



Mechanical property evolution with radiation damage in (U,Pu)O₂ a MD simulation study

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Mechanical Property Evolution with Radiation Damage in (U,Pu)O₂:

a Molecular Dynamics Simulation Study

L. Van Brutzel, H. Balboa, A. Chartier

DEN, DPC, SCCME

CEA-Saclay, 91191 Gif-sur-Yvette, FRANCE

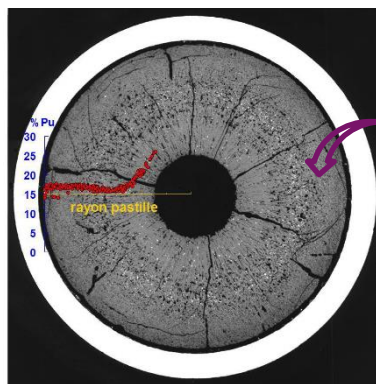
NuMat 2018

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materialstoday
Connecting the materials community

MOX FUEL DESIGN, AN ENGINEERING CHALLENGE

Transverse metallographic section of a Phénix fuel pin



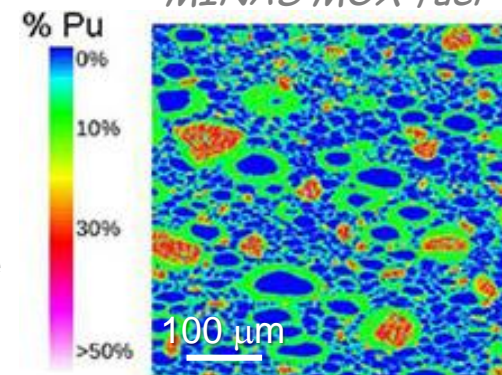
In reactors

- Temperature, ∇T
- Stress, $\nabla \sigma$
- Burn-up

Microstructure heterogeneity

- High Pu zone
↗ radiation damage

EPMA images of MINAS MOX fuel



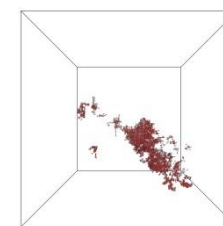
(Oudinet JNM 375 (2008) 86)

**Origin of microstructure evolution?
Mechanical properties?**

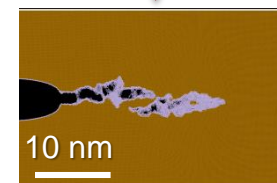
■ **Method:** atomistic simulations → nanoscale (U,Pu)O₂
Molecular Dynamics

■ **Goal:**

- Understanding phenomena
- Input parameters for mesoscale models



radiation



mechanical properties

- I. Properties of non-irradiated (U,Pu)O₂**
- II. Structure evolution with radiation damage**
- III. Mechanical behavior for irradiated (U,Pu)O₂**
- IV. Summary**

EMPIRICAL POTENTIALS

- Rigid ion potentials (no charge transfer)

$$\phi(r) = \underbrace{E_{\text{Coulomb}}(r^{-1}) + E_{\text{rep}}(e^{-r}) + E_{\text{vdW}}(r^{-6})}_{\text{2-body}} + \underbrace{E_{\text{EAM}}(r, \rho)}_{\text{many-body}}$$

- Two potentials have been assessed systematically:

- **MOX-07:** 2-body (Potashnikov JNM 419 (2011) 217)

- **Cooper:** 2-body + EAM (Cooper JNM 461 (2015) 206)

$E_{\text{EAM}} \Rightarrow$ reproduces Cauchy violation ($C_{12} \neq C_{44}$)

- For both potentials thermodynamic properties fit Fink's recommendation

(Fink JNM 279 (2000) 1)

- Lattice parameter, thermal expansion \rightarrow 2100 K

- Vegard's law verified \rightarrow 2100 K \Rightarrow (U_yPu_{1-y})O₂ solid solution

- Specific heat: $C_p = \frac{1}{n} \left(\frac{\partial H}{\partial T} \right)_p \rightarrow \lambda\text{-peak} =$ superionic transition at $T \approx 0,8 T_m$

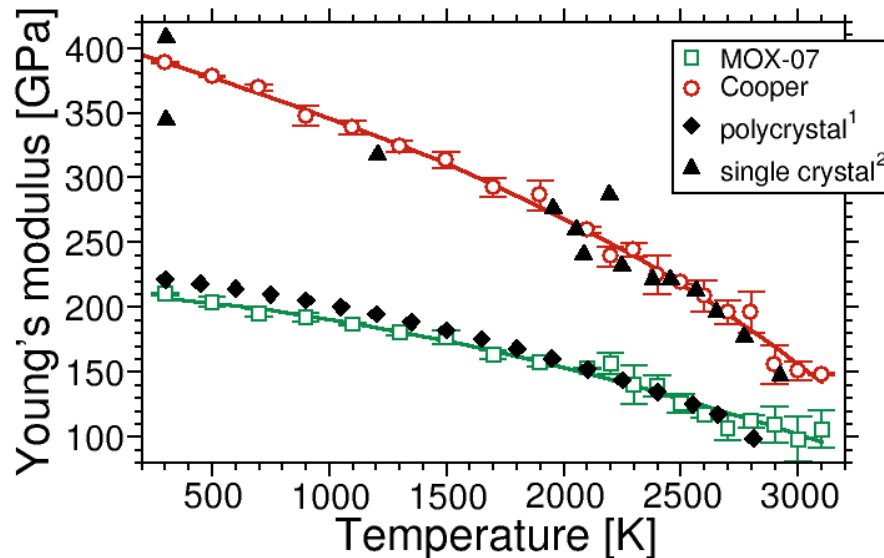
(Balboa JNM 495 (2017) 66)

POTENTIALS: MECHANICAL PROPERTIES I

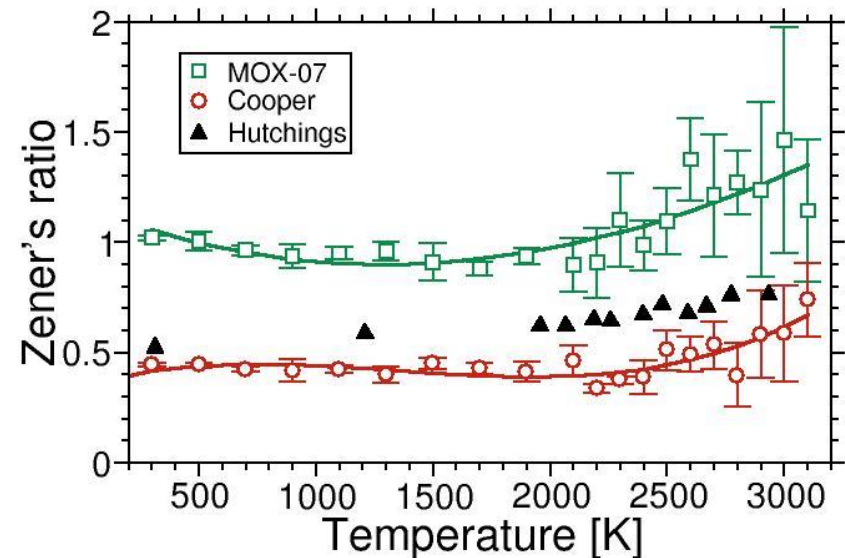
Elastic stiffness coefficients (C_{11} , C_{12} , C_{44})

- Anisotropy factor **Zener's ratio**: $Z = \frac{2C_{44}}{C_{11}-C_{12}}$, $Z=1 \rightarrow$ isotropic (cubic: $Z<1 \rightarrow E_{111}<E_{100}$)

UO₂



UO₂



- Cooper fit single-crystal exp.² / MOX-07 fit polycrystal recommendation¹

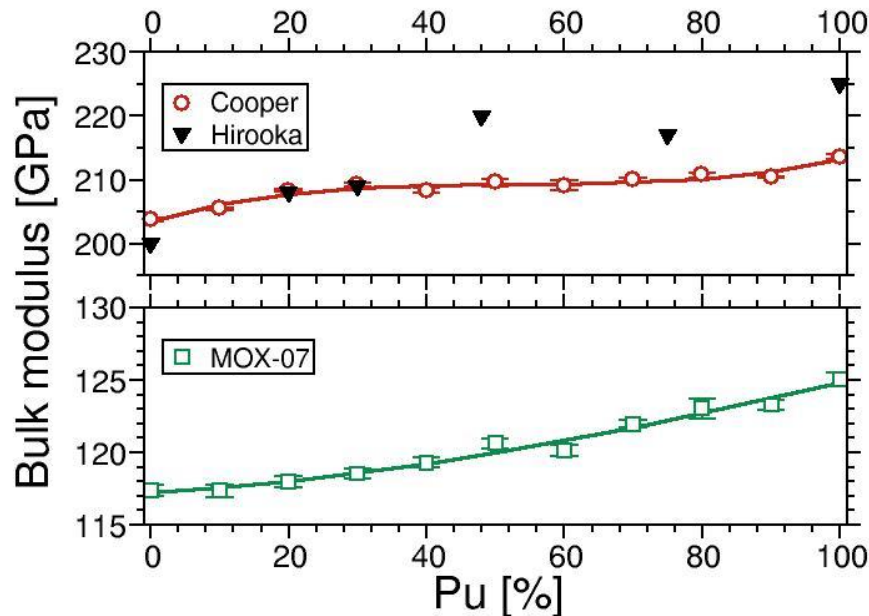
- Cooper: **anisotropic** / MOX-07: **isotropic**

