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# Interpretation of GEDEON-1 and GEDEON-2 gadolinium depletion experimental analysis with the DARWIN2.3 package

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## ABSTRACT

*In the eighties a two phases experimental program, called GEDEON, was designed at CEA for the validation of gadolinium depletion calculation in a 13 x 13 LWR assembly (3.25% <sup>235</sup>U enrichment). In the first experiment, gadolinium pins are enriched with 3.5% of <sup>235</sup>U and contained 5% in mass of natural gadolinium. In the second experiment gadolinium support pins are made of depleted uranium (0.2% <sup>235</sup>U) and contain 8% in mass of natural gadolinium. DARWIN is an evolution code package developed at CEA in cooperation with industrial companies (EDF, Framatome, Orano) in order to compute physical quantities of radioactivity related to various application fields such as nuclear fuel cycle. This paper presents the first interpretation, with DARWIN2.3 package, of those two experiments with the aim of gadolinium depletion experimental validation of DARWIN. Interpretations are performed using the European evaluation file JEFF-3.1.1 and a 281 group energy mesh. Results show quite good agreements between calculations and measurements, in respect with experimental and calculation uncertainties, especially for <sup>155</sup>Gd and <sup>157</sup>Gd isotopes depletion.*

## KEY WORDS

*Gadolinium depletion, burnable poison, DARWIN.*

## 1. INTRODUCTION

Burnable poisons incorporated in UO<sub>2</sub> fuel rods, such as gadolinium oxide (Gd<sub>2</sub>O<sub>3</sub>), give an opportunity to increase the length of nuclear reactor fuel cycle by allowing the use of higher fuel enrichment. Assemblies incorporating such poisoned fuel rods (up to 8% of Gd<sub>2</sub>O<sub>3</sub>) are included in some French core management. Moreover, such assemblies containing gadolinium loaded pins are planned to be used in the first core of the new EPR<sup>TM</sup> GEN-3 reactor. Gadolinium depletion, which is faster than fuel depletion, may introduce an increase of the assembly reactivity. To be able to correctly estimate the occurrence of such reactivity peak, as well as its intensity, it is necessary to have an accurate evaluation of the gadolinium isotopes neutron capture behavior. The latter requires a rigorous experimental validation of gadolinium isotopes depletion calculation.

The GEDEON two phases experimental program was held in the frame of qualification studies of neutron calculation of assemblies containing pins loaded with gadolinium oxide as burnable poison [1] [2] [3]. Those experiments took place at the MELUSINE research reactor located at CEA/Grenoble, from November 1982 to February 1984, and from May 1985 to March 1988. The aim of GEDEON-1 [2] was the qualification of <sup>155</sup>Gd and <sup>157</sup>Gd depletion in isolated gadolinium pins, up to an assembly burnup of 10 GWj/t. GEDEON-2 [3] was designed to qualify, up to an assembly burnup of 13 GWj/t, the azimuthal effects of adjacent gadolinium rods and the presence of water holes in front or in the angle of such gadolinium rods. Both experiments, GEDEON-1 and GEDEON-2, were performed on a 13x13 PWR assembly (UO<sub>2</sub> enriched with 3.25% <sup>235</sup>U) containing several UO<sub>2</sub>-Gd<sub>2</sub>O<sub>3</sub> pins. In the first experiment assembly, irradiated up to a burnup of 10 GWj/t, gadolinium pins were also made with UO<sub>2</sub> enriched with 3.25% of <sup>235</sup>U and contained 5% of natural gadolinium. In the second experiment assembly, irradiated up to a burnup of 13 GWj/t, gadolinium pins were made of depleted uranium (0.2% of <sup>235</sup>U) and contained 8% of natural gadolinium.

Those two experiments have been previously interpreted with the deterministic code APOLLO2.8 [4], associated with the nuclear data base JEFF-3.1.1 [5], showing a good agreement between measured and calculated gadolinium depletion [2] [3].

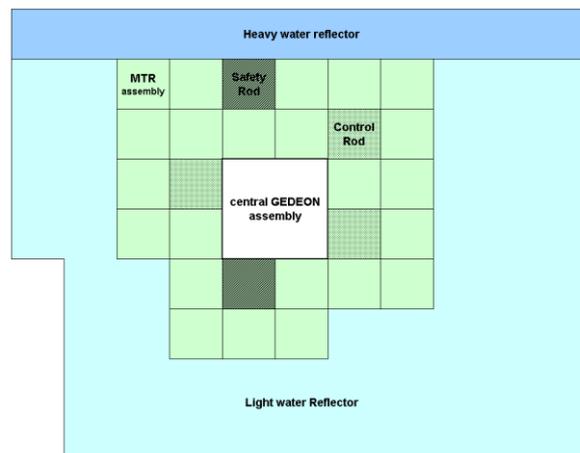
This paper describes the first interpretation of those experiments using the last version of the French reference package for fuel cycle studies, DARWIN2.3 [6], with the aim of its experimental validation regarding gadolinium depletion. In addition of gadolinium isotopes depletion analyses, calculation of major actinides concentrations (uranium isotopes in GEDEON-1 and -2, and plutonium isotopes in GEDEON-1), was also compared with measurements. The latter were also measured in a so called monitor pins (located near the centre of the assembly), and in UO<sub>2</sub> pin adjacent to the gadolinium one. Since neodymium fission products (<sup>148</sup>Nd, <sup>150</sup>Nd, <sup>145</sup>Nd and <sup>146</sup>Nd) are considered directly proportional to the number of fissions, their concentrations, in the monitor pin, were used to calibrate calculation assemblies' power during irradiation. Analyses of the adjacent UO<sub>2</sub> give an indication on the flux depletion around the gadolinium pins.

