

Feasibility study of fissile mass detection in 870 L radioactive waste drums using delayed gamma rays from neutron-induced fission

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1	Feasibility study of fissile mass detection in 870 L
2	radioactive waste drums using delayed gamma rays
3	from neutron-induced fission
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10 Abstract

The measurement of delayed gamma rays following neutron-induced fission is simulated with MCNP 6.1 to investigate the feasibility of fissile material detection in long-lived, medium activity radioactive waste in 870 L. The signal from homogeneously distributed fissile material in the drum is several hundred counts in the main delayed gamma peaks of interest. In a peripheral position or in the drum center, the signal is however too small to allow for a reliable measurement.

17 Keywords

18 Delayed gamma, neutron induced fission, long-lived medium activity waste, 870 L19 radioactive waste drum, MCNP

20

22 Introduction

23 Since the end of the '80s, CEA has produced large volume 870 L radioactive waste 24 drums [1] that are stored in Cadarache, France. These legacy drums are filled with wafers 25 corresponding to smaller compacted drums. The fissile mass within the drums needs to be 26 known in order to limit criticality risks during transport, interim storage and in the final 27 repository for which the maximum accepted fissile mass is of the order of 200 g. In 28 practice, only tens of grams of fissile mass are really expected to be present in these 29 drums [2]. The goal of the work presented in this paper is to test the preliminary detectability of some tens of grams of ²³⁵U or ²³⁹Pu with three different distributions in 30 31 the 870 L drum by neutron-induced fission delayed gamma rays measurement.

The delayed gamma rays of interest emitted by the fission products of ²³⁵U and ²³⁹Pu 32 have been identified in previous work mainly presented in [2] and [13]. We select six of 33 34 these delayed gamma rays for this feasibility study. These delayed gamma rays and their 35 respective fission product and half-life based on LARA nuclear database [3] are reported 36 in Tab. 1. The MCNP 6.1 Activation Control Card (ACT Card) [4] is used to simulate 37 fission delayed gamma rays. As shown in more details in the work presented in [5], the 38 ACT card correctly reproduces the order of magnitude of the experimental net counts 39 obtained by irradiating bare samples (i.e. without waste matrix) of Highly Enriched 40 Uranium (HEU) and Plutonium in REGAIN Prompt Gamma Neutron Activation 41 Analysis (PGNAA) cell of the Nuclear Measurement Laboratory of CEA Cadarache, 42 France. REGAIN was made of graphite walls, a pulsed DT neutron generator and a 33 % 43 HPGe (high purity germanium) detector.

As REGAIN is today dismantled and was only able to accept 120 L waste drums, we decided to perform this feasibility study of fission delayed gamma-ray detectability in 870 L legacy waste drums with the MCNP model of another PGNAA cell called MEDINA (Multi Element Detection based on Instrumental Neutron Activation), located at FZJ in Jülich, Germany. With this MEDINA model, we already studied the detection of neutron-induced fission delayed gamma rays in 225 L waste drums as reported in [6], without the ACT card. In [6], calculation was split in two steps: (1) fission rate followed

51 by (2) detection of fission delayed gamma rays. In the present study, the ACT card allows 52 simplifying calculation by directly obtaining the fission delayed photon flux at the 53 entrance of the HPGe detector. For the present work, the MCNP model of MEDINA was 54 adapted to accept 870 L drums. The time vs. energy output data from the MCNP 55 calculations (F5:P tally, i.e. photon flux at the detector position) was then processed with 56 MODAR Software (MCNP Output Data Analysis with Root) [7]. This last allows a 57 temporal analysis of gamma rays of interest and the convolution of the photon flux 58 spectra with the response function of a HPGe detector.

γ ray energy	885 keV	1011 keV	1384 keV	1436 keV	1768 keV	2218 keV
Fission fragment	¹⁰⁴ Tc	101 Mo	⁹² Sr	¹³⁸ Cs	¹³⁸ Xe	¹³⁸ Cs
Half-life T _{1/2}	18.3 min	14.6 min	2.65 h	33.4 min	14.1 min	33.4 min

Table 1. Main delayed gamma rays emitted by ²³⁵U and ²³⁹Pu fission fragments for this
 study.