¹ (Martin High Temp. High Press. 21 (1989) 13)

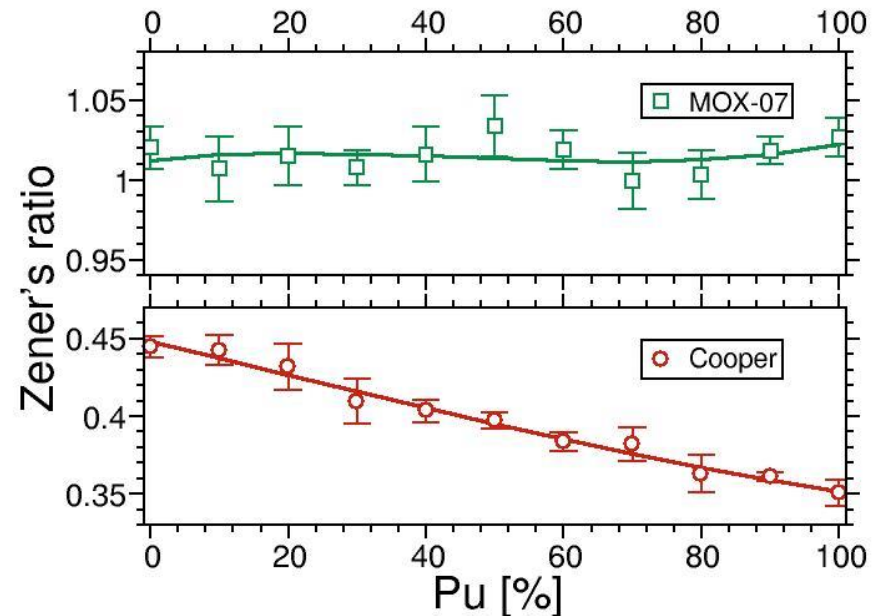
² (Hutchings J. Chem. Soc., Faraday Trans. 83 (1987) 1083)

Influence of the Pu content

300 K



300 K



- **Bulk modulus:** 5% **increase** with Pu content **for both potentials**
- **Zener:** Cooper **decreases** with Pu content / MOX-07 **constant**

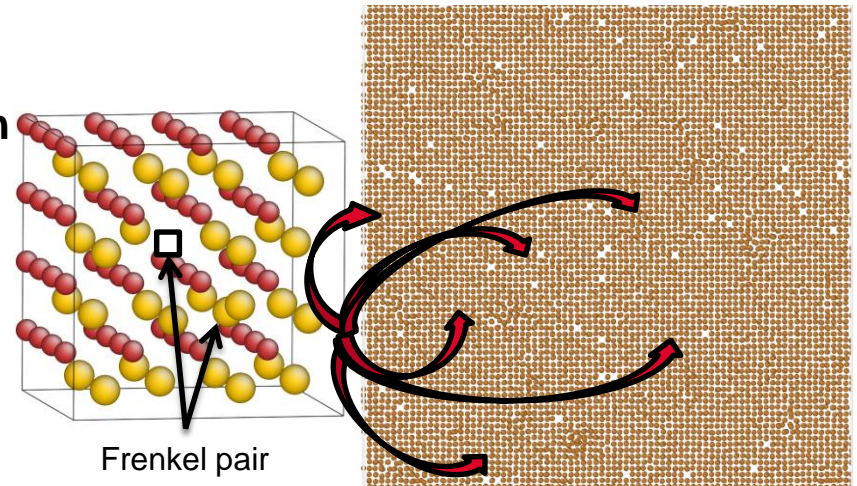
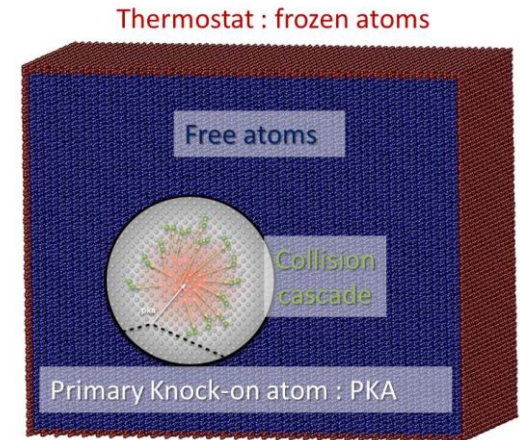
Empirical potential main difference = **anisotropy**




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Study of Primary Damage with Molecular Dynamics

- Code: **LAMMPS**
- $(U,Pu)O_2$: U and Pu randomly distributed
- **Primary Damage: Displacement Cascades**
 Primary Knock-on Atom: Cation
 $E_{PKA} = 2 \rightarrow 75 \text{ keV}$
 $T = 300 \text{ K}$
 \Rightarrow **1 radiation event** = parameter for FPA
- **Dose Effects: Point Defects Accumulation**
 Creation of random Cation Frenkel pairs
 Dose rate: 10^9 dpc/s
 Dose: $0 \rightarrow 3 \text{ dpc}$
 $300 - 1600 \text{ K (relaxation NPT)} \rightarrow \text{Swelling}$



Microstructure evolution

■ MD analysis: **OVITO** 

- Point defect: Voronoï cell
- Dislocation: DXA

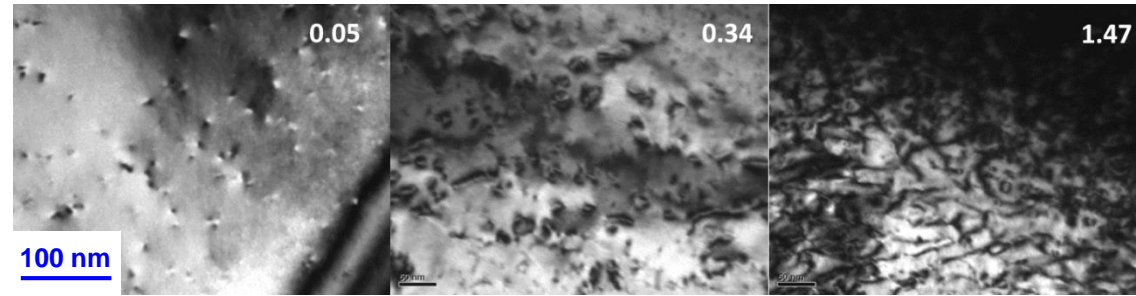
5 stage process

1. point defects creation
2. aggregation into clusters
3. nucleation of Frank loops
4. transformation into unfaulted loops via Shockley that in turn grow
5. reorganization into forest dislocations

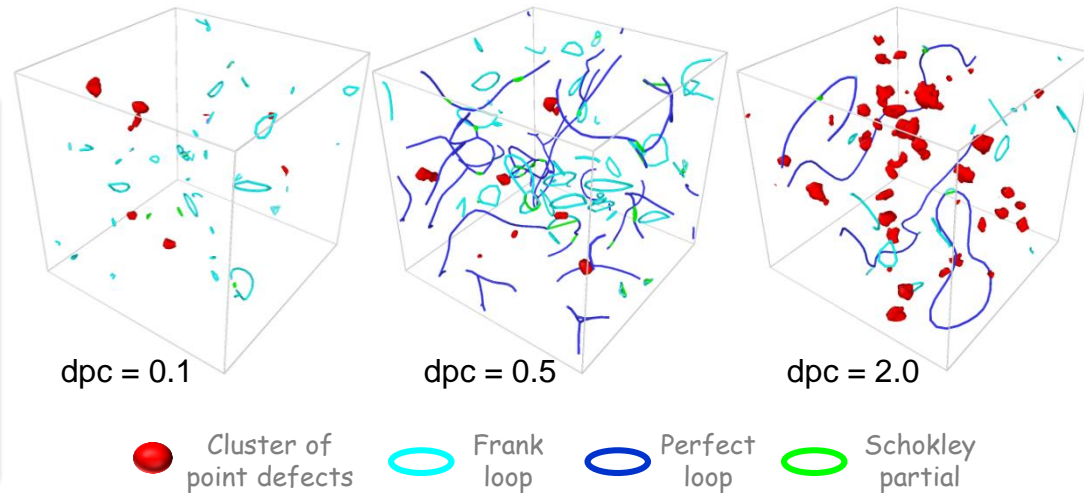


Onofri J. Nucl. Mat. 482 (2016) 105
 Onofri J. Nucl. Mat. 494 (2017) 252
 Chartier Appl. Phys. Lett. 109 (2016) 181902
 Balboa <https://doi.org/10.1016/j.jnucmat.2018.07.056>

