

Overview of applications of the pyrochemical process developed by the CEA for the treatment of transmutation fuel targets

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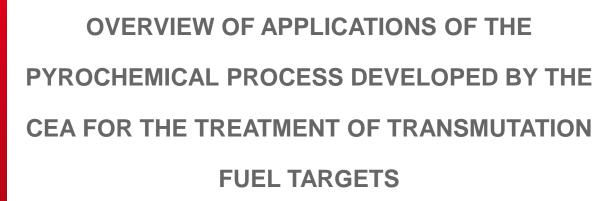
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rom research to industry

CEA Marcoule / Nuclear Energy Division, RadioChemistry & Processes Department Modelling and Separation Chemistry Service Development of Separation Processes Laboratory



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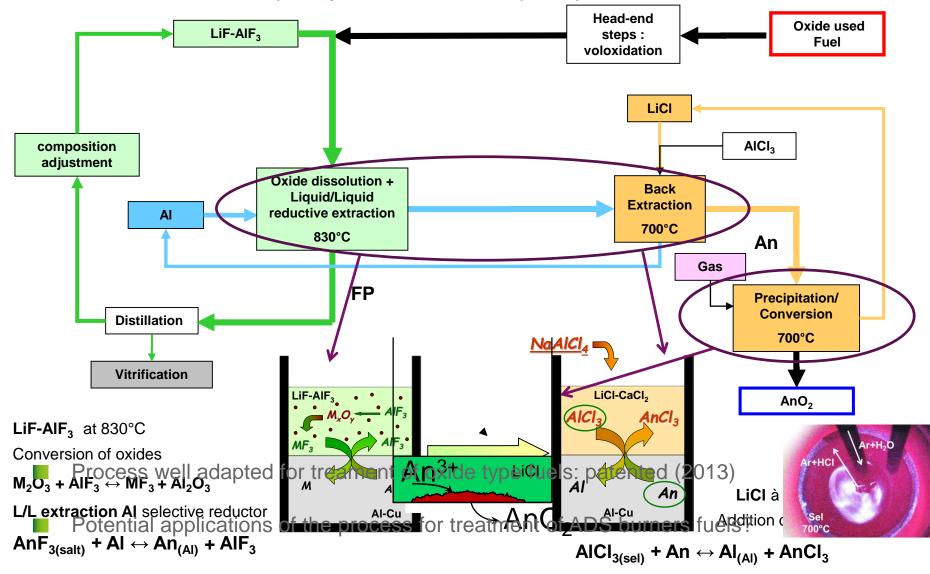
IPRC 2016 2016 International Pyroprocessing Research Conference 21-23/09/2016 - Jeju (South Korea) I Eric Mendes

SEPTEMBER 21ST – 23RD 2016

Ceaden outlines

FROM RESEARCH TO INDUSTR

Process developed by CEA: Reductive liquid/liquid extraction in fluoride media



MATERIAL TO BE REPROCESSED

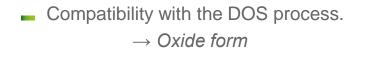
Two types of fuels considered : CERCER and CERMET

CERCER

22 den

- Ceramic matrices, e.g. oxide MgO, ZrO₂...
 - MgO suitable for ADS burners.
 - Reference Composition:

Ref.	Composition	Vol. frac. Mg
FUTURIX	(Pu _{0.5} Am _{0.5})O _{2-∂} -MgO	70%



CERMET

- Metallic matrice.
 - Mo suitable for ADS burners.
 - Composition:

Ref.	Composition	Vol. frac. Mo	Mo/MA Ratio
ITU-5	(Pu _{0.797} Am _{0.198} Np _{0.005}) O _{2-x}	86%	29,3
ITU-6	(Zr _{0.532} Pu _{0.228} Am _{0.124} Np _{0.006}) O _{2-x}	60%	6,1

■ Compatibility with the DOS process: Needs prior conversion of Mo into oxide \rightarrow MoO₂ and/or MoO₃

Assessment requirements:

- Behaviour of matrix material in the process, e.g. dissociation of oxide into the salt and behaviour regarding the reductive extraction by AI.
- **Feasibility** of the reprocessing of surrogate or genuine material
- Influence of matrix material on the extraction efficiency of MA

TREATMENT OF CERCER MATRICES

Ceade∩ Behaviour of MgO IN THE DOS PROCESS

Sintered 4h 1600°C

Open porosity <1%

Dissolution of MgO in LiF-AIF₃ at 830°C

Starting material:

MgO powder \rightarrow solubility limit Pellets \rightarrow dissolution kinetic Sintering: similar to condition as for preparation of CERCER pellets.