This paper presents the experimental data of GEDEON-1 and GEDEON-2 experiments, the DARWIN2.3 package and the calculation hypothesis. Then comparisons between calculation and measurement are presented and discussed.

## 2. EXPERIMENTAL DATA

### a. MELUSINE reactor

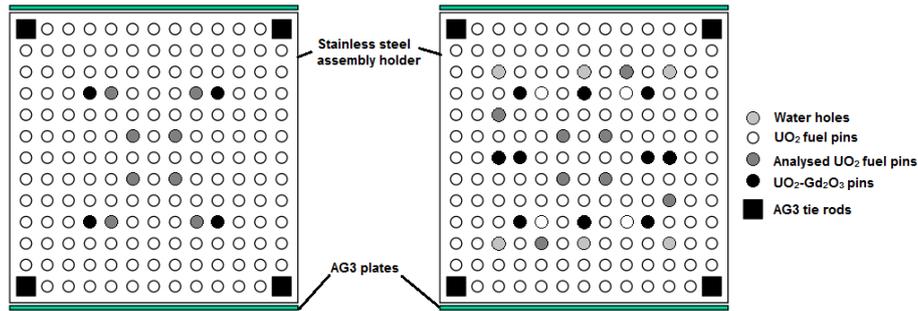
MELUSINE was an 8 MWth experimental reactor located at CEA Grenoble, and was dismantled in 2002. Experimental assembly was placed in the centre of the MELUSINE driver core made of MTR assemblies (Material Test Reactor made of highly enriched Uranium–Alloy plates), surrounded by a D<sub>2</sub>O and H<sub>2</sub>O reflector, as shown in Figure 1.



**Figure 1: Radial cross section of MELUSINE reactor**

### b. GEDEON experiments

Central assemblies from GEDEON-1 and GEDEON-2 experimental programs are illustrated in Figure 2. They are both based on a regular 13 x 13 square pattern supported by a stainless steel box, AG3 structural elements (tie rods, plates), and surrounded by water.



**Figure 2 : GEDEON-1 (on the left) and GEDEON-2 (on the right) assemblies**

Three and four successive discharges were considered respectively for GEDEON-1 and GEDEON-2 experiments. At each discharge, a set of several pins is removed and replaced in successive quadrants of the assemblies. These removed pins are then chemically analysed by Inductive-Coupling-Plasma and Mass Spectrometry. Moreover, two fissile heights were analysed for most of the rods: 270 mm from the bottom of the active fuel (mid height), and 100 mm in order to obtain a lower burnup. Gadolinium pins from GEDEON-2 assembly are located either near a water hole (face or angle) or another gadolinium pin. Based on usual PWR gadolinium assemblies' configuration, where most of gadolinium pins are located near a water hole (angle), only analyses of gadolinium pins in such a position in the GEDEON-2 assembly are considered in this study.

For the GEDEON-1 experiment, since no precise history of irradiation is available, irradiation is supposed continuous for each cycle without any cooling time between cycles. For GEDEON-2, irradiation is also supposed continuous for each cycle, and cooling times between cycles are provided. Table I resumes the irradiation time and assembly BU corresponding to each cycle, and the cooling time, when it is available, between cycles and between extraction and analyses of the different UO<sub>2</sub> (monitor and adjacent) and UO<sub>2</sub>-Gd<sub>2</sub>O<sub>3</sub> (gadolinium) pins.

**Table I : Irradiation time (supposed to be continuous), and cooling time associated with each GEDEON-1 and GEDEON-2 irradiation cycle**

	GEDEON-2				GEDEON-1				
	Assembly BU (GWd/t)	Time (days)	Cooling time (days)		Assembly BU (GWd/t)	Time (days)	Cooling time (days)		
			Monitor	Adjacent			Monitor	Adjacent	Gado
<b>Cycle 1</b>	≈ 3.5	171	434	455	≈ 3.0	134	199	200	203
Inter-cycle		251							
<b>Cycle 2</b>	≈ 7.0	192	385	503	≈ 6.4	196	150	172	152
Inter-cycle		23							
<b>Cycle 3</b>	≈ 10.0	179	1105	1137	≈ 8.9	91	412	362	316
Inter-cycle		11							
<b>Cycle 4</b>	≈ 13.0	114	1692	1643					

