurities)
  - Model to describe the plasma sheath
  - Databases or specific model to describe wall properties (recycling properties, sputtering...)
  - Solver for neutrals (fluid or kinetic)



Example of SOLEDGE-EIRENE simulations for WEST geometry

- <u>Reduction</u>: Radial turbulent transport treated with <u>empirical diffusion coefficients</u>
- **Non-exhaustive list of transport codes**: SOLEDGE-EIRENE, SOLPS-ITER, EDGE2D-EIRENE, EMC3-EIRENE, COREDIV, SONIC, UEDGE, ...

## Modelling radial transport in transport codes: the gradient-diffusion closure

Plasma mean-field transport solver

$$\frac{\partial n}{\partial t} + \boldsymbol{\nabla}.\left(n\boldsymbol{u}\right) = S(n, \boldsymbol{u}, \dots)$$

• Scale separation  $n = \overline{n} + \widetilde{n}$ 

 $u = \overline{u} + \widetilde{u}$ 

$$\frac{\partial \bar{n}}{\partial t} + \nabla \cdot \left( \bar{n} \overline{\boldsymbol{u}} + \langle \tilde{n} \widetilde{\boldsymbol{u}} \rangle_{t,r} \right) = S(\bar{n}, \overline{\boldsymbol{u}}, \dots) + \langle S(\tilde{n}, \widetilde{\boldsymbol{u}}, \dots) \rangle_{t,r} + \cdots$$



gradient-diffusion closure

$$\underline{\mathsf{re}} \quad \langle \tilde{n} \tilde{\boldsymbol{u}} \rangle_{t,r} = -Dn \boldsymbol{\nabla} \langle n \rangle$$



$$\frac{\partial \langle n \rangle}{\partial t} + \boldsymbol{\nabla} \cdot (\langle n \rangle \boldsymbol{v}_{\parallel} - D_n \boldsymbol{\nabla} \langle n \rangle) = S_n$$

- Solves only the fluctuation averaged fluid equations
- Diffusion coefficient is chosen to reproduce outer midplane profiles <u>from experiments</u>

### DERIVATION OF A SEMI-EMPIRICAL MODEL FOR TURBULENT INTENSITY IN EDGE TOKAMAK PLASMA

- Taking inspiration from the *κ ε* model for neutral fluids ([Jones, Launder 1971]) and prey-predator models [Miki, Diamond 2013]
- Transport equation for turbulent intensity  $\kappa = \frac{1}{2} \langle \tilde{u}^2 \rangle$  <u>H. Bufferand et al, CPP 2016</u>

- Source term:  $S_{\kappa} = \gamma_{int}\kappa$  with  $\gamma_{int}$  is the interchange growth rate  $\gamma_{int}^2 = c_s^2 \left(\frac{\vec{\nabla}B \cdot \vec{\nabla}p_i}{Bp_i} \frac{\Theta}{R^2}\right)$  with  $\Theta$  the interchange threshold so that interchange develops for  $\frac{R}{\lambda_p} > \Theta$  [X. Garbet et al., *Nucl. Fusion* **32** (1992)]
- *γint* : linear growth rate of the interchange instability (governs a ballooning of the local drive)
- Sink term:  $\varepsilon = \Delta \omega k^2$  represents turbulence non-linear saturation
- $\Delta \omega$  is the free parameter  $\rightarrow$  model closure: tuning with scaling law to improve predictive capabilities
- Assuming transport coefficient proportial to turbulent intensity ( $D \propto \kappa$ )

# DERIVATION OF A **SEMI-EMPIRICAL MODEL** FOR TURBULENT INTENSITY IN EDGE TOKAMAK PLASMA

- Neglecting transport, steady-state is reached when  $\gamma_{int}k = \Delta\omega k^2$  that is k = 0 or  $\mathbf{k} = \frac{\gamma_{int}}{\Delta\omega}$
- The SOL balance gives  $\frac{c_s}{L_{||}} \approx \frac{D}{\lambda_{SOL}^2}$  hence, recalling that  $D = kt_{||}$  and  $k = \frac{\gamma_{int}}{\Delta \omega}$
- $\Delta \omega = \frac{L_{||\gamma_{int}|}}{c_s \lambda_{SOL}^2}$
- The free parameter  $\Delta \omega$  is determined using the scaling law for  $\lambda_{SOL}$

$$\boldsymbol{\lambda_{SOL}} = \boldsymbol{\lambda_{SOL}^{scaling}} \sim 4\rho_i q_{95}$$

[R.J. Goldston Nucl. Fusion 2012]

$$\rho_i = \frac{m_i c_s}{q_i B_{tot}} \qquad q_{95} = \frac{a B_{\varphi}}{R B_{\theta}}$$

$$\frac{\partial \kappa}{\partial t} + \nabla . \mathbf{K} = \mathbf{\gamma}_{int} \kappa - \Delta \boldsymbol{\omega} k^2$$

[Scarabosio et al JNM 2013]



#### $\mathbb{C}\mathbb{Z}$ IMPLEMENTATION IN SOLEDGE AND APPLICATION TO TCV EXPERIMENT

- **One-equation model** implemented in SOLEDGE tested vs very well diagnosed TCV experiment (*Maurizio et* al., NF, 58 (2018); Gallo et al., PPCF, 60 (2018)])
- This experiment consists in L-mode, LSN discharges with same main plasma parameters and varying magnetic divertor geometry  $(L_{div})$ .



