



Laser surface texturing Numerical analysis of formation of low depth holes

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Laser surface texturing

Numerical analysis of formation of low depth holes

Morgan Dal*, Lucille Gouton

04/02/2015

Introduction

Objectives :

Texturing with pulsed fiber laser :

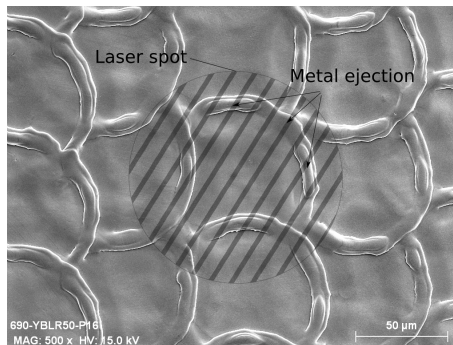


FIGURE : SEM picture of surface treated

Better **understanding** of the surface deformation under laser radiation → to have a better **control**.

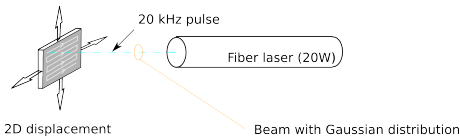
Outlines

- 1 Experimental setup
- 2 Numerical Simulation
- 3 Results
- 4 Analysis
- 5 Conclusion

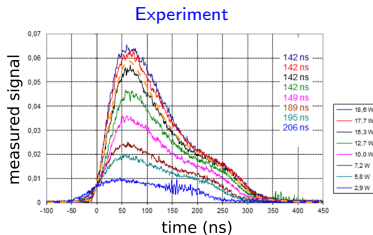
Experimental setup and parameters

Experiment :

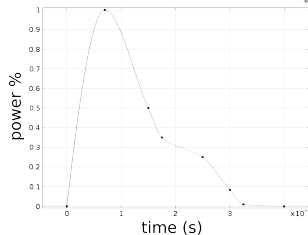
Laser multi-pulse treatment



Time distribution of one pulse :



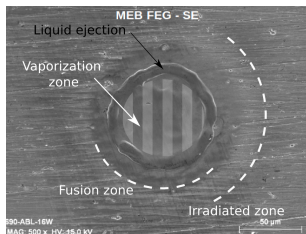
Assumption for the simulation



Experimental setup and parameters

Experiment :

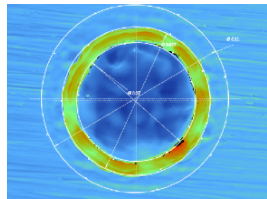
Laser one-pulse analysis



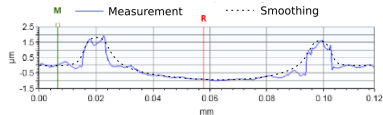
16 W mean power

Analysis

- Disturbed shape (sensor sensitivity)
- Maximum $1.5 \mu\text{m}$
- Minimum $-1 \mu\text{m}$



Bidimensionnal topology



Diameter topology

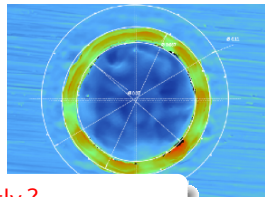
Experimental setup and parameters

Experiment :

Laser one-pulse analysis



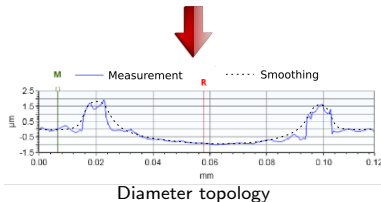
16 W mean power



What happen exactly ?

Analysis

- Disturbed shape (sensor sensitivity)
- Maximum $1.5 \mu\text{m}$
- Minimum $-1 \mu\text{m}$



Numerical Simulation

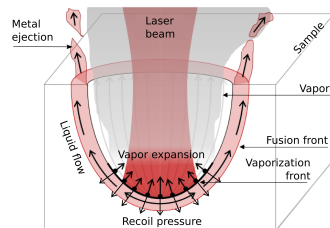
Introduction :

Why ?