Experimental: TEM images of irradiated UO_2



MD simulations: FPA in $(\text{U,Pu})\text{O}_2$ calculated with MOX-07



Exp: 2 nm min (*TEM resolution*)

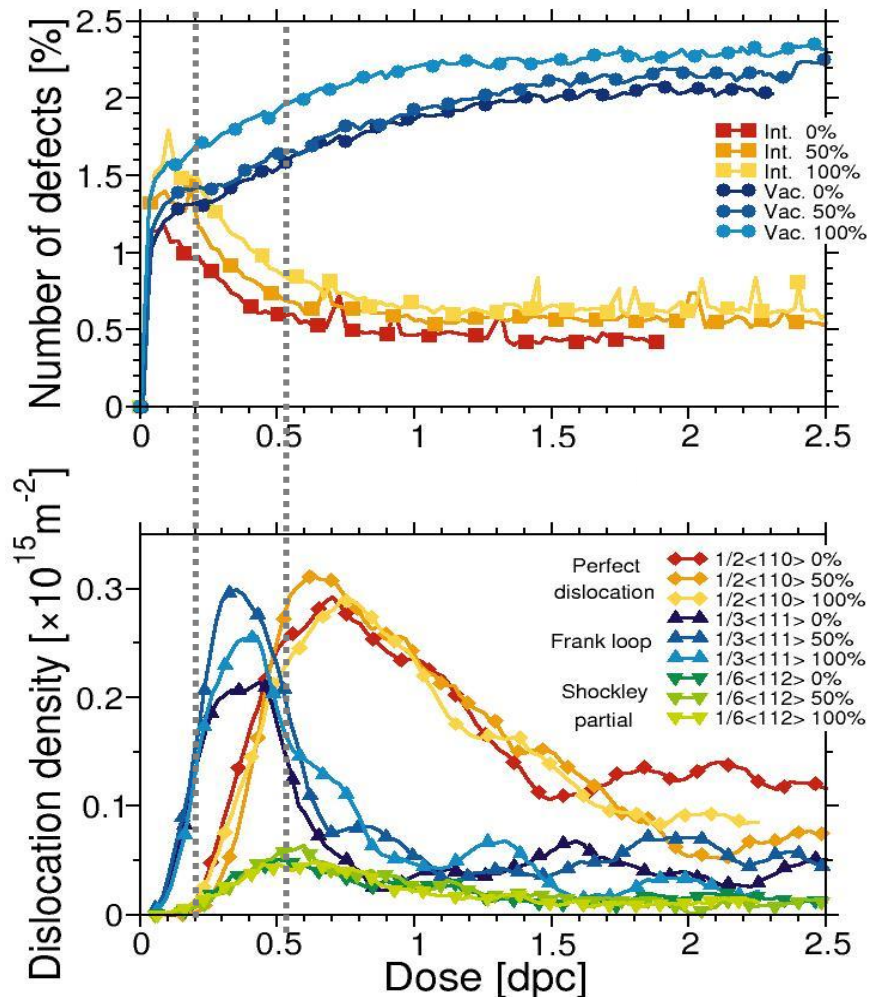
$\frac{1}{2} \langle 110 \rangle$ loops $\rightarrow \frac{1}{2} \langle 110 \rangle$ lines

MD: point defects $\rightarrow \frac{1}{3} \langle 111 \rangle$ loops $\rightarrow \frac{1}{2} \langle 110 \rangle$ loops $\rightarrow \frac{1}{2} \langle 110 \rangle$ lines

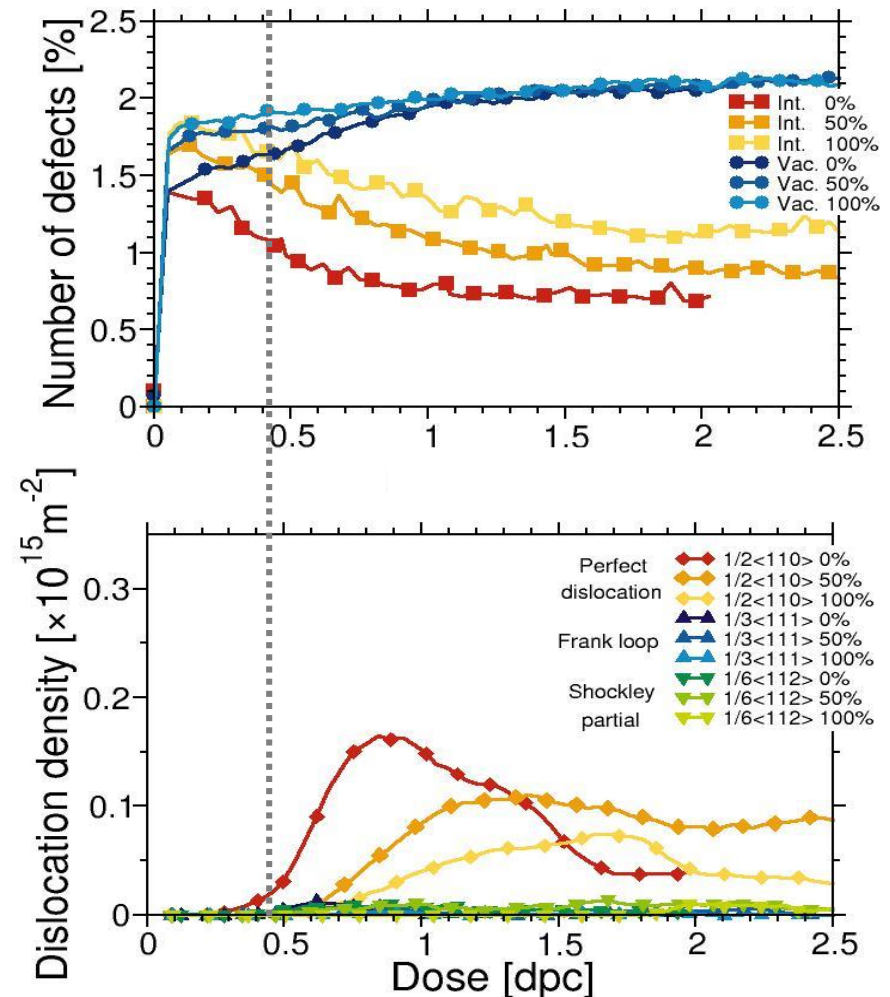
Frank loops perfect loops

MICROSTRUCTURE EVOLUTION VS DOSE

MOX-07



Cooper



■ Cooper: more point defects, less dislocations / more Pu influence

- I. Properties of non-irradiated (U,Pu)O₂
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MECHANICAL PROPERTIES WITH DOSE - METHOD

Elastic constants: small deformation

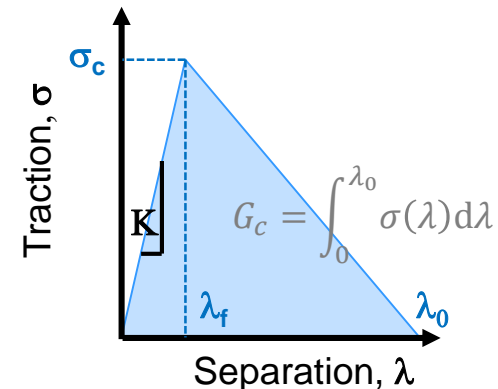
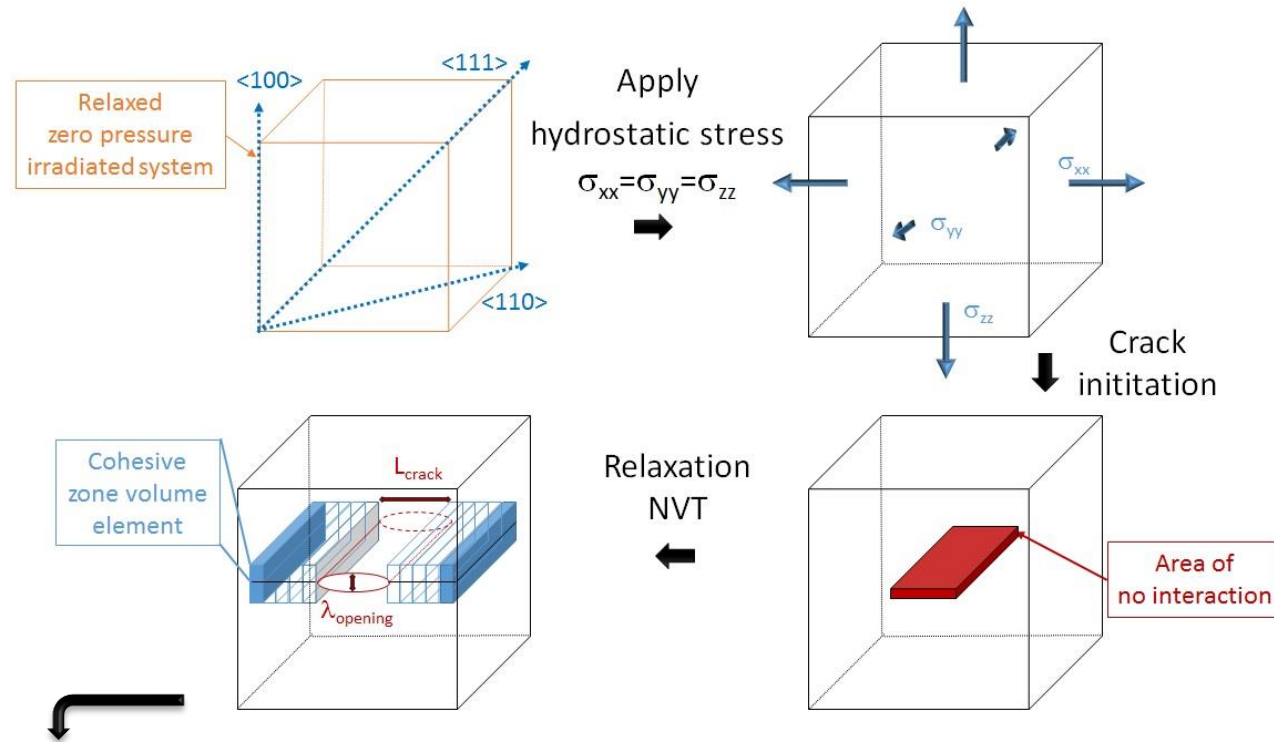
$$\sigma_{ij} = C_{ijkl} \varepsilon_{kl}$$