S. Baschetti et al., J. Phys.: Conf. Ser. (2018) S. Baschetti, PhD manuscript, Aix-Marseille University, 2019

### CO2 IMPLEMENTATION IN SOLEDGE AND APPLICATION TO TCV EXPERIMENT

**□** Simulation parameters: pure deuterium,  $n_{sep,OMP} = 0.7 \cdot 10^{19} m^{-3}$  and  $P_{in} = 100 kW$ ;

□ By changing the magnetic equilibrium, the **main plasma is not affected**;

□ Very good agreement between simulation results (----) with HRTS data (\*) in the SOL.



S. Baschetti et al., J. Phys.: Conf. Ser. (2018) S. Baschetti, PhD manuscript, Aix-Marseille University, 2019

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### POLOIDAL MAP OF DIFFUSION COEFFICIENT OBTAINED FROM SOLEDGE COUPLED TO THE EQUATION ON TURBULENT INTENSITY



### GENERALIZATION TO 2-EQUATIONS MODEL FOR TURBULENCE INTENSITY

• Two transport equations on turbulent intensity and its dissipation rate from a heuristic approach (Baschetti *et al.* NF 2021):

$$\frac{\partial \kappa}{\partial t} + \nabla . \mathbf{K} = \gamma_{\kappa} \kappa - \varepsilon \qquad \qquad \kappa \equiv \frac{1}{2} \langle \tilde{v}_{\perp}^2 \rangle$$
$$\frac{\partial \varepsilon}{\partial t} + \nabla . \mathbf{E} = \gamma_{\varepsilon} \varepsilon - \beta_{\varepsilon} \varepsilon^2 \qquad \qquad \varepsilon \equiv \kappa / \tau_{\kappa \varepsilon}$$

Rate of turbulent energy dissipation (drive the damping of the fluctuations) with  $\tau_{\kappa\varepsilon}$  characteristic time of turbulence

• Quadratic saturation term for  ${m arepsilon}$ 

Linear driving terms

$$\beta_{\varepsilon} = \frac{V}{\kappa^{3/2}}$$
 with  $V = \rho^* c_S$   $\gamma_{\kappa} = \gamma_{\varepsilon} = \gamma = \frac{c_S}{R} \sqrt{R^2 \frac{\nabla p \cdot \nabla B_t}{pB_t}}$ 

κ²

10

# APPLICATION TO WEST EXPERIMENT #55049

- $\circ$  Plasma composition
  - Pure Deuterium
- **o** Wall parameters
  - Recycling coefficients of the wall is 0.99.
  - Red line on the wall represent the passive pumping with the recycling coefficient 0.9
- $\circ~$  Core boundary conditions
  - P<sub>in</sub>=P<sub>tot</sub>-P<sub>radiated,bulk</sub>-P<sub>ripple</sub>= 1 MW
  - Plasma density controlled by gas puff injection
- Transport coefficients obtained from  $\kappa \varepsilon$  model





Contour plot of k/k<sub>max</sub> in the poloidal plan (logarithmic scale) Diffusion coefficient D in the poloidal plan (logarithmic scale)



- Recovering the ballooned radial transport
- Spreading of κ and D governed by parallel transport in the near SOL region

Baschetti et al. NF 2021

# **Cea** RADIAL TRANSPORT AND COMPARISON WITH 3D TURBULENT SIMULATIONS

Diffusion coefficient D in

the poloidal plan

(logarithmic scale)

Contour plot of k/k<sub>max</sub> in the poloidal plan (logarithmic scale)



Poloidal map of density fluctuations obtained from 3D turbulence simulation performed with SOLEDGE3X.



### Baschetti *et al*. NF 2021 H. Bufferand et al, NF 2022

#### COMPARISON BETWEEN EXPERIMENTAL AND SIMULATION PROFILES Cez (WEST #55049)

WEST

 $_{at}$  (10<sup>5</sup> A / m<sup>2</sup>)



#### outer midplane profiles



SE2D

20

R - R<sub>sep</sub> (mm)

outer target profiles

T<sub>a</sub> and n<sub>a</sub> radial profiles at the outer midplane (radial extension where experimental data are available)

Ion saturation current and parallel heat flux at the outer strike point

- Agreement in the near SOL region  $(0.01m \le R R_{sep} \le 0.03m)$
- Too strong numerical gradients in the far SOL  $(0.03m < R R_{sep} \le 0.05m)$

Baschetti et al. NF 2021

20

R - R<sub>sep</sub> (mm)

SE2D

# SUMMARY AND CONCLUSIONS

- We address the issue of modelling radial transport in edge plasma transport codes
- **Taking inspiration from what have been done in CFD community** we introduced a self-consistent approach for turbulent intensity from which one can derive the radial transport coefficients
  - a single scalar to be fixed
  - 2D map of radial transport obtained with this approach (recovering the ballooning feature)
- Results from SOLEDGE simulations in L-mode plasma coupling transport equations with κ–ε model for radial transport: good match with the experimental profiles, both at the divertor and at the midplane is found for TCV and WEST experiments
- Increasing the database and comparison with turbulent 3D simulations
- Generalization to transport simulations with impurities
- Ongoing work for introducing in the κ–ε model the dependence of the radial coefficients on ExB shear flow intensity in order to address the L-H transition

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