61 Validation of the use of MCNP 6.1 Activation Control Card

62 The study presented in details in [5] consisted in confronting experimental results 63 obtained with REGAIN graphite cell with simulated results. Some of the experiments led 64 during the campaign presented in [6] consisted of interrogating a metallic Highly 65 Enriched Uranium (HEU) or plutonium bare sample of some tens of grams by 14 MeV neutrons emitted by a GENIE 16 neutron generator of 8.10^7 s⁻¹ average intensity 66 67 thermalized in the cell. The HEU and plutonium samples were irradiated for 2 h and were 68 then moved to a low-background spectrometer where the delayed gamma rays were 69 measured with a 25 % relative efficiency HPGe, with sequential spectra acquisitions 70 every 15 min, for a global 24-h measurement time. In the low-background cell, a thin 3 71 mm lead shield was placed between the fissile materials metallic samples and the HPGe detector in order to limit the signal from the low energy gamma rays of ²⁴¹Am. The 24-h 72 73 measurements have been simulated using the models described in [5], taking into account 74 the transfer of the bare samples from REGAIN cell to the low-background cell (1-min transfer). The time chronogram of these experiments is presented in Fig. 1. 75

All gamma rays from activation of non-nuclear materials in the cell were not calculated by using the option NONFISSION=NONE of ACT Card, thus simulating the lowbackground cell conditions. The delayed gamma rays calculated with MCNP 6.1 ACT card were studied by analyzing the decay time of non-nuclear activated elements and fission fragments as detailed in [5]. The simulated net counts are calculated for the first 15 min after the end of irradiation by applying the formula in Eq. (1):

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$$MCNP_{counts}(E) = \int_{t_2}^{t_3} (\int_{E'} F5_{ACT}(E',t) \times RF_{HPGe33\%}(E',E)dE') dt. T_{irrad} \cdot E_n$$
 (1)

83 where $t_2 = 1$ min is the time transfer from REGAIN to the low-background spectrometer 84 and $t_3 = 16 \text{ min}$; $F5_{ACT}(E',t)$ corresponds to the point photon flux obtained at the entrance 85 of the HPGe detector; The response function $RF_{HPGe33\%}(E',E)$ corresponds to the 86 probability that a photon with energy E' leads to an energy deposit E in the gamma-ray 87 HPGe detector of 33% relative efficiency; T_{irrad} (s) is the full irradiation time of 2 hours; E_n (n.s⁻¹) is the 8.10⁷ n.s⁻¹ average neutron emission of the GENIE 16 neutron generator 88 89 during irradiation. In addition, as MODAR response function corresponds to a 33 % 90 HPGe, we have also calculated the efficiency of the 25 % HPGe used in the low-91 background spectrometer and we have applied the correction reported in Tab. 2 for each 92 delayed gamma ray. The respective full energy peaks efficiencies are calculated with an 93 isotropic mono-energetic photon point source placed 12.5 cm from both 25 % and 33 % 94 relative efficiency HPGe detectors (like in REGAIN experiment) and a F8:P energy 95 deposition tally in the volume of the respective germanium crystal cells presented in Fig. 96 2.

97 In the MCNP net simulated counts in Tab. 3 only statistical uncertainties linked to each 98 computation are reported. Indeed, these numerical simulations have been performed with 5×10^9 source neutrons, which corresponds to a relative statistical uncertainty on each 99 100 gamma ray present in the F5:P photon flux tally between 1 % and 3 %. However, this 101 figure does not represent the total MCNP calculation uncertainty. Indeed, the uncertainty 102 associated to the fine geometrical description of nuclear material metallic HEU and Pu 103 bare samples in the numerical model might be significant as self-shielding is large in 104 these samples, and extremely geometry-dependent. Calculated self-shielding factors

105 reported in ref. [6] are 3.8 and 5.7 in the HEU and Pu samples, respectively, but ref. [6] 106 also reports that calculation underestimates the measured fission rates by 55 % and 37 %. 107 respectively. This is probably due to discrepancies between the models and the real 108 geometry of these samples. Indeed, the geometry of the metallic fissile core of these old 109 samples manufactured in the '60s is not known with a good precision and only their outer 110 dimensions (of the zirconium alloy envelope) and masses are well known. In addition, the 111 uncertainties on nuclear data, in particular on fission products yields (leading to delayed 112 gamma ray emissions) are not taken into account. Concerning experimental results 113 reported in Tab. 3, the standard deviation on the net peak area S (number of counts) of a 114 delayed gamma ray is calculated with Eq. 2 (following Poisson law).