Cohesive strength:
Yamakov method

→ avoid strain-rate issue
(phase transition at the crack tip)

Yamakov J. Mech. Phys. Solids, 54
(2006) 1899

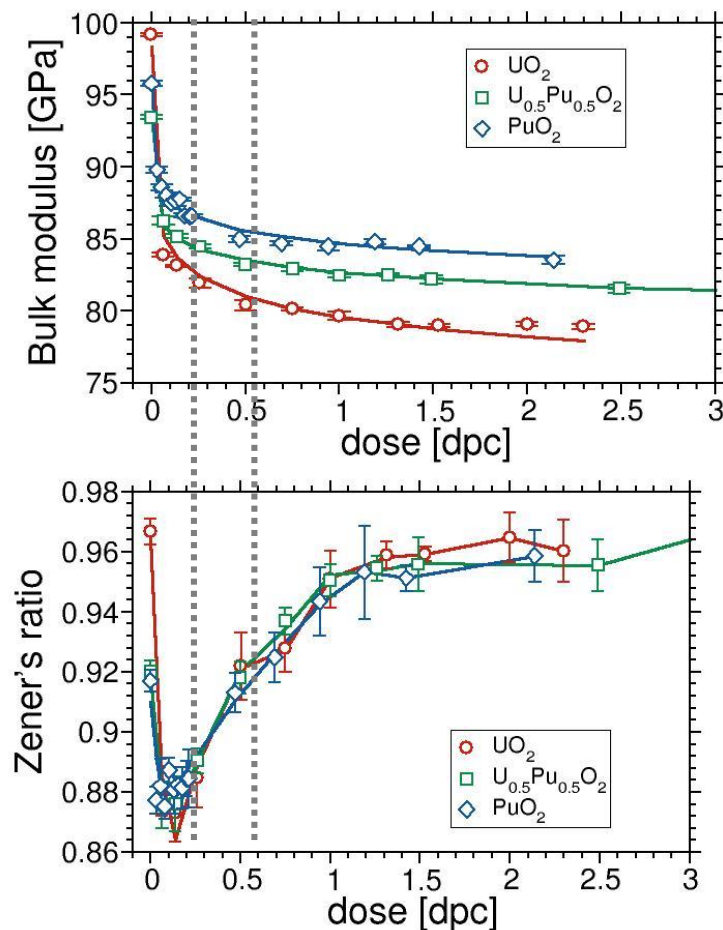
Output
Traction-separation
Cohesive Strength: σ_c
Energy release stresses
 $G_c \rightarrow K_{IC}$