Open porosity <1%

Dissociation in the salt:

Mechanism:

Solubility seems to reach a limit: ~3 wt%

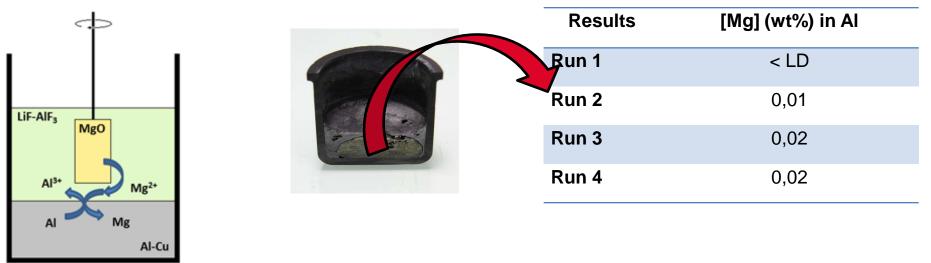
 $3MgO + 2AIF_3 \leftrightarrow 3MgF_2 + AI_2O_3$ 3,5 3,0 Kinetics: $V = \frac{dC}{dt} = kA(Cs - C)$ Concentration (% massique) 2,5 2,0 $v = 2,53.10^{-4}$ to 3,13.10⁻⁴ cm³.s⁻¹ 1.0 0,5 MgO powder LiF-AIF₃ MgO Sintered MgO pellet 0,0 Commercial MgO rod (Goodfellow) 100 200 300 400 500 0 DEN/DRCP/SCM 2016 | PAGE 5 Temps (min)

Behaviour of Mg regarding extraction

Theoretical study: Redox standard potential calculations (HSC chemistry)

AI + $3/2F_{2(g)} = AIF_3$ $\Delta_G = -1223,17 \text{ kJ.mol}^{-1} \longrightarrow \Delta E^0 = -4,23 \text{ V vs } F_2$ Mg + $F_{2(g)} = MgF_2$ $\Delta_G = -932,86 \text{ kJ.mol}^{-1} \longrightarrow \Delta E^0 = -4,83 \text{ V vs } F_2$

From thermodynamic approach : No Mg should be reduced by the metallic phase



Experiments

Good agreement with Thermodynamic approach: Al not reductive enough to reduce Mg²⁺

Ceade∩ Impact of MgO ON THE DOS PROCESS

Reprocessing of a non irradiated CERCER pellet

Unirradiated pellet prepared in ATALANTE facility within the FP6 Eurotrans framework program

Experimental conditions:



1/2

Pellet containing 200mg of Pu, 200mg of Am and 325 mg MgO Addition125mg of Nd₂O₃ (simulating FPs)

Prefusion step needed to dissolve the pellet in the salt: due to very high activity

L/L contact 4h at 830°C, sampling after contact. Pu and Am quantified by α and γ spectrometry, Nd and Mg quantification by ICP-MS

Results:

97% of Am and 99% of Pu in the metallic phase after contact (Nd < 5%, Mg < DL). Successful demonstration for reprocessing of CERCER material



Ceaden Impact of MgO ON THE DOS PROCESS

Impact of MgO accumulation in the salt: reuse of salt

- Uranium \rightarrow simulating An behaviour
- Experiments performed :

Same amount of U_3O_8 in each experiment (~500mg U)

Progressive addition of MgO in the salt from run 1 to 4: 0 - 13.5 wt%.

MgO: 3wt%. Based on used CERCER pellets, corresponds of reprocessing of 150 pellets/Kg of salt

After L/L contact samples of the two phases. U quantified by fluorescence X spectroscopy

			Uranium		
	Run	MgO wt%	Metal phase (%)	Salt phase (%)	Undissolved (%)
j	_1	0	93,6 (± 4,5)	3,3 (±1,8)	3,1 (±6,3)
	2	3	85,9 (±6,5)	1,2 (±0,5)	12,9 (±7)
	3	6	66 (±5,9)	5,8 (±3,7)	28,2 (±9,6)
	4	13,5	45,7 (±1,3)	_	_