115
$$\sigma = \sqrt{S + 2B} \quad (2)$$

116 where B is the Compton continuum background under the peak (number of counts). For 117 the main experimental results σ corresponds to an experimental relative uncertainty of 118 about 10 %, which is much smaller than the uncertainties related to self-shielding which 119 are described above. Calculations and measurements being of the same order of 120 magnitude is however encouraging enough to allow further numerical exploratory 121 investigations using MCNP 6.1 ACT card. Consequently, we will use this delayed 122 gamma-ray calculations method based on MCNP ACT card to study the feasibility of the 123 870 L drum characterization by the measurement of delayed gamma rays from neutron-124 induced fission.



Fig 1: Time chronogram related to the HEU/Pu samples irradiation in REGAIN and
 delayed gamma measurement in the low-background spectrometer



130 Fig. 2 MCNP models of the 33 % and 25 % relative efficiencies HPGe detectors with

131 their respective germanium crystals (red) and aluminum envelopes (blue). Note that the

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XZ and XY views are not at the same scale.

γ ray energy	885 keV	1011 keV	1384 keV	1436 keV	1768 keV	2218 keV
Efficiency for a HPGe 25%	1.471x10 ⁻³	1.334x10 ⁻³	1.014x10 ⁻³	0.982x10 ⁻³	0.820x10 ⁻³	6.582x10 ⁻⁴
Efficiency for a HPGe 33%	1.875x10 ⁻³	1.686x10 ⁻³	1.317x10 ⁻³	1.277x10 ⁻³	1.054x10 ⁻³	0.880x10 ⁻³
Correction factor	0.784	0.791	0.770	0.769	0.778	0.748

133 Table 2. Detection efficiencies of the 33 % and 25 % HPGe detectors calculated with

MCNP (see models in Fig. 2) for a gamma point source located at 12.5 cm from the
detector entrance surfaces as in the experiment.

γ ray energy	885 keV	1011 keV	1384 keV	1436 keV	1768 keV	2218 keV
Experimental						
net counts	790 ± 67	918 ± 98	612 ± 40	1211 ± 54	172 ± 25	102 ± 24
with U						
MCNP 6.1						
net counts	648 ± 8	744 ± 23	597 ± 10	877 ± 12	183 ± 4	130 ± 3
with U						
Experimental	1464 +					
net counts	1404 -	760 ± 66	347 ± 36	1057 ± 48	102 ± 29	198 ± 37
with Pu	100					
MCNP 6.1						
net counts	873 ± 6	552 ± 14	238 ± 3	567 ± 4	118 ± 2	85 ± 1
with Pu						

Table 3 Simulated net counts vs. experimental net counts of the main delayed gamma
rays of interest from HEU and plutonium samples after a 15-min measurement following
a 2-h irradiation in the REGAIN neutron interrogation cell.

140 MCNP model of the measurement cell for the 870 L drums

141 The graphite cell used for this study is based on an existing MCNP model of the 142 MEDINA facility of the Forschungszentrum Jülich (FZJ) described in [6] [8] [9]. As 143 MEDINA was built with the aim of detecting toxic chemicals in up to 225 L drums the 144 model of this MEDINA cell has been slightly modified by enlarging the interrogation 145 cavity to accept the 870 L waste drum. A graphite block has also been added in the 146 bottom of the cell to limit neutron leakages to the ground. In the same way, the graphite 147 roof of the cell has been enlarged to limit neutron leakage in the top corners of the cell 148 and thus improve the thermal neutron flux and hence fissile mass interrogation. The new 149 model of the cell named MEDINA 2 is presented in Fig. 3.

As MEDINA cell, MEDINA 2 is modelled with high purity graphite blocks allowing the 14 MeV fast neutron thermalisation. The composition of this graphite blocks used for this model is reported in Tab. 4. An isotropic 14 MeV neutron point source is simulated with a 10^{10} s⁻¹ intensity (corresponding to a GENIE 35 neutron generator of SODERN). Note that the original 104 % relative efficiency HPGe of MEDINA is replaced by a 33 % HPGe, the response function of this detector being available in MODAR for time-energy investigations. For the first study, 10 g of 235 U or 239 Pu were simulated with a

homogenous distribution in the five compacted drums filling the 870 L drum, meaning 2 g per wafer. The detailed description of the 870 L drum geometry and materials is given in [2]. For the second and third case studies corresponding to heterogeneous fissile materials, two metallic 10 g 235 U and 239 Pu spheres (radius ≈ 0.5 cm) were simulated at the edge and in the center of the third wafer. Spheric shapes are chosen as simplification, in order to avoid anistropic self-attenuation effects within the sample.