### 3. CALCULATION TOOL AND MODELS

#### a. The DARWIN2.3 package

The DARWIN package [6] is the French reference calculation package for the fuel cycles of all types of reactors (PWR, BWR, FBR, advanced reactor) and fuels (UOX, MOX, innovative fuels). It has been developed by CEA and its French partners (EDF, Framatome, Orano) to estimate the physical quantities (material balance; decay heat; activity; neutron, alpha, beta and gamma sources and spectra; radiotoxicity)

which characterized reactors spent fuels. DARWIN is also used in the back-end cycle for actinide incineration or long-term interim storage studies.

b. Calculation scheme description

The optimized and validated REL2005 scheme for LWR calculation is based on the APOLLO2.8 code developed by the CEA [4]. In the specific case of fuel cycle studies, a consistent scheme CYCLE2008 has been developed and validated using the benefit of the validation program of the REL2005 scheme. It should be noted that the accuracy of the DARWIN results depends mainly on the APOLLO2 assembly calculation. The CYCLE2008, uses the CEA2005 cross-section library in a 281-group-structure Santamarina-Hfaiedh energy mesh [7] (SHEM) processed from the JEFF-3.1.1 evaluation [5]. Neutron energy spectrum is first calculated in a 2-D assembly geometry, using a Pij multicell model. The fuel pellets are split into four rings, and the gadolinium one into 6 rings because of the very high capture cross section of gadolinium. Local spectrum calculation is performed in the SHEM 281-energy-group structure. Space-dependent self-shielding (used only  $>23$  eV, which is the upper limit of the fine mesh in SHEM) is repeated at the recommended burnup steps, optimized consistently with the REL2005 recommendations (0, 4, 8, 12 and every 12 GWd/t), as well as at every change of core parameter (case of detailed cycle monitoring). Then the Method Of Characteristic solvers (MOC) flux calculation is performed using a precise 2-D geometry. Refined burnup steps are used for the depletion calculation based on the MOC flux (in MWd/t : 0, 9.375, 18.75, 37.5, 75, 112.5, 150, 237.5, 325, 412.5, 500, 625, 750, 1000, steps of 250 up to 2000, steps of 500 up to 20000, and then a step every 2000). Additional steps corresponding to the burnup at the end of each cycle are added. Because of convergence issues, the evolution step following the latter is subdivided into three smaller steps. The PEPIN2 depletion module then uses the results provided by APOLLO2, i.e. self-shielded cross sections and multigroup spectra, to produce the collapsed library with burnup-dependent cross sections, required in order to characterize the isotopes described in the depletion chains.

c. Calculation geometry description

Because of self-shielding treatment in APOLLO2, all various pins are considered at the same effective temperature. The pellet cladding is made of zircaloy. For the self-shielding calculation, gadolinium cells and cells around, cells on assembly periphery and the monitor cell are calculated individually. The water around the assembly is homogenized with the stainless steel assembly support and AG3 plates. The whole reflector is considered as light water, without heavy water. The MTR buffer zone is made of UAl plates enriched with 93.5% of  $^{235}\text{U}$ . To reduce time calculation, the latter is replaced by an homogeneous medium corresponding to an average burnt UAl assembly containing traces of majors fission products.

Analyzed pins are made of :

- Enriched  $\text{UO}_2$  with 3.25%  $^{235}\text{U}$  for GEDEON-1 and GEDEON-2 (monitor and adjacent pins)
- $\text{Gd}_2\text{O}_3$  with enriched  $\text{UO}_2$  with 3.25%  $^{235}\text{U}$  and 5% of natural gadolinium for GEDEON-1
- $\text{Gd}_2\text{O}_3$  with depleted  $\text{UO}_2$  with 0.2%  $^{235}\text{U}$  and 8% of natural gadolinium for GEDEON-2

Due to experimental conditions, GEDEON-1 assembly is simulated with APOLLO2 with a 1/8 symmetry, see Figure 3. Because of some pins displacement during GEDEON-2 experimental program, as illustrated on the same figure, the whole assembly and core are modeled. Reflector and MTR buffer zone are supposed to be symmetrical.

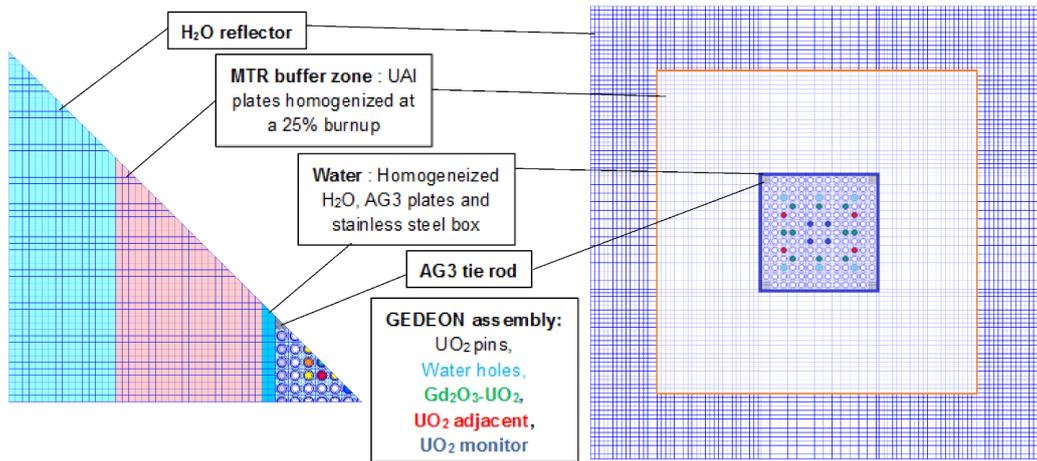


Figure 3. APOLLO2 calculation geometries (GEDEON-1 on the left, GEDEON-2 on the right).