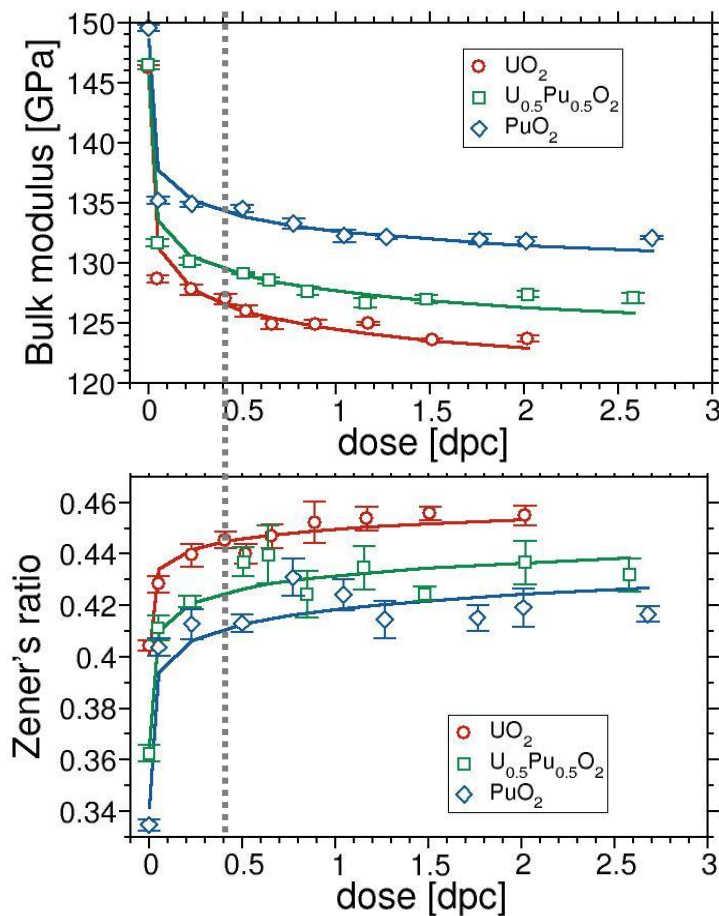
MECHANICAL PROPERTIES WITH DOSE

Elastic stiffness coefficients

MOX-07



Cooper



Point defects \Rightarrow Bulk modulus decrease & anisotropy changes

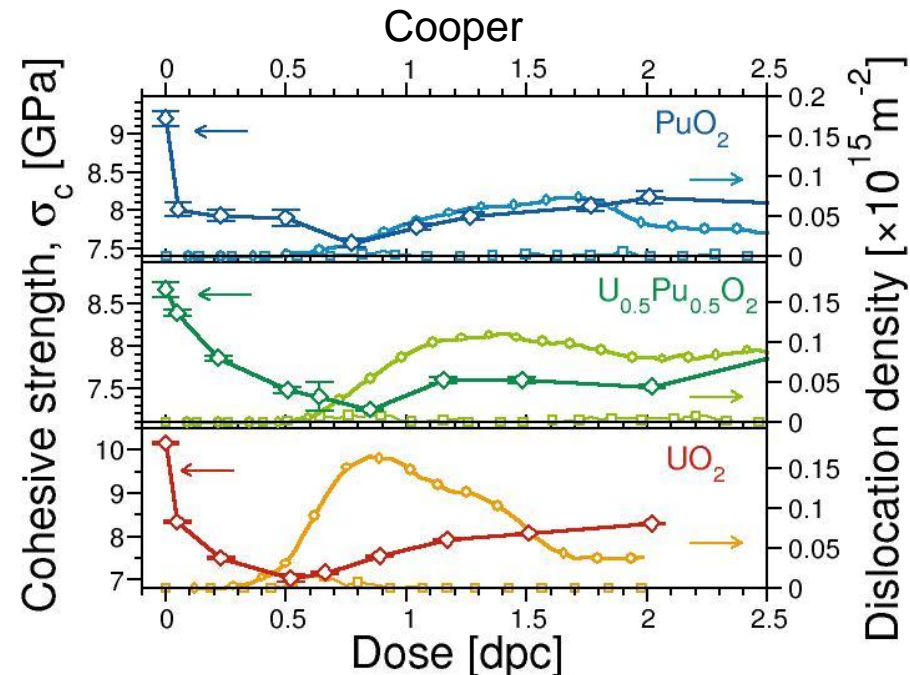
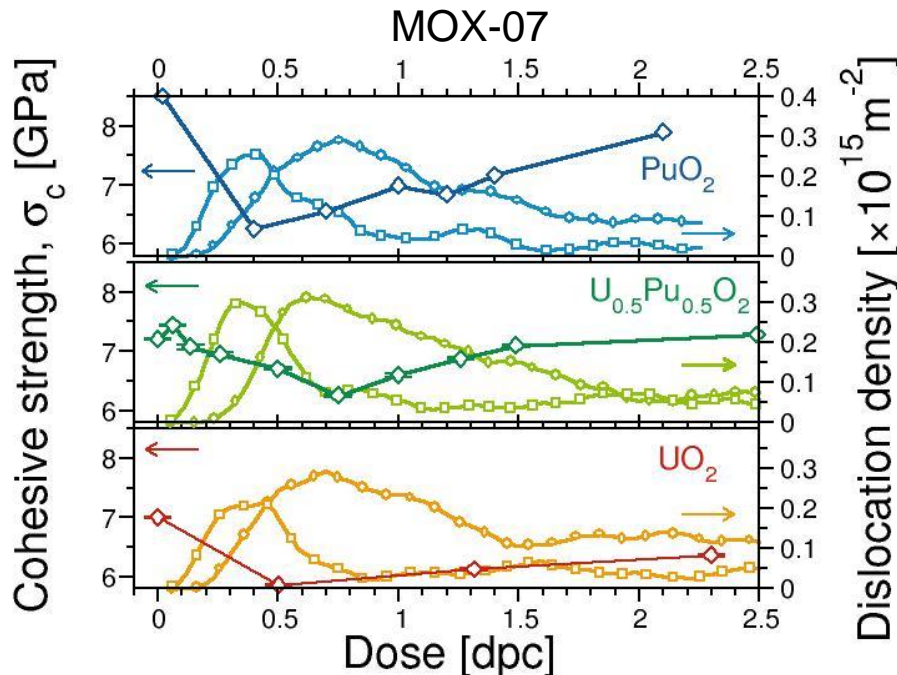
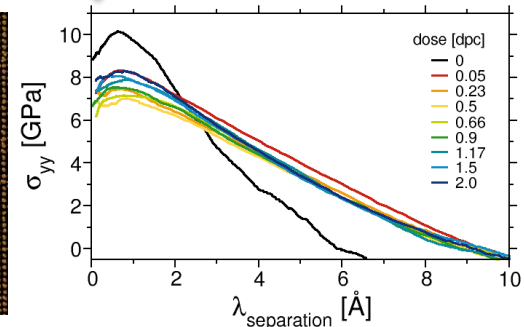
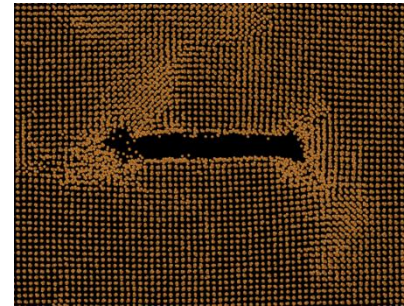
MECHANICAL PROPERTIES WITH DOSE

Cohesive Strength

- Both potentials have similar behavior
- $\text{Min } \sigma_c \Leftrightarrow \text{Max int.} + \text{Frank loops}$

Cohesive strength related to:
point defects + Frank loops

Cracking example



(\diamond) cohesive strength, (\circ) $\frac{1}{2}\langle 110 \rangle$ perfect dislocation, (\square) $\frac{1}{3}\langle 111 \rangle$ Frank loop

■ **Mechanical behavior assessment** of (U,Pu)O₂ with MD simulations

- Two rigid ion interatomic potentials: **Cooper** & **MOX-07**
- **Difference** in the elastic stiffness **anisotropy**
- Variations but **main behavior identical**

■ **Radiation structure evolution**

- 5 stage process:

1) point defects 2) clustering 3) Frank loop 4) unfaulted loop 5) forest of dislocations

■ **Mechanical properties with dose**

- **Bulk modulus** ↘ correlated to **point defects** (swelling)
- **Cohesive strength** ↘ correlated to **point defects** + **Frank loops**

■ **Pu content**

- Influence on the absolute values but not on the behavior

Acknowledgments



Challenge project – C097073



Thank you for listening

Questions ?

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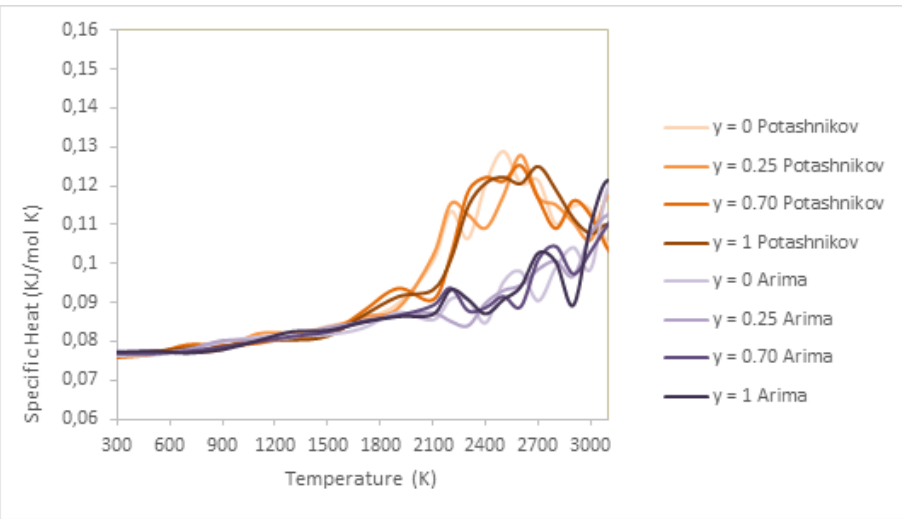
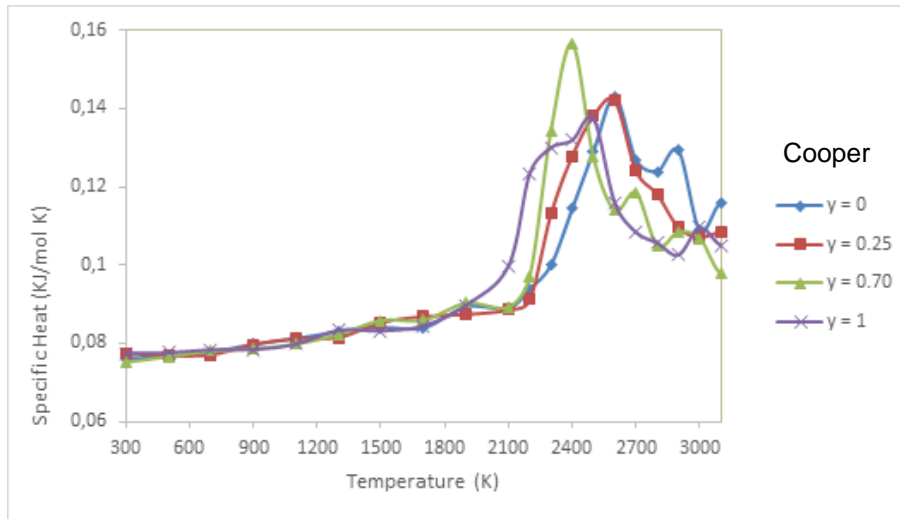
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Direction de l'Energie Nucléaire
Département de Physico-Chimie
Service de la Corrosion et du
Comportement des Matériaux dans
leur Environnement

ASSESSMENT POTENTIAL - THERMODYNAMICS

Assessment of $U_{1-y}Pu_yO_2$: $0 < y < 1$ and $300 \text{ K} < T < T_m$

- Lattice parameter, thermal expansion fit well Fink's recommendation & Uchida → 2100 K
- Vegard's law verified → 2100 K
- Specific heat: $C_p = \frac{1}{n} \left(\frac{\partial H}{\partial T} \right)_P$