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Fig. 3. 3D view (left), horizontal cross section (middle) and vertical cross section (right)
 of the MEDINA 2 graphite cell with a 870 L drum.

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Element	% Weight	Element	% Weight	Element	% Weight
¹² C	99.913	$^{1}\mathrm{H}$	$4.05 imes 10^{-3}$	⁴⁶ Ti	$3.28 imes 10^{-4}$
⁴⁰ Ca	1.09×10^{-2}	⁵⁴ Fe	2.93 x 10 ⁻⁴	⁴⁷ Ti	$2.99 imes 10^{-4}$
⁴² Ca	1.27×10^{-4}	⁵⁶ Fe	4.59 x 10 ⁻³	⁴⁸ Ti	$3.03 imes 10^{-4}$
⁴³ Ca	2.73×10^{-5}	⁵⁷ Fe	1.10×10^{-4}	⁴⁹ Ti	2.26×10^{4}
⁴⁴ Ca	$5.58 imes 10^{-4}$	⁵⁸ Fe	$1.40 imes 10^{-5}$	⁵⁰ Ti	2.21×10^{-4}
⁴⁸ Ca	$3.71 imes 10^{-4}$	³⁵ Cl	$1.52 imes 10^{-4}$	$^{10}\mathrm{B}$	$3.70 imes 10^{-5}$
³² P	$1.09 imes 10^{-2}$	³⁷ Cl	4.87×10^{-5}	¹¹ B	$1.49\times10^{\text{-4}}$
³³ P	8.63×10^{-5}	⁵¹ V	$3.50 imes 10^{-4}$		
³⁴ P	$4.84\times10^{\text{-4}}$	²⁷ Al	$4.05 imes 10^{-2}$		



Table 4: Graphite blocks composition for the model of the MEDINA2 measurement cellfor the 870 L drums

176 MCNP calculations for a homogeneous distribution of fissile materials

177 The delayed gamma ray spectra emitted by 10 g of fissile masses homogenously distributed in the five compacted drums are shown in Fig. 4 for both ²³⁵U and ²³⁹Pu. The 178 179 main high energy delayed gamma rays of interest from uranium and plutonium (reported 180 in Tab. 1) are present in both spectra. With the aim of being closer to realistic practical 181 measurement of these drums, the net number of counts in these peaks has been simulated 182 for a 3-h acquisition time following the end of the 2-h irradiation, see Tab. 5. The MCNP net number of counts for this study are calculated following Eq. (1) with $t_2 = 1$ min and 183 184 $t_3 = 3$ hours.

Tab. 5 reports statistical uncertainties on the net peak area (number of counts S aftersubtraction of the Compton continuum background B in the HPGe gamma spectrum

187 simulated with MCNP) of the delayed gamma rays of interest, calculated following Eq.188 (2).

189 In addition, in order to calculate detection limits, the active background spectrum 190 corresponding to the activation of the 870 L waste package materials with the 191 NONFISSION = P option of the ACT card has been calculated. The same conditions as 192 for the fission delayed gamma ray useful signal have been used (neutron generator 193 emission, irradiation and counting time). The calculated activation background spectrum 194 reported in Fig. 5 shows no interference between delayed gamma rays of interest for this 195 study and activation gamma rays from the 870 L waste drum. However, the useful signal 196 spectrum of fission delayed gamma rays is 1 to 2 orders of magnitude smaller than the 197 active background spectrum (see Fig. 4 vs. Fig. 5, respectively). Detection Limits (DL in 198 counts) are calculated following Eq. (3), which corresponds to a non-detection risk and a false-alarm risk α =2.5 % and β =2.5 %, respectively [10]: 199

200
$$DL(E) \approx 3.92.\sqrt{2.B_{active background}(E)}$$
 (3)

where $B_{active \ background}$ (*E*) corresponds to Compton continuum (counts) of the active background spectrum evaluated in the region of interest of each fission delayed gamma ray (energy E), the width of which is between 7 and 8 keV depending on the peak. DL is then divided by the useful signal sensitivity, noted $S_{U/Pu}$ (in g⁻¹), which corresponds to the net counts reported in Tab. 5 per fissile mass unit (U or Pu). The number of counts for the 870 L drum active background continuum and the detection limits in grams for a fissile mass homogeneous distribution in the 5 wafers of the 870 L drum are reported in Tab. 6.