#### 4. ANALYSES INTERPRETATION

##### a. Burnup calibration from monitor fuel pins

Neodymium isotopes,  $^{145}\text{Nd}$ ,  $^{146}\text{Nd}$ ,  $^{148}\text{Nd}$  and  $^{150}\text{Nd}$ , are stable (or at least with a period longer than  $10^{18}$  years), are mainly produced by fission, and with a negligible capture rate. Furthermore, their cumulated fission rates have very small uncertainties (about 1 to 3%). For all these reasons, they are good burnup indicators, and thus are used to calibrate assembly power through the corresponding irradiation time. Equation (1) gives the expression of the recommended burnup calibration factor.

$$F = \frac{1}{4} \left[ \frac{C_{148\text{Nd}}}{E_{148\text{Nd}}} + \frac{C_{150\text{Nd}}}{E_{150\text{Nd}}} + 2 \times \left( \frac{C_{145\text{Nd}} + C_{146\text{Nd}}}{E_{145\text{Nd}} + E_{146\text{Nd}}} \right) \right] \quad (1)$$

With  $C_X$  and  $E_X$  the calculated and measured concentrations of the isotope X.

Preliminary studies of GEDEON-1 experiment, point out some issues with  $^{150}\text{Nd}$  analyses [2], especially for the first cycles. To avoid any bias, this isotope is not considered in the calibration factor for the first cycles of GEDEON-1. Otherwise, all four isotopes were used when measurements were available. When no experimental neodymium isotopes concentrations are available (which is the case for some GEDEON-2 measurements), the  $^{235}\text{U}$  isotope concentration is chosen for burnup calibration. All assembly burnup, after calibration, are presented in Table II.

**Table II : GEDEON-1 and -2 assembly burnup corresponding to 100 mm and 270 mm samples height, after neodymium calibration from monitor pins.**

Assembly BU (GWd/t)	GEDEON-1			GEDEON-2			
	Cycle 1	Cycle 2	Cycle 3	Cycle 1	Cycle 2	Cycle 3	Cycle 4
100 mm	2.8	5.8	8.1	3.9	6.9	9.3	11.1
270 mm	3.2	7.0	9.6	4.6	7.7	10.7	12.8

Calculation/experiment ratio observed on  $^{145}\text{Nd}$ ,  $^{146}\text{Nd}$  and  $^{148}\text{Nd}$  isotopes ( $< 1\%$ ) for monitors pins show that burnup calibration is correct. As mentioned previously, strong underestimation of  $^{150}\text{Nd}$  isotope for the two first cycles of GEDEON-1 (about 8%), much higher than usually observed in such interpretations, may raise questions about the accuracy of the measurement.

b. Calculation/experiment ratio uncertainties

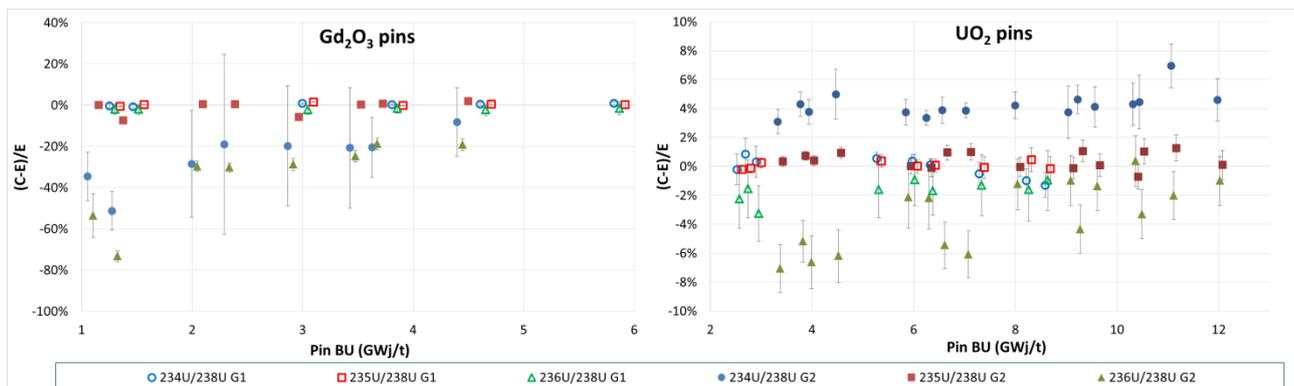
Calculation/experiment ratio uncertainties are related to :

- Experimental uncertainty of chemical analyses,
- Initial isotopic composition uncertainty on  $^{235}\text{U}$ ,  $^{155}\text{Gd}$ ,  $^{157}\text{Gd}$  et  $\text{Gd}_{\text{tot}}$ , from experimental report (respectively 0.15%, 0.14%, 0.13%, and 0.4% in relative, at  $1\sigma$ ),
- Temperature uncertainty on fuel ( $T_{\text{comb}} \pm 50^\circ\text{C}$ , at  $1\sigma$ ) and moderator ( $T_{\text{mod}} \pm 2^\circ\text{C}$ , at  $1\sigma$ ): generally accepted upper values for the uncertainties of codes solving heat equations,
- Burnup (BU) calibration uncertainty from calculation/experiment ratio of neodymium isotope concentration commonly considered about 2% at  $1\sigma$ .

