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### BEHAVIOR UNDER LOCA CONDITIONS OF ENHANCED ACCIDENT TOLERANT CHROMIUM COATED ZIRCALOY-4 CLADDINGS

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# Cea introduction

**Cr-coated zirconium nuclear fuel cladding** developed within CEA - Areva NP- EDF collaborative program as short-term **Enhanced Accident Tolerant Fuel for LWRs (EATF):** Previous studies have shown that the developed Cr-coated claddings are characterized by:

- Excellent corrosion behavior in nominal conditions see J. Bischoff et al. this conference;
- Significant decrease of the oxidation rate with steam at HT (LOCA).





# **AIM OF PRESENT WORK**

Present work focused on <u>1<sup>st</sup> step of LOCA transient</u>, i.e., <u>internal pressure (isothermal or</u> <u>ramp) tests inducing creep/ballooning and burst</u> of the tested nuclear fuel clad segments:



Uncoated claddings appearance after ballooning and burst (« EDGAR ») testing

=> Preliminary evaluation of the <u>influence of Cr-coating on the overall clad thermo-mechanical</u> <u>behavior</u> compared to uncoated cladding by focusing on the following parameters:

- Steady-state creep rate / time to rupture
- Size of balloon and burst opening
- => Checking also the coating adhesion capacity at HT in highly deformed (ballooned) zone

## THERMAL-MECHANICAL CLAD TESTING UNDER LOCA CONDITIONS AT CEA ("EDGAR" FACILITY)

- Single(\*) Rod Tests (50cm in length)
- Steam environment, Any T&P transients
- Tmax: ~1300°C, dT/dt: up to 200°C/s,
- T gradients (axial, azimut.) < 5°C,
- Pmax: 200 Bar, dP/dt: [-10, +10] Bar/s
- \* No contact measurements:

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- T: optical pyrometers (+ internal TC)
- Continuous ext. diam. measur.: laser
- (\*) on-going multi-rod facility development





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LOCA behavior of Cr-coated Zr claddings | TOPFUEL 2016 - Boise, Idaho, USA, Sept. 11-15, 2016 | PAGE 4



## MATERIALS STUDIED AS-RECEIVED EXAMINATIONS



SRA Zircaloy-4 substrate

SEM micrograph (BSE mode) of the Cr coating thickness ⇒ No modification of
 the SRA metallurgical
 conditions of the
 substrate after the
 coating process
 *=> no modification of the As-Received clad mechanical properties*

- $\Rightarrow$  Good homogeneity
- $\Rightarrow$ **Good density**(no porosities)

⇒ No cracks within the bulk Cr nor at the Zr-Cr interface (good adhesion)

OM (polarized light) of the wall (coated) clad thickness

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## CHECKING OF THE HT STEAM OXIDATION 15 µm-THICK Cr COATING RESISTANCE

15μm-thick Cr coated clad <u>one-sided steam oxidized</u> for <u>600s at 1200°C</u> (ECR<sub>BJ</sub>~17%)



SEM (BSE mode) micrograph of the **post-HT-oxidized coating thickness** 



#### Weight % Oxygen



after oxidation for 600s at  $1200^{\circ}C$  $\Rightarrow$  High cladding PQ ductility preserved

# HT CREEP TEST RESULTS (1/2) FROM 600°C (α<sub>zr</sub> PHASE DOMAIN) UP TO 1000°C (β<sub>zr</sub> PHASE DOMAIN)



Typical creep curves obtained on uncoated & 15µm thick Cr-coated Zry-4 clad segments **at 600°C**, for an applied internal pressure of **120 bar** 

Time to rupture as a function of initial hoop stress for EDGAR (internal pressure) isothermal creep tests performed at different temperatures

Evidence of a Cr-coating HT strengthening effect => compared to uncoated Zircaloy-4:

~3 times increase of the time to rupture  $\Leftrightarrow$  ~3 times decrease of the creep rate



# HT CREEP TEST RESULTS (2/2)

Burst appearance after EDGAR creep tests:







Same observations as for isothermal creep tests:

=> good coating adherence, negligible oxidation, smaller balloon size when burst occurs in the  $a_{Zr}$  temperature range (high internal pressure applied), very small burst opening when burst occurs in the HT  $\beta_{Zr}$  temperature range (low internal pressure applied)...

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# **CONCLUSIONS AND ON-GOING/FURTHER WORK**

- 50cm long 15-µm Cr-coated Zircaloy-4 clad segments have been fabricated and then submitted to ("EDGAR") HT internal pressure creep/ramp tests;
- No modification of the underlying Zy-4 µstructure/properties induced by the Cr-coating process;
- Very good adherence of Cr-coating in both nominal & accidental conditions;
- Significantly improved behavior in LOCA conditions:
- Confirmation of the HT steam oxidation resistance;
- Reinforcement of cladding by Cr-coating observed at HT upon creep/ramp tests in the a<sub>Zr</sub> temperature range;
- In the {a<sub>Zr</sub> + β<sub>Zr</sub>} and full β<sub>Zr</sub> phase temperature ranges (~850-1000°C), even if some significant ballooning occurred prior to the cladding failure, burst openings are generally very small (=> may have positive effect in LOCA for high BU materials, by reducing the risk of fuel fragments dispersal in the coolant.)
- On-going and further work: additional creep & thermal ramp tests under internal pressure on Cr-coated materials including M5<sup>™</sup> substrate
  + further modelling

# THANK YOU FOR YOUR ATTENTION

#### Some CEA references:

[1] I. Idarraga et al., "Assessment at CEA of coated nuclear fuel cladding for LWRs with increased margins in LOCA and beyond LOCA conditions", in proceedings of 2013 LWR Fuel Performance Meeting/TopFuel, Charlotte, USA, (Sept. 15-19, 2013)

[2] J.C. Brachet, Ch. Lorrette, et al., "CEA studies on advanced nuclear fuel claddings for enhanced Accident Tolerant LWRs Fuel (LOCA and beyond LOCA conditions)", Proceedings of the 8th. Int. Symposium "Fontevraud 8" ,Avignon, France, (Sept. 14-18 2014)

[3] J.C. Brachet et al., "On-going studies at CEA on chromium coated zirconium based nuclear fuel claddings for enhanced tolerant LWRs fuel", proceedings of TopFuel 2015, Zurich, Switzerland (Sept. 13-19, 2015)

[4] J.C. Brachet et al., "Out-of-pile R&D on chromium coated nuclear fuel zirconium based claddings for enhanced accident tolerance in LWRs", proceedings of 18th Int. Symp. on Zr in Nucl. Ind.", Hilton Head, SC, USA (May 15-19, 2016)

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