For this 2-h irradiation and 3-h measurement, depending on the delayed gamma ray of interest, detection limits vary between 31.6 g and 123.4 g of ²³⁵U, or between 24.1 g and 109.7 g of ²³⁹Pu homogeneously distributed in the drum.

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γ ray energy	885 keV	1011 keV	1384 keV	1436 keV	1768 keV	2218 keV
Net area for ²³⁵ U (counts)	397 ± 24	265 ± 19	308 ± 22	395 ± 23	83 ± 11	90 ± 12
Net area for ²³⁹ Pu (counts)	656 ± 39	412 ± 33	280 ± 23	524 ± 26	90 ± 11	102 ± 11

Table 5 Net counts in the main fission delayed gamma rays calculated with MCNP for a

3-h measurement after the end of the 2-h neutron irradiation, for 10 g of ²³⁵U and ²³⁹Pu
homogeneously distributed in the 870 L drum.



Fig. 4 MCNP simulated spectra obtained for a 3-h measurement after a 2-h irradiation of
 a 870 L drum containing 10 g of homogenously distributed ²³⁵U (above) and ²³⁹Pu
 (below).



Fig. 5 Simulated active background spectra for a 3-h measurement with a HPGe of 33 %
 relative efficiency detector after a 2-h irradiation of a 870 L drum, and corresponding
 zoom sections

JRNC	

γ ray	885 keV	1011 keV	1384 keV	1436 keV	1768 keV	2218 keV
energy						
DL	1928	1882	1457	1262	987	729
(in counts)	1720	1002	1107	1202	201	129
DL in ²³⁵ U	48.2	69.7	47.0	31.6	123.4	81.0
mass (g)	10.2	0,.,	17.0	5110	12011	0110
DL in ²³⁹ Pu	29.4	45 7	52.0	24.1	109.7	71.5
mass (g)	<i>27</i> . 4	тЈ.7	52.0	∠ - T •1	107.7	/1.5

Table 6 Detection limits of ²³⁵U and ²³⁹Pu homogeneously distributed in the 870 L drum
 for each delayed gamma ray of interest.

227 MCNP calculations for a peripheral distribution of fissile materials

The second study corresponds to a 10 g sphere of ²³⁵U or ²³⁹Pu located in a peripheral 228 229 position, i.e. 1 cm from the edge of the third middle wafer. Four positions with respect to 230 neutron generator and detector have been studied: 0°, 90°, 180° and 270° as shown in Fig. 6. The results obtained for 10 g of ²³⁵U or ²³⁹Pu placed at the edge of the drum are 231 232 reported in Tab. 7 and Tab. 8, respectively. For each angle, irradiation time is 2 h. The net counts obtained for both uranium and plutonium in 0° and 270° positions are much 233 234 smaller than with a homogenous distribution, and the signal is not detectable in the 90° 235 and 180° positions. This is mainly due to neutron self-shielding and gamma self-236 absorption inside the thick nuclear material spheres (1 cm in diameter), and to 237 combined matrix-position effects leading also to large neutron and gamma attenuation in 238 the 870 L waste materials. Detection limits have also been estimated following Eq. (3) for 239 a peripheral distribution at 0° and 270° with respect to the neutron generator, and are 240 reported in Tab. 9. Detection limits are too high (dozens or hundreds of grams) to 241 envisage a practical application of the method for these drums.



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Fig. 6 XY view of MEDINA 2 cell and the 870 L drum with a 10 g fissile material sphere
 placed at the following irradiation angles with respect to neutron generator: 0°, 90°, 180°
 and 270°.

γ ray energy	885 keV	1011 keV	1384 keV	1436 keV	1768 keV	2218 keV
Net area at 0° (counts)	39 ± 11	60 ± 9	74 ± 11	64 ± 10	13 ± 5	14 ± 5
Net area at 90° (counts)	< 1	< 1	< 1	< 1	< 1	< 1
Net area at 180° (counts)	< 1	< 1	< 1	< 1	< 1	< 1
Net area at 270° (counts)	145 ± 16	115 ± 12	126 ± 14	167 ± 18	30 ± 7	31 ± 7

Table 7 Net counts for a 3-h measurement after the end of the 2-h neutron irradiation for
 the main delayed gamma rays of 10 g of ²³⁵U placed at the edge of the 870 L drum.