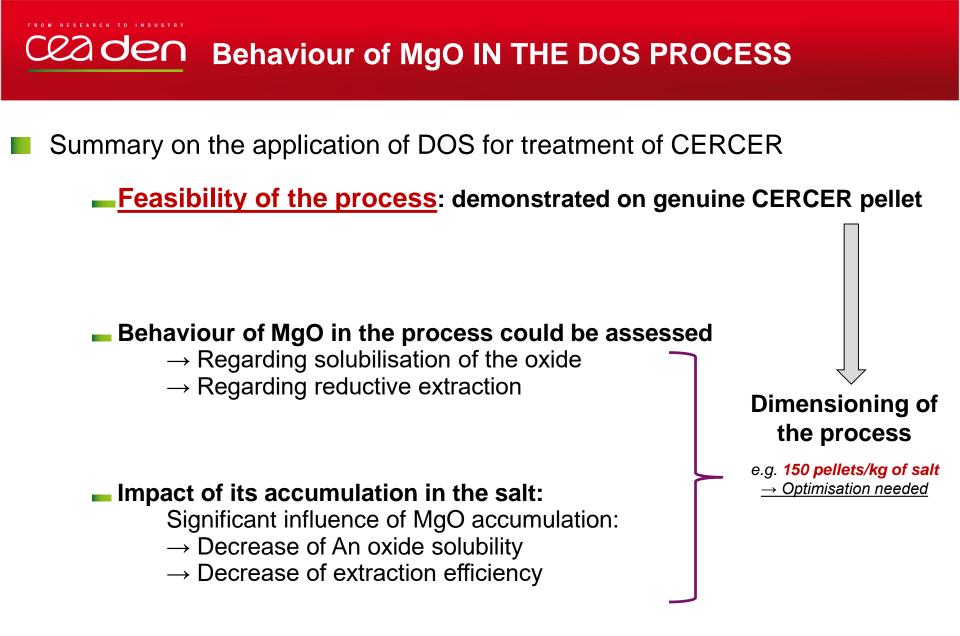
U in metal decreases when MgO increase: mainly due to U_3O_8 dissolution decrease.

 \rightarrow Solubilisation affected by excess of oxides in the salt.

Accumulation of MgO: possible change of physical properties of the salt

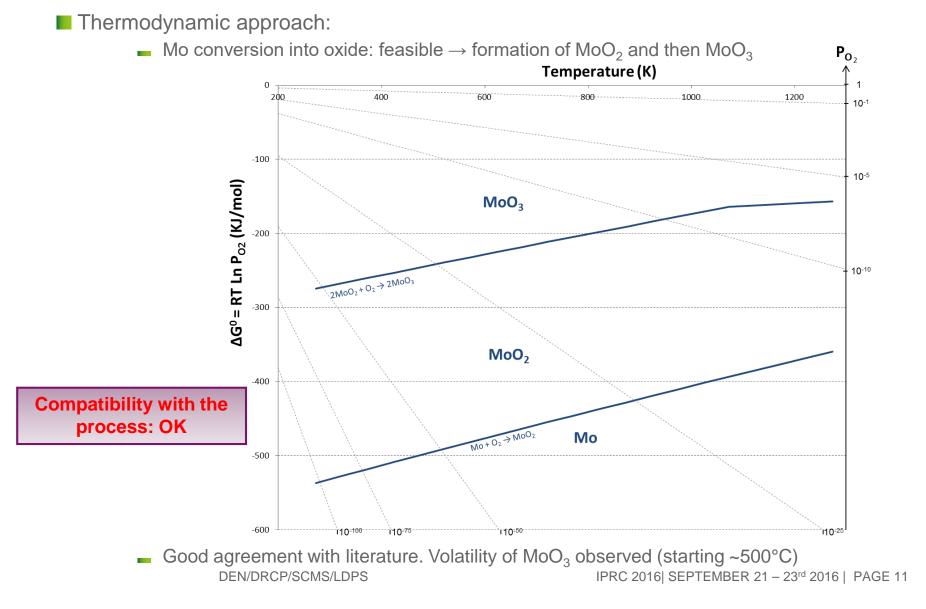
High contents of non dissolved MgO: strong decrease of extraction efficiency. \rightarrow Accumulation of oxides at the salt/met. Interface + changes of physical properties of the salt (viscosity).