- Can not measure deformation → how ?
- Can not observe → our fast cameras allow a micro second measurement
- Appropriate to understand

Knowledge

- The physical knowledge of laser welding
- The simulation of laser drilling
- Using the well known software Comsol Multiphysics®



Scheme of major phenomena
[Girardot]

Numerical Simulation

The Model :

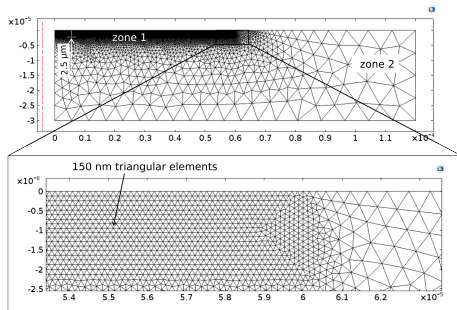
Main assumptions

- ① Bi-dimensionnal study (single spot)
- ② No gas (just the workpiece)
- ③ Heat transfer and fluid flow only

Physical assumptions

- Newtonian flow
- Thermal properties = $f(T)$
- No buoyancy
- No multiple reflexion
- Free boundary accounted with ALE method

Geometry and mesh



Geometry and Mesh

Numerical Simulation

The Model :

Heat transfers

① Heat equation

$$\rho c_p^{eq} \frac{\partial T}{\partial t} + \rho c_p \vec{V} \nabla T = \nabla \cdot (\lambda \nabla T) \quad (1)$$

② Initial condition

$$T(r, z, t = 0) = T_{\infty} \quad (2)$$

③ Boundary conditions

- at the top :

$$-\lambda \nabla T = \phi_{laser} - \phi_{cv} - \phi_{rad} - \phi_{evap} \quad (3)$$

- at the right and bottom :

$$-\lambda \nabla T = 0 \quad (4)$$

- at the left :

$$-\lambda \nabla T = 0 \quad (5)$$



Laser power distribution

$$\phi_{laser} = \alpha \frac{2P_{moy}}{\tau f} \frac{\exp(-\frac{r^2}{2r_{laser}^2})}{2\pi r_{laser}^2}$$

Heat losses

$$\phi_{cv} = h_{cv}(T - T_{\infty})$$

$$\phi_{rad} = \epsilon \sigma (T^4 - T_{\infty}^4)$$

Evaporation flux

$$\phi_{evap} = \dot{m} L_v$$

$$\dot{m} = \sqrt{\frac{M}{2\pi R}} \frac{p_{sat}}{\sqrt{T}} (1 - \beta_r)$$

Numerical Simulation

The Model :

Fluid flow

- ① Mass and momentum conservation

$$\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{V}) = 0 \quad (6)$$

$$\rho \frac{\partial \vec{V}}{\partial t} + \rho (\vec{V} \cdot \vec{\nabla}) \cdot \vec{V} = \vec{\nabla} \cdot \left[-p \mathbf{I} + \mu (\vec{\nabla} \vec{V} + (\vec{\nabla} \vec{V})^T) \right] + \vec{F} \quad (7)$$

- ② Initial condition

$$\vec{V}(r, z, t = 0) = \vec{0} \quad p(r, z, t = 0) = 1.013 \cdot 10^5 \text{ Pa} \quad (8)$$

- ③ Boundary conditions

- at the top :

$$p - \sigma_D \cdot \vec{n} = p_{rec} + \gamma \vec{\nabla}_s \vec{n} \quad (9)$$

- at the right and bottom :

$$\vec{V} = \vec{0} \quad (10)$$

- at the left :

$$\vec{V} \cdot \vec{n} = 0 \quad (11)$$

Recoil pressure

$$p_{rec} = p_0 + \frac{p_{sat}}{2} (1 + \beta_r)$$

Saturation vapor pressure

$$p_{sat} = p_0 \exp \left(\frac{ML_v}{R} \left(\frac{1}{T_{vap}} - \frac{1}{T} \right) \right)$$

Numerical Simulation

The Model :

Free boundary

ALE method

- 1 In the bulk
→ free deformation (optimize the mesh quality)