The relative calculation/experiment ratio uncertainty associated to each parameters listed above is determined by direct perturbation in APOLLO2 calculation. The relative calculation/experiment ratio variation is then associated to the uncertainty due to the corresponding perturbed parameter. Since all uncertainty sources are considered independent, the total uncertainty on the relative calculation/experiment ratio is obtained by a quadratic sum. The total calculation/experiment ratio uncertainty is mainly due to the 2% BU uncertainty, except for  $^{234}\text{U}$  isotope in GEDEON-2 gadolinium pin where the main source of uncertainty is the experimental uncertainty ( $>10\%$ ).

c. Calculation to experiment comparison

The whole calculation/experiment ratios are shown in **Erreur ! Source du renvoi introuvable.**, Figure 5, and Figure 6. Uncertainties are given at  $1\sigma$ . Measurements of gadolinium isotopes concentration are expressed relatively to the total gadolinium concentration in case of GEDEON-1, or relatively to the  $^{160}\text{Gd}$  isotope concentration in case of GEDEON-2, and then cannot be normalized to  $^{238}\text{U}$  isotope as all the other isotope ratios. Even if  $^{160}\text{Gd}$  and  $\text{Gd}_{\text{tot}}$  concentrations are not significantly varying during irradiation (of about 1% according to calculations), these normalizations might introduced some bias if the corresponding concentrations are not precisely known.

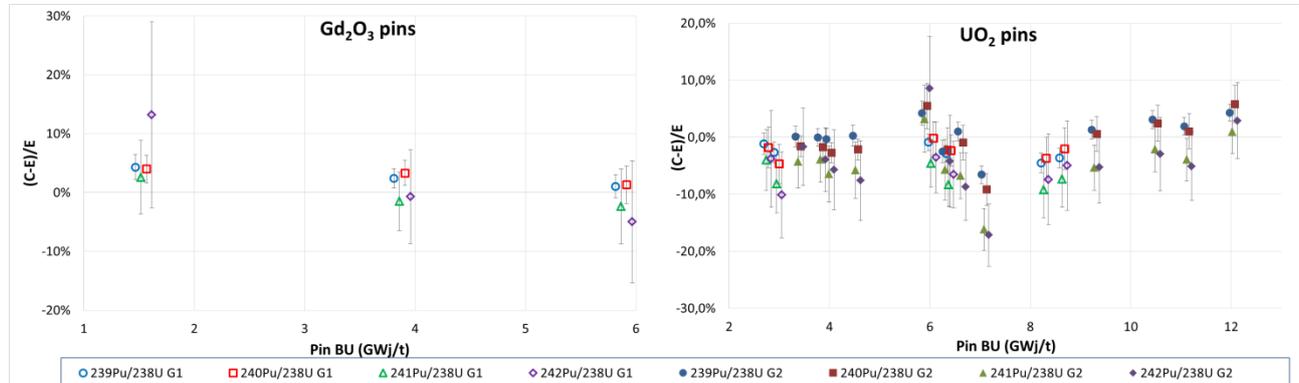


**Figure 4. Uranium isotopes calculation/experiment relative ratio for GEDEON-1 (G1) and GEDEON-2 (G2)**

$^{235}\text{U}$  isotope is well reproduced by calculation.

$^{234}\text{U}$  isotope, which is well reproduced by calculation for GEDEON-1, is overestimated by about  $4\% \pm 1\%$  in case of GEDEON-2  $\text{UO}_2$  pins and underestimated by about  $20\% \pm 20\%$  for GEDEON-2 gadolinium pins. Nevertheless the observed overestimation in  $\text{UO}_2$  pins is consistent with some UOX fuel analyses from the DARWIN experimental validation report [8], and is probably due to lack of knowledge of the exact initial concentration. Indeed, the experimental validation report shows that in the case of well-known initial conditions, this isotope is well reproduced. For the gadolinium pin, the significant calculation/experiment ratio uncertainty is due to the 10% to 30% experimental uncertainty on  $^{234}\text{U}$  relative concentration.

$^{236}\text{U}$  isotope from GEDEON-2 pins seems to be underestimated especially as the burnup is low ( $7\% \pm 2\%$  for  $\text{UO}_2$  pin, up to  $73\% \pm 3\%$  for gadolinium pin), which may be due to an underestimation of  $^{235}\text{U}$  neutron capture rate. Since DARWIN experimental validation report shows that  $^{236}\text{U}$  is well estimated thanks to the reevaluation of  $^{235}\text{U}$  capture cross section in JEFF3.1.1, a  $^{235}\text{U}$  neutron capture rate underestimation might be linked to neutron flux calculation. Another reason may also be, as for  $^{234}\text{U}$ , a lack of knowledge of the exact initial concentration.