TREATMENT OF CERMET MATRICES

Ceaden Mo conversion into oxide form



Ceaden solubility of mo oxide in the salt

Experiments performed on MoO_2 powder (1 - 4g) in LiF-AlF₃ (65 - 35 mol%) at 830°C first tests on MoO₃ solubility \rightarrow not possible due to high volatility of Mo(VI) 0.12 MoO₂ salt 0.1 %wt of molybdenum in the Two steps variation: 0.08 \rightarrow Increase of concentration \rightarrow Decrease of concentration 0.06 LiF-AIF 0.04 0.02 0 100 200 300 400 $\mathbf{0}$ Time (min) $\frac{3}{4}MoO_2 + AlF_3 = \frac{3}{4}MoF_4 + \frac{1}{2}Al_2O_3$ ΔG_{830°C}= -261,541 kJ/mol

Possible oxidation of Mo^{IV} into Mo^{VI} \rightarrow Volatilisation

Metallic phase added: L/L contact 4h at 830°C

 $\rightarrow\,$ Sampling of each phase: quantification of Mo

LiF-All	410
•	$M_x O_y \longrightarrow AlF_3$
MF ₃	
м	AI
	Al-Cu

% Mo in metal	% Mo in the salt	%Mo remaining
38,9 ± 2,8	$1,6 \pm 0,4$	59,5 ± 3,2

~40% of Mo in the metallic phase => possible reduction of Mo by Al

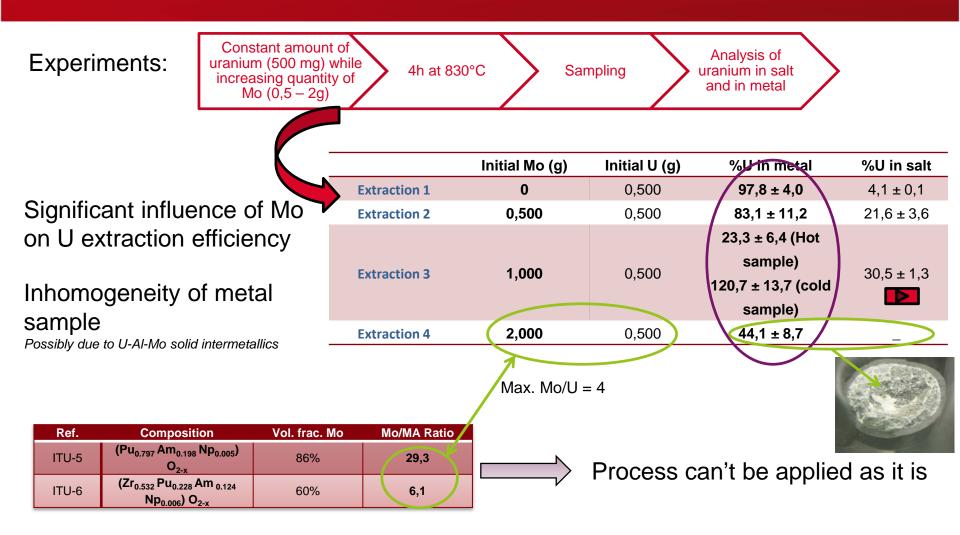
	Mo extraction by aluminium: possible mechanism	
Mechanism	Reaction	ΔG (kJ/mol) at 830°C
Direct	$\frac{3}{4} MoO_2 + Al = \frac{3}{4} Mo + \frac{1}{2} Al_2O_3$	-372,338
Indirect	$\frac{3}{4}MoF_4 + Al = \frac{3}{4}Mo + AlF_3$	-604,275
	$\frac{1}{2} MoF_6(g) + Al = \frac{1}{2} Mo + AlF_3$	-599,056

Coextraction of molybdenum together with actinides suspected

60% Mo not measured : Volatility + possible **solid Al-Mo intermetallic** compounds formed



MO INFLUENCE ON U EXTRACTION EFFICIENCY



Molybdenum must be removed prior the DOS process step



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DEN/DRCP/SCMS/LDPS

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Ceaden mo oxide volatilisation

From thermodynamic approach, metallic **Mo easily converted into MoO₂ and MoO₃** at high temperature MoO_3 : high volatility \rightarrow **Possibility to remove Mo prior the DOS process** with appropriate thermal treatment At 830°C At 1000°C **TGA** measurements MoO_3 volatilisation: MoO_3 volatilisation: $79.6 \pm 0.8\%$ 99.2% MoO₃ 100 - 200 mg 830 - 1000°C (Ar) 4h theoretical Mo/MA theoretical Mo/MA ratio after treatment **Reference pellet** Mo/AM initial ratio ratio after treatment at 830°C at 1000°C ITU 5 29.3 6.0 0,3 ITU 6 6.1 1,3 0.06 Results obtained with uranium %U in salt Mo/AM %U in metal 4.1 ± 0.1 0 97.8 ± 4.0 83,1 ± 11,2 $21,6 \pm 3,6$ Thermal treatment not sufficient ⇒ Thermal treatment sufficient \Rightarrow DOS process can be applied to CERMET reprocessing DEN/DRCP/SCMS/LDPS IPRC 2016 | SEPTEMBER 21 - 23rd 2016 | PAGE 15