- 2 at the top

$$v_n = un_r + wn_z \quad (12)$$

- 3 at the right and left

$$d_r = 0 \quad (13)$$

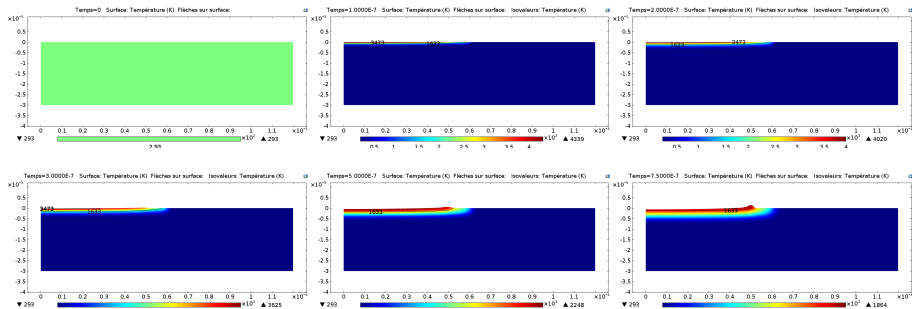
- 4 at the bottom

$$d_r = 0 \quad (14)$$



Results

The Thermal field :



Observations

- Domain sizes
- Vaporization process
- Creation of a hole shape

Questions

- Is it realistic?
- How the ring is created?
- What is the model parameter effect (T_{vap})?

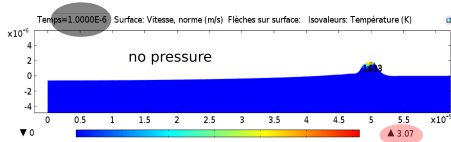
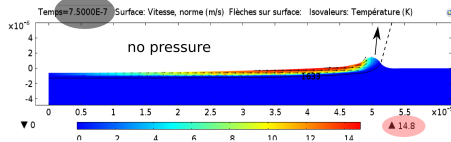
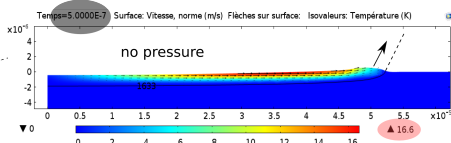
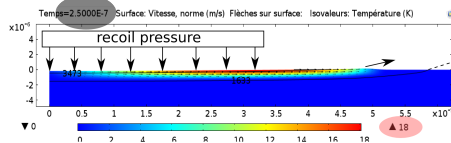
Experimental validation :

	Experiment	Simulation	
Mean power	16 W	16 W	
Depth	0.9 μm	0.6 μm	
Ring height	1.4 μm	1.8 μm	→ total deformation : 2.3 μm vs 2.4 μm
Liquid diameter	110 μm	120 μm	
Ring max diameter	90 μm	103 μm	→ also 10 μm to large

Potential reasons

- Laser power distribution ✗ (spatial and temporal measurement)
- Material absorption ✓
- Material thermal properties ✓
- Pressure calculation ?
- No gas shear stress ?

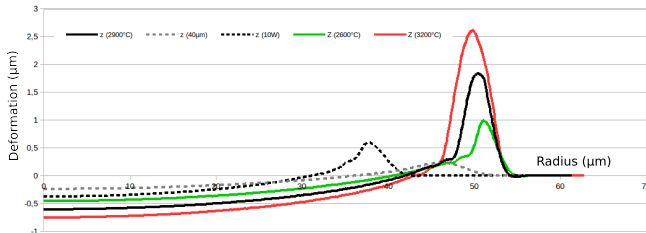
Ripple formation :



Observation :

The deformed ring is not only created by the recoil pressure (few deformation).
This particular shape is due to the inertia of the fluid coupled to the solidification.

Vaporization temperature and power effects :



Comparison

- An increase of 10% on T_{vap} → increase of 40% on positive deformation
- An increase of 10% on T_{vap} → increase of 25% on negative deformation
- T_{vap} have no effect on the ring radius
- Reducing the power to 10 W → reduction of 67% on positive deformation and 37% on negative deformation
- Ring radius decreases of 26%

Conclusion and future works

Conclusion

- Quite efficient model
- Deformation due mainly to the solidification
- Increase the laser radius avoid this effect
- Difficulties with thermal properties

Future works

- Quantify the material properties
- Compute interaction between several shots

Conclusion and future works

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Thank you for your attention !