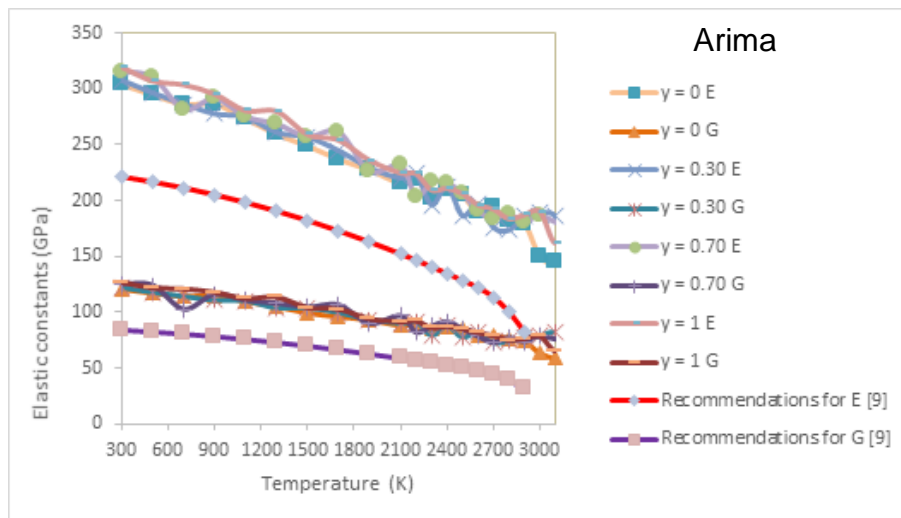
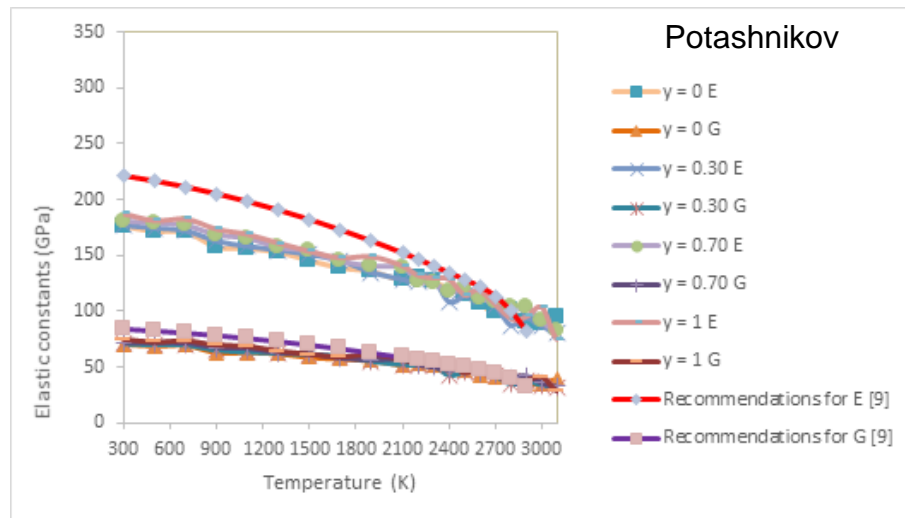
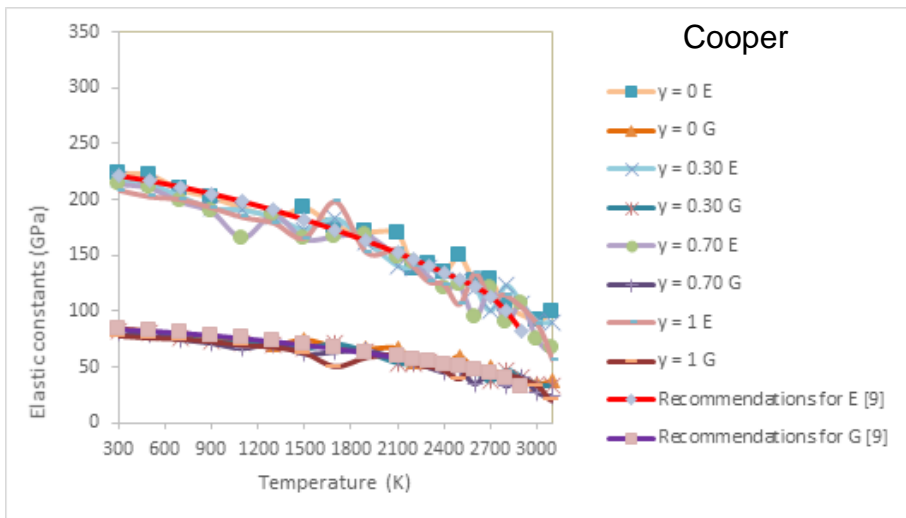
- λ -peak = superionic transition^{1,2} at $T \approx 0,8 T_m$
- Cooper & Potashnikov = OK, Arima no λ -peak

¹J Ralph, J of Chemical Society 83, 1253 (1987)

²C Ronchi, J Alloys Compd, 213, 159 (1994)

ASSESSMENT POTENTIAL – MECHANICS I

Elastic stiffness coefficients



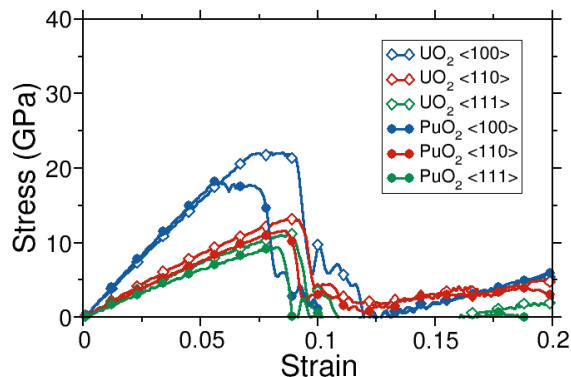
E: Young's modulus
G: shear modulus

All potentials \searrow with temperature &
independent to Pu content
but
Cooper > Potashnikov > Arima

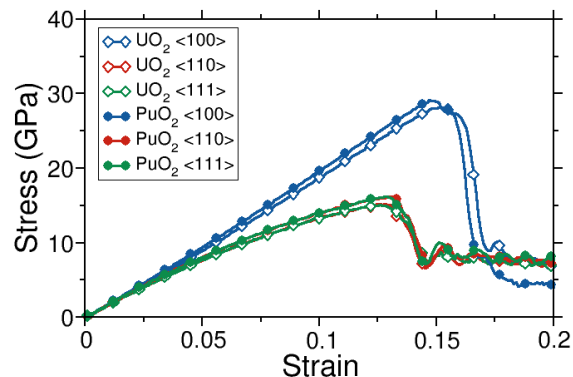
Stress-Strain curves in bulk

- All potentials: $\sigma_{\text{yield}}\langle 100 \rangle \gg \sigma_{\text{yield}}\langle 111 \rangle$ & $\sigma_{\text{yield}}\langle 110 \rangle \Rightarrow$ agreement with experiments
- For $\langle 111 \rangle$ & $\langle 110 \rangle$ few influence of the Pu content

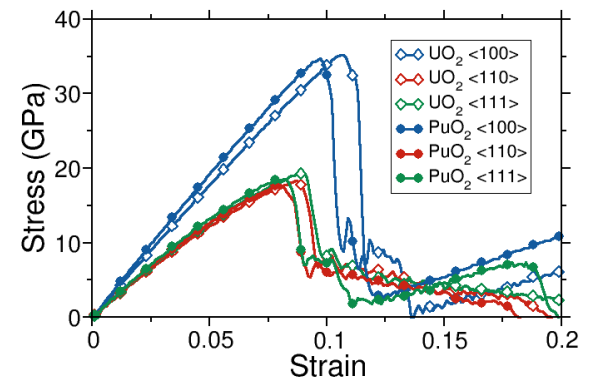
Cooper - 300 K



Potashnikov - 300 K



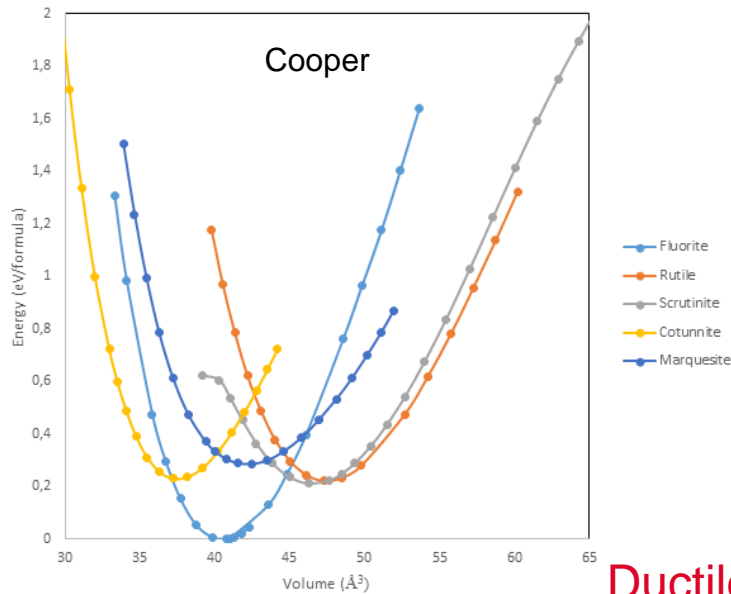
Arima - 300 K



Cooper				Potashnikov				Arima			
		σ_{yield} (GPa)	$\epsilon_{\text{fracture}}$ (%)	σ_{yield} (GPa)	$\epsilon_{\text{fracture}}$ (%)	σ_{yield} (GPa)	$\epsilon_{\text{fracture}}$ (%)	σ_{yield} (GPa)	$\epsilon_{\text{fracture}}$ (%)	σ_{yield} (GPa)	$\epsilon_{\text{fracture}}$ (%)
<100>	UO ₂	22.0	7.6	28.1	15.2	35.1	10.6				
	PuO ₂	18.5	5.6	29.0	14.8	34.2	9.6				
<110>	UO ₂	13.2	9.0	15.1	13.0	18.0	8.8				
	PuO ₂	11.6	8.5	16.1	13.1	17.8	8.0				
<111>	UO ₂	10.9	8.8	15.0	12.7	19.3	9.0				
	PuO ₂	9.3	8.3	16.1	12.9	18.4	8.3				

σ_{yield} : Arima > Potashnikov > Cooper
 $\epsilon_{\text{fracture}}$: Potashnikov > Cooper \geq Arima