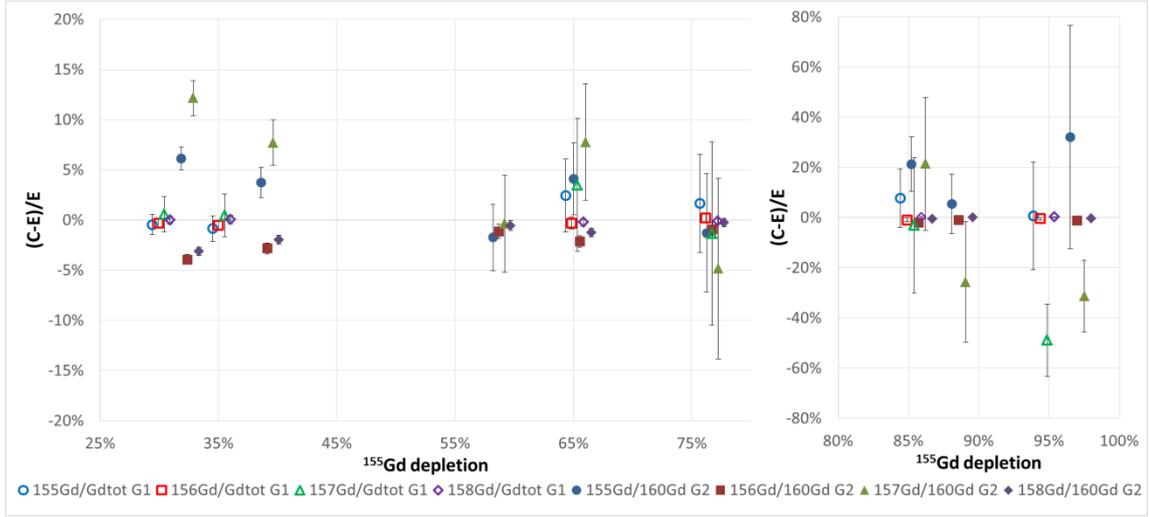


**Figure 5. Plutonium isotopes calculation/experiment relative ratios for GEDEON-1 (G1) and GEDEON-2 (G2)**

No plutonium isotopes measurements have been performed in gadolinium pins from GEDEON-2. On the opposite of the  $\text{UO}_2$  pins, plutonium isotopes are overestimated by about  $4\% \pm 2\%$  in GEDEON-1 gadolinium pins. This overestimation may be caused by the definition of a too high temperature in the gadolinium pins (decreasing the effective temperature in the fuel induces plutonium overestimation reduction) [2]. This is indeed consistent with the observed decreasing of the plutonium overestimation for highest burnup (gadolinium depletion results in an increasing of the fission rate and then then of the temperature). Plutonium isotopes are mostly underestimated in  $\text{UO}_2$  pins, especially for the highest atomic numbers.

$^{239}\text{Pu}$  and  $^{240}\text{Pu}$ , underestimated between 2% and 4% in case of GEDEON-1, are well estimated in the case of GEDEON-2 except for pin BU of about 6, 7 and 12  $\text{GWj/t}$ . For the first BU value, which corresponds to a monitor pin, the discrepancy between calculations and measurements might be due to BU calibration based on  $^{235}\text{U}$  concentration since no neodymium measurements were available. The two other BU values correspond to pins adjacent to gadolinium. These discrepancies between measurement and calculation are consistent with discrepancies on neodymium isotopes from those same adjacent pins (overestimation of about 3%). While assembly burnup seems to be well calibrated from monitor pin neodymium isotopes, it appears that calculations do not correctly reproduce the burnup in the adjacent pin in the case of GEDEON-2.  $^{241}\text{Pu}$  and  $^{242}\text{Pu}$  isotopes are mostly underestimated (between 5% and 10%). Nevertheless, due to their strong sensitivities to burnup calibration, the calculation/experiment ratio uncertainty is also high (of about 5% and 7% respectively for  $^{241}\text{Pu}$  and  $^{242}\text{Pu}$ ).

As for the main absorbing gadolinium isotopes,  $^{155}\text{Gd}$  and  $^{157}\text{Gd}$ , calculations are consistent with measurement for GEDEON-1 first cycle. The even gadolinium isotopes are well estimated for all GEDEON-1 cycles, as for the three last cycles of GEDEON-2. For the latter, an underestimation of about 2% to 4% of  $^{156}\text{Gd}$  and  $^{158}\text{Gd}$  concentrations is observed for the first cycle. This is consistent with overestimation of  $^{155}\text{Gd}$  and  $^{157}\text{Gd}$  isotopes concentrations, and probably due to an underestimation of the thermal neutron flux at the gadolinium pin. The latter might be due to the 2D calculation which does not take into account control rods insertion close to the assembly at beginning of irradiation [3]. For the highest burnup, significant discrepancies between calculation and experiment are observed for odd gadolinium isotopes, but with significant uncertainties (up to 45%). Nevertheless, one can notice that for both experiments, GEDEON-1 and -2, the uncertainty on the calculation/experiment ratio for  $^{157}\text{Gd}$  isotope is too low to explain the full observed discrepancy.