CONCLUSIONS

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CERCER reprocessing

- Process successfully demonstrated on genuine unirradiated pellet
 - Mg remains in the salt \rightarrow No influence on Pu and Am extraction efficiency
- Accumulation of Mg in the process:
 - Significant influence on extraction efficiency of An
 - \rightarrow MgO : 0 3 wt%: no major influence
 - \rightarrow MgO : > 3wt% strong influence

- Dimensioning of the process: Possible treatment of 150 CERCER pellets/Kg of salt
- Further accumulation of MgO: Salt treatment needed
- Process needs to be optimised (use of $Na_3AIF_6 \rightarrow higher \ solubility \ expected$)
- CERMET reprocessing
 - Significant influence of Mo on An extraction efficiency
 - Coextraction of Mo
 - Solid intermetallic U-Al-Mo possibly formed
 - Mo oxides volatility:
 - \rightarrow Thermal treatment at 1000°C volatilises 99.2% of Mo

DOS process can be applied with and additional thermal treatment prior extraction step Mo/volatile FP separation? \rightarrow Refabrication of fresh matrix

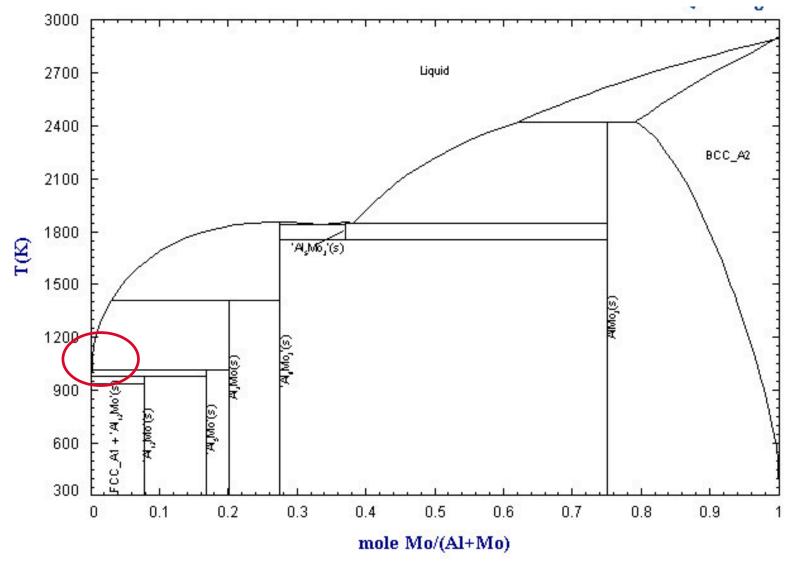
Prior removal of Mo needed

Thank you for your attention

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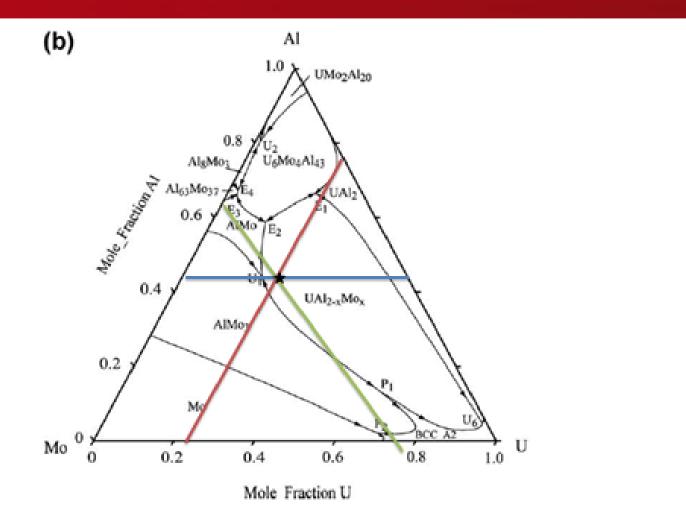
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TGA experiments on MoO₃ volatility