ASSESSMENT POTENTIAL – MECHANICS III

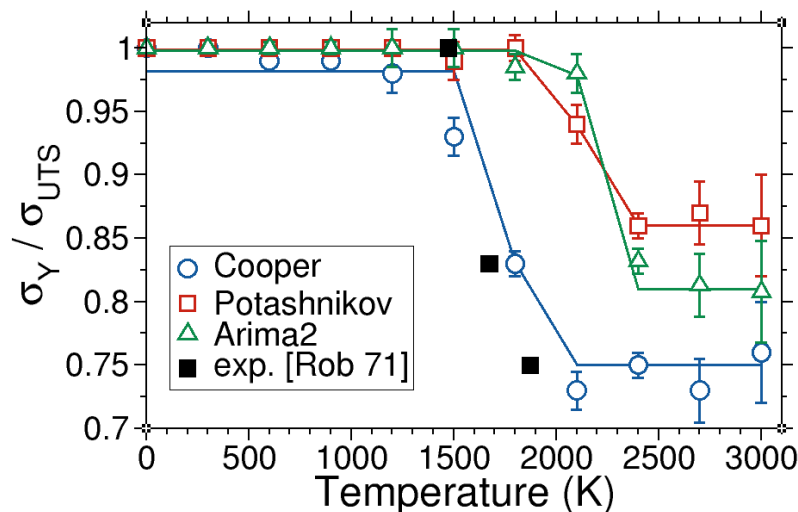


Transition pressure	Fluorite to			
	Cotunnite (GPa)	Rutile (GPa)	Scrutinite (GPa)	Marquesite (GPa)
Cooper	2.95	-6.84	-8.02	-15.99
Potashnikov	16.03	-10.57	-12.08	-
Arima	44.34	-8.30	-9.61	-

Cooper shows lower transition pressures than the other potentials

Ductile-brittle transition temperature

MOX, PuO₂ 20% wt

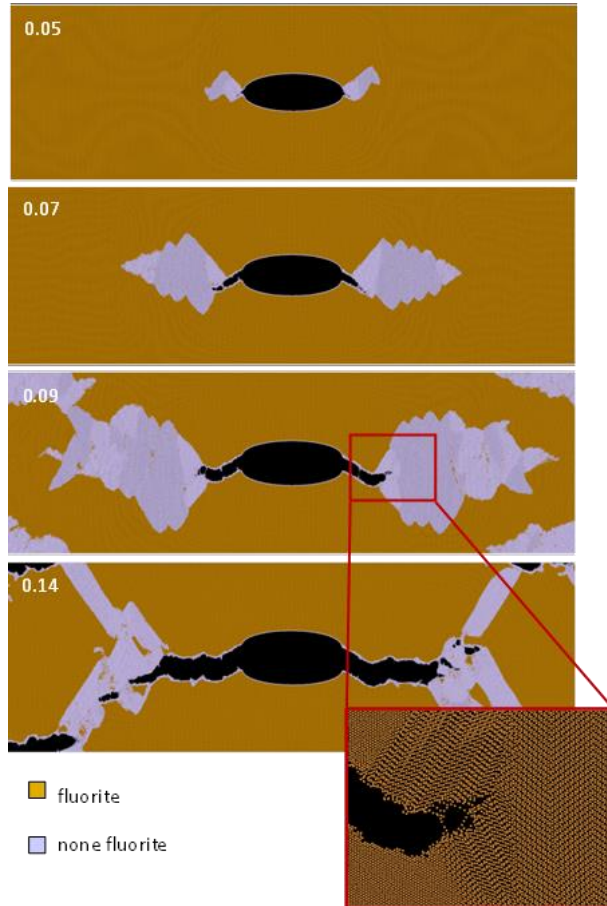


Cooper potential shows a behaviour closer to experiments

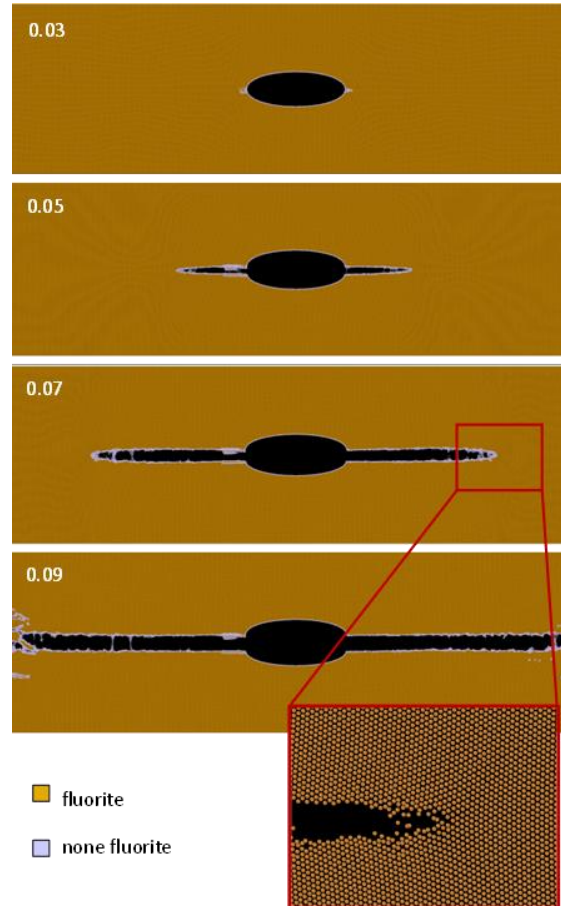
ASSESSMENT POTENTIAL – MECHANICS IV

- Crack propagation – 15% Pu, $\langle 111 \rangle$, 300 K
- The system included 4.4×10^6 atoms with box size equal to $240 \times 70 \times 4$ nm