**Figure 6. Main gadolinium isotopes calculation/experiment relative ratios for GEDEON-1 (G1) and GEDEON-2 (G2)**

However, the latter are associated to very small amount of  $^{155}\text{Gd}$  and  $^{157}\text{Gd}$  gadolinium isotopes. As the latter becoming smaller and smaller during irradiation, a calculation/experiment ratio is calculated on the relative depletion of these isotopes. The same parameter is also calculated for even isotopes ( $^{156}\text{Gd}$  and  $^{158}\text{Gd}$ ). The calculated depletion ( $D_c$ ), for the burnup BU, and for the isotope X is expressed as shown in equation:

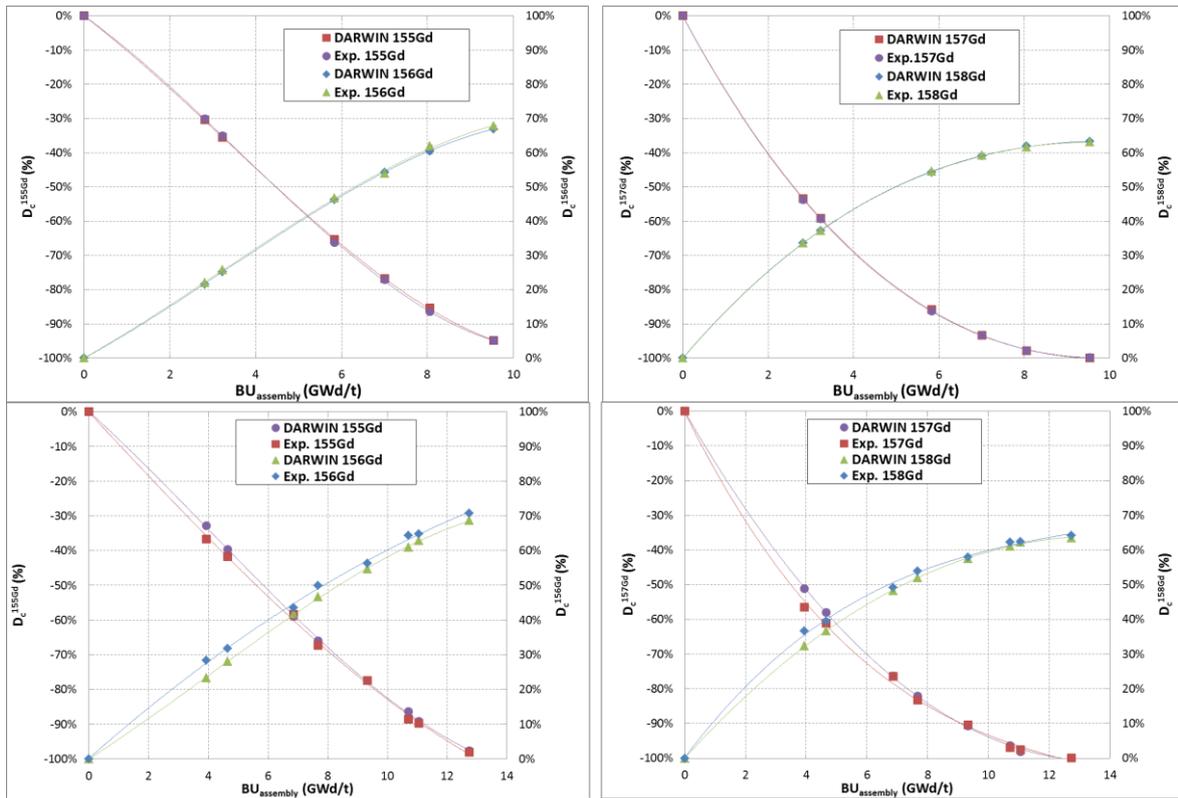
$$D_c^{XGd}(BU) = \frac{C^{XGd}(BU) - C^{XGd}(0)}{C^{XGd}(0)} \quad (2)$$

As the experimental gadolinium depletion was not measured, then experimental relative concentration at the burnup (BU) has been normalized using equation (3), A being Gd<sub>tot</sub> or  $^{160}\text{Gd}$  for GEDEON-1 and GEDEON-2 respectively.

$$D_E^{XGd}(BU) = \frac{\frac{E^{XGd}(BU)}{E^A(BU)} \times \frac{C^A(BU)}{C^A(0)} - \frac{E^{XGd}(0)}{E^A(0)}}{\frac{E^{XGd}(0)}{E^A(0)}} \quad (3)$$

$D_c^{XGd}$  and  $D_E^{XGd}$ , for  $^{155}\text{Gd}$ ,  $^{156}\text{Gd}$ ,  $^{157}\text{Gd}$  and  $^{158}\text{Gd}$  isotopes, are represented in Figure 7, as a function of the assembly burnup.