γ ray energy	885 keV	1011 keV	1384 keV	1436 keV	1768 keV	2218 keV
Net area at 0° (counts)	188 ± 33	77 ± 20	72 ± 11	90 ± 12	20 ± 5	22 ± 5
Net area at 90° (counts)	< 1	< 1	< 1	< 1	< 1	< 1
Net area at 180° (counts)	< 1	< 1	< 1	< 1	< 1	< 1
Net area at 270° (counts)	233 ± 25	128 ± 17	122 ± 13	161 ±14	25 ± 6	30 ± 6

Table 8 Net counts for a 3-h measurement after the end of the 2-h neutron irradiation for

250 the main delayed gamma rays of 10 g of 239 Pu placed at the edge of the 870 L drum.

251

γ ray	885 keV	1011 keV	1384 keV	1436 keV	1768 keV	2218 keV
energy						
DL in ²³⁵ U						
mass (g) at	494	313	197	197	760	520
0°						
DL in ²³⁹ Pu						
mass (g) at	102	250	202	140	494	331
0°						
DL in ²³⁵ U						
mass (g) at	133	164	115	76	329	235
270°						
DL in ²³⁹ Pu						
mass (g) at	83	147	119	78	394	243
270°						

Table 9 Detection limits (grams) of ²³⁵U and ²³⁹Pu located in the 870 L drum at 0° and
 270° with respect to the neutron generator, for each delayed gamma ray of interest.

254 MCNP calculations with fissile materials in the drum center

255 The third case study consists of fissile material placed in the drum center, in the middle 256 of the third wafer as shown in Fig. 7. The results obtained for a 2 h drum irradiation followed by a 3 h counting measurement for the ²³⁵U and ²³⁹Pu spheres are reported in 257 258 Tab. 10. In this configuration, for each high energy delayed gamma ray of interest from 259 uranium and plutonium, the net number of counts is lower than 10 and it is clear that 260 detecting 10 g of fissile masses in the center of a 870 L drum is not possible. Note that 261 detection limits have not been calculated for this section as the net counts signal from 262 delayed gamma rays of interest is hardly detectable. Indeed, the performances of the 263 method are intrinsically very poor due to the attenuation of the interrogating neutron flux

- 264 in the concrete envelope of the 870 L drum. Therefore, another method based on delayed
- 265 gamma rays induced by photo-fission with high energy X-rays (produced by a 15 MeV
- 266 electron LINAC) is also currently under study at CEA, which shows more encouraging
- results for nuclear materials detection in 870 L waste drums [2] [11] [12].



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Fig. 7 Vertical cross section of MEDINA 2 cell showing the 870 L drum with a 10 g
fissile material sphere placed in the center.

γ ray energy	885 keV	1011 keV	1384 keV	1436 keV	1768 keV	2218 keV
Net area for ²³⁵ U (counts)	3 ± 2	2 ± 1	7 ± 4	2 ± 1	2 ± 1	2 ± 1
Net area for ²³⁹ Pu (counts)	7 ± 4	5 ± 3	5 ± 3	7 ± 3	1 ± 1	2 ± 1

Table 10 Net counts in the main fission delayed gamma rays, for a 3-h measurement
 after the end of the 2-h neutron irradiation, for 10 g of ²³⁵U and ²³⁹Pu placed at the 870 L
 drum center.

274 Conclusion and prospects

This feasibility study explored the detectability of ²³⁵U or ²³⁹Pu in 870 L legacy CEA drums by means of neutron activation analysis and neutron-induced fission delayed gamma measurements. For this purpose, a graphite cell has been modeled with MCNP 6.1 and the net counts in the main delayed gamma rays of interest have been calculated

279 for different fissile masses distributions, for a 3-h measurement with an HPGe detector of 33 % relative efficiency following a 2-h irradiation with a neutron source of 10^{10} s⁻¹. 280 281 Results are encouraging for fissile materials homogeneously distributed in the waste, with detection limits between 31.6 and 123.4 grams of ²³⁵U, or between 24.1 and 109.7 grams 282 283 of ²³⁹Pu for the main high energy delayed gamma rays of interest. However, in case of 284 small samples of fissile materials located in periphery of the drum, the net counts are 285 much smaller due to both self-shielding and combined matrix-position effects and 286 detection limits are too high for a practical application to 870 L drums. Finally, if the 287 samples are located in the center of the drum, it is effectively impossible to detect any 288 delayed gamma ray of interest.

The signal could be increased by using a detector with higher efficiency, such as the 104 % HPGe detector used in MEDINA cell [6], and by implementing several HPGe detectors around the 870 L drum. The acquisition could also be performed between the pulses of the neutron generator (instead of after irradiation only) to increase the delayed gamma counting time.

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