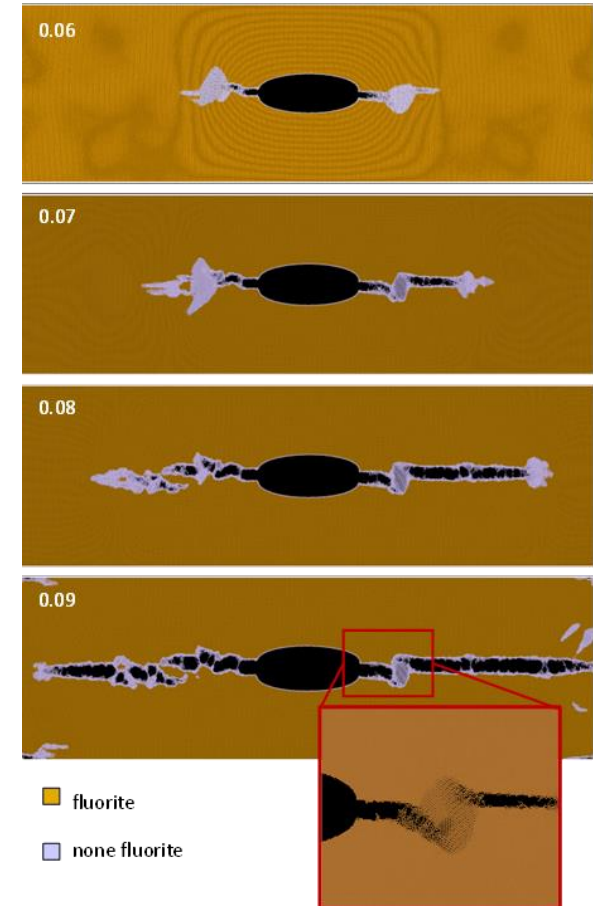
Cooper



MOX-07



Arima



Strain
↕

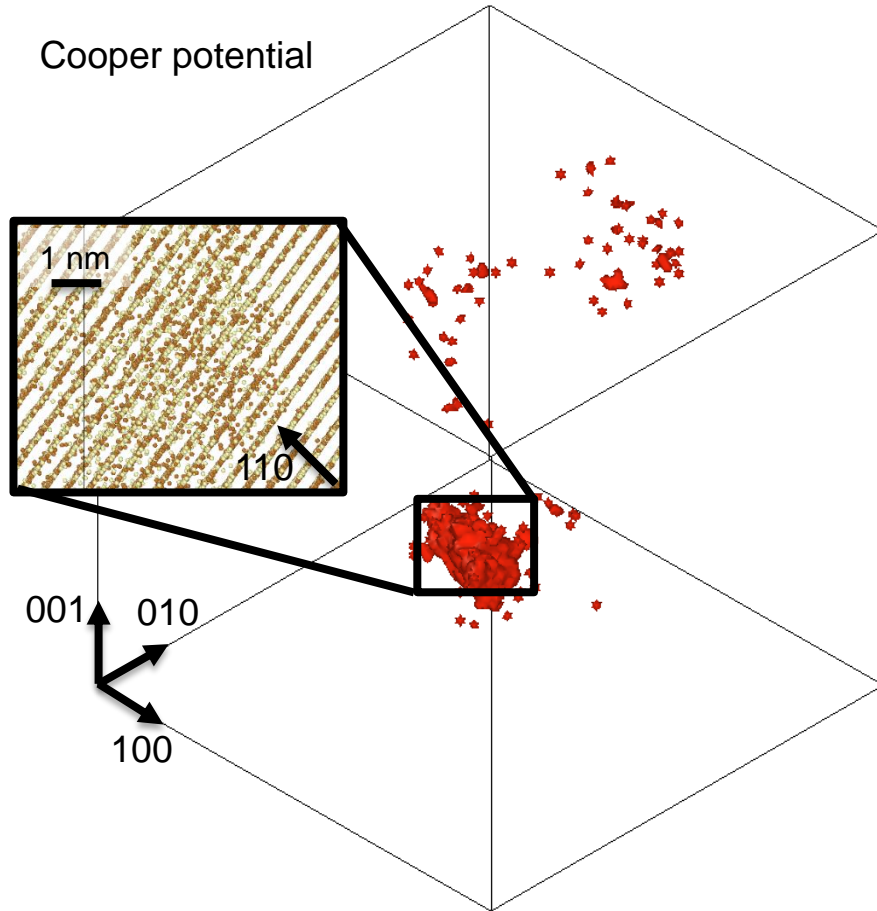
■ Cooper & Arima \Rightarrow "plastic-like" ; MPX-07 \Rightarrow brittle behaviour

Results included in this document are CEA's property. They cannot be disclosed without prior authorization.

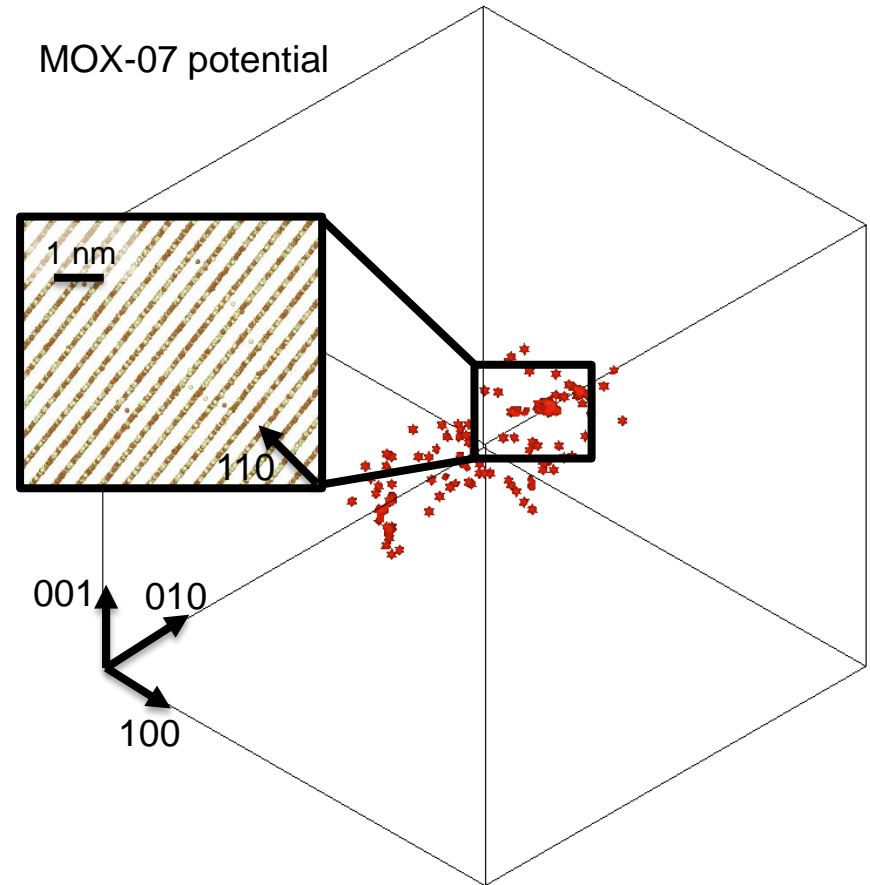
DISPLACEMENT CASCADES

Damage created by 75 keV displacement cascade in $\text{U}_{0.5}\text{Pu}_{0.5}\text{O}_2$

Cooper potential

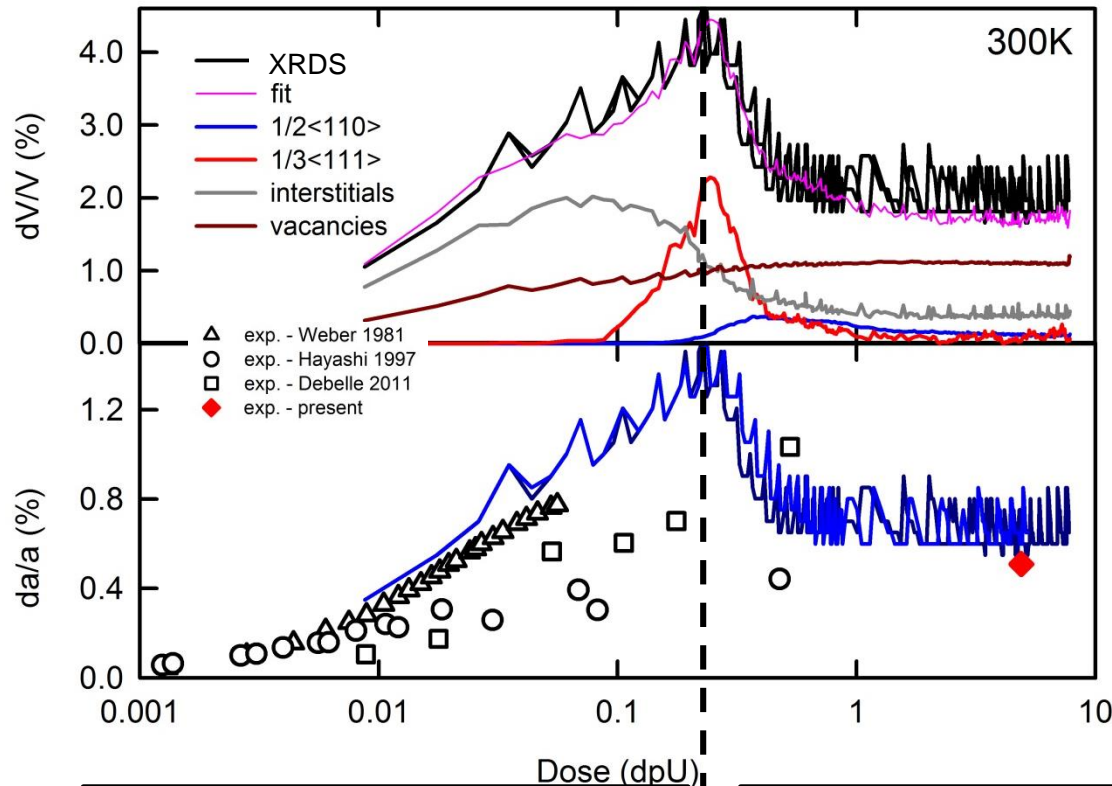


MOX-07 potential



LATTICE EVOLUTION WITH IRRADIATION DOSE

Deconvolution of the Lattice evolution under irradiation

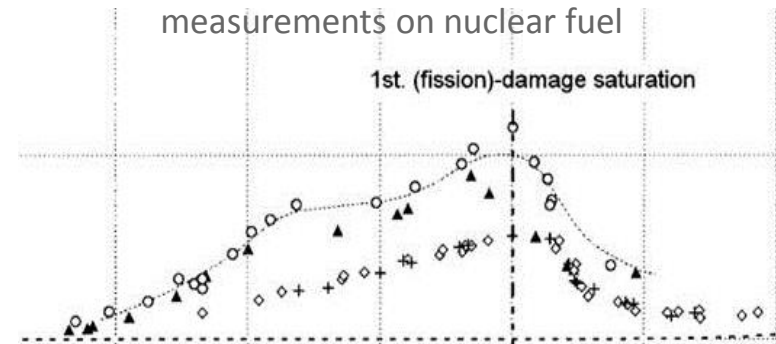


$$\frac{\Delta V}{V} = V_I^f \times \rho_{\text{line}} + \frac{\overline{R_{\text{loop}}} \times b}{2} \times \rho_{\text{loop}} + \frac{V_{\text{rel}}^I}{\Omega} \times C_I + \frac{V_{\text{rel}}^V}{\Omega} \times C_V$$

$$\text{with } V_I^f = 5.6 \text{ \AA}^3; \overline{R_{\text{loop}}} \sim 3 \text{ nm}; V_{\text{rel}}^I = V_{\text{rel}}^V = 1. \Omega$$

Lattice expansion

contraction comparable to
measurements on nuclear fuel



Swelling:

- **interstitials** and **vacancies**
- 1/3<111> **Frank loops**

Contraction:

- transformation of **Frank loops** into **perfect loops**
- **vacancies** at steady state