In case of GEDEON-1, gadolinium depletion is quite well reproduced. In case of GEDEON-2 calculation, depletion of odd isotopes is well estimated, except a highest underestimation for the lowest burnup. Depletion is not very sensitive to capture cross sections ( $\approx 0.1\%$  / %), this underestimation of the capture rate indicates a possible underestimation of the thermal flux near gadolinium pins at the beginning of irradiation. The latter is consistent with the underestimation of gadolinium even isotope production. For highest burnup, except for the  $^{156}\text{Gd}$  depletion underestimate about 2%, calculations are in agreement with experiment.



**Figure 7. Calculated and measurement depletion/production of main gadolinium isotopes ( $^{155}\text{Gd}$ ,  $^{156}\text{Gd}$ ,  $^{157}\text{Gd}$  and  $^{158}\text{Gd}$ ), in %, as a function of the assembly burnup (GEDEON-1 on top and GEDEON-2 at the bottom).**

All the results presented in this paper are consistent with previous GEDEON-1 and GEDEON-2 interpretation using APOLLO2.8/JEFF3.1.1 [2] [3].

## 5. CONCLUSION

This paper summarizes the interpretation of GEDEON-1 and GEDEON-2 experiment for gadolinium depletion experimental validation of DARWIN2.3 package. Analyses are performed from a  $13 \times 13$   $\text{UO}_2$  assembly containing several gadolinium pins, irradiated in the MELUSINE reactor. At several burnup steps, three pins (one central  $\text{UO}_2$  for burnup calibration, one  $\text{UO}_2$  adjacent to a gadolinium pin and one gadolinium pin) are removed and chemically analyzed. For almost each analyzed pin, two samples are collected (at mid-height and at the bottom of the pin). Isotopes concentrations are expressed relatively to  $^{238}\text{U}$  concentration, except gadolinium isotopes which are normalized to the total gadolinium for GEDEON-1 and  $^{160}\text{Gd}$  for GEDEON-2.

Calculations are performed using DARWIN2.3 package. As the flux in the MTR buffer zone of the MELUSINE core needs to be precisely estimated, a two steps calculation scheme is used:

- JEFF-3.1.1 nuclear data.
- Neutron calculation using APOLLO2.8-4 with two steps calculation,  $P_{ij}$  flux and self-shielded cross section calculation followed by method of characteristics (MOC) flux calculation, using a 281 group energy mesh,
- Depletion calculation using DARWIN/PEPIN2.4.2,

Uranium isotopes calculations are globally consistent with experiments, the main discrepancies probably coming from lack of knowledge of the precise initial concentration, as well as maybe some underestimation of  $^{235}\text{U}$  capture rate at the beginning of the irradiation. Plutonium isotopes are mostly underestimated by calculation as much as their atomic number is high. For the GEDEON-2 experiment, discrepancies are observed for main plutonium isotopes in adjacent  $\text{UO}_2$  pins, which is most likely due to incorrect local burnup calculations, as the same discrepancies are observed on neodymium isotopes. The power profile in the GEDEON-2 assembly may not be correctly calculated. In case of gadolinium pins, the more significant

discrepancy observed between calculation and experiment of plutonium isotopes probably come from the use of too high temperature in those pins. For burnup close to the lowest burnup from DARWIN2.3 experimental validation report (last GEDEON cycle), uranium and plutonium calculation/experiment ratio are consistent with value from the report [8].

Globally, even gadolinium isotopes are well calculated, except for the first cycle of GEDEON-2 where the overestimation of odd isotopes reflecting an underestimation of gadolinium capture rate and then of even isotopes production. The significant reduction of  $^{155}\text{Gd}$  and  $^{157}\text{Gd}$  isotopes concentration during irradiation, and their sensitivity to the burnup, leads to focus on the depletion of those isotopes.

This work shows the reasonable performances of DARWIN2.3 for gadolinium depletion calculation, except the first cycle of GEDEON-2 first cycle, showing an underestimation of odd gadolinium isotopes depletion (associated with an underestimation of corresponding even isotopes production), probably due to underestimation of thermal neutron flux at gadolinium pin. The mean calculation/experiment depletion ratio of  $^{155}\text{Gd}$  and  $^{157}\text{Gd}$  is about  $-0.1\% \pm 1.4\%$  and  $-0.2 \pm 0.5\%$  in case of GEDEON-1, and  $-1.3\% \pm 1.5\%$  and  $-1.1 \pm 2.1\%$  in case of GEDEON-2.

For this interpretation using DARWIN2.3, the CYCLE2008-REP scheme has been adapted to take into account the MELUSINE axial heterogeneity. It may be interesting to consider future interpretation from PWR gadolinium pin at low burnup. The latter may allow the use of the PWR CYCLE2008-REP scheme from DARWIN2.3 package on a pin representative of those usually used in PWR (8-10% Gd and 2-3%  $^{235}\text{U}$  enrichment) confirming the results from GEDEON-1 (5% Gd and 3.25%  $^{235}\text{U}$  enrichment) and GEDEON-2 (8% Gd and 0.2%  $^{235}\text{U}$  enrichment). Such pin should be measured by SCK-CEN research center in the frame on international collaboration called REGAL (**R**od-**E**xtremity and **G**adolinia **A**na**L**ysis).

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