

Towards an innovative $R_{ij}-\epsilon$ model for turbulence in bubbly flows from DNS simulations

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5th International Conference on Turbulence and Interactions

Towards an innovative $R_{ij} - \epsilon$ model for turbulence in bubbly flows from DNS simulations



1 : DEN-Service de thermo-hydraulique et de mécanique des fluides (STMF), CEA, Université Paris-Saclay, F-91191 Gif-sur-Yvette

2 : PROMES-CNRS (UPR 8521) Université de Perpignan Via Domitia

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Industrial purposes and boiling flows



Safety issue for PWR : the boiling crisis

Pressurized water reactor : a very large system
 Critical heat flux : a very local phenomenom
 Solution : the upscaling strategy

Lack of predictive model in two phase flows

- A lot of different regimes
- The importance of the transition between boiling and slug flows
- Bubbles at the wall \rightarrow decrease of heat transfer
- Importance of the void fraction prediction
- Focus on dynamical aspects in bubbly flows









Towards a numerical reactor Need for powerful simulations



How can complex two-phase flows be solved in a system code?









Towards a numerical reactor Need for powerful simulations



How can complex two-phase flows be solved in a system code?









Towards a numerical reactor Need for powerful simulations



How can complex two-phase flows be solved in a system code?









RANS closures limitations

- Empirical correlations built on coupled mechanism simultaneously
 - \rightarrow Interfacial forces :
 - Drag force
 - Lift force
 - Added-mass force
 - **Dispersion forces**
- Point-size particle approach No surface tension effects One pressure closure
- Theoretical modelling based on questionable parallel with single phase flows
 - → Turbulence closure Single-phase turbulence Wake structure Wake interactions and instabilities



Two different kinds of turbulence







Flow led by the upward pressure gradient

- Classical turbulence with elongated streaks
- Single Phase Turbulence (SPT) due to shear stresses at the wall
- Sufficient existing model

Two different kinds of turbulence







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Flow led by bubbles buoyancy (WIF+WIT)

- Potential flow and averaged Wake Induced Fluctuations (WIF)
- Wake Induced Turbulence due to interactions and instabilities of wakes (WIT)
 - Unsatisfactory models

Two different kinds of turbulence





WIF+WIT

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Modelling conclusion : Bubble turbulence cannot be modelled as a kinetic energy source term





Introduction

Direct Numerical Simulations

Governing equations Limitation of DNS Numerical setup

Results and modelling on swarm calculations

Local scale (DNS) / Averaged scale (RANS)

Local instantaneous description

Navier-Stokes equations :

$$\frac{D\rho_k \mathbf{u}_k}{Dt} = -\nabla P_k + \rho_k \mathbf{g} + \nabla \cdot \underbrace{\left[\mu_k \left(\nabla \mathbf{u}_k + \nabla^T \mathbf{u}_k\right)\right]}_{\tau_k}$$

Interfacial jump conditions :

$$\mathbf{u}_{\mathbf{l}}^{\mathbf{i}} = \mathbf{u}_{\mathbf{v}}^{\mathbf{i}}, \qquad \sum_{k} \left(\boldsymbol{p}_{k} \mathbf{n}_{\mathbf{k}} - \tau_{k} \cdot \mathbf{n}_{\mathbf{k}} \right) = \sigma \kappa \mathbf{n}_{\mathbf{k}}$$



Local scale (DNS) / Averaged scale (RANS)

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Extension to full space

Multiply by phase indicator function : $\chi_k = 1$ in phase k, 0 otherwise.

 $\frac{D\chi_k\rho_k\mathbf{u}_k}{Dt} = -\nabla\left(\chi_k\boldsymbol{P}_k\right) + \chi_k\rho_k\mathbf{g} + \nabla\left(\chi_k\tau_k\right) \\ - \left(\boldsymbol{\rho}_k\mathbf{n}_k - \tau_k.\mathbf{n}_k\right).\nabla\chi_k$



Local scale (DNS) / Averaged scale (RANS)

Local instantaneous description

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One-fluid formulation

'one-fluid' variables : $\phi = \sum_k \chi_k \phi_k$

$$\frac{D\rho \mathbf{u}}{Dt} = -\nabla P + \rho \mathbf{g} + \nabla \left[\cdot \mu \left(\nabla \mathbf{u} + \nabla^T \mathbf{u} \right) \right] + \sigma \kappa \mathbf{n} \delta^i$$



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Definition of averaging operators

Statistical average = temporal average :

$$\overline{\phi(x,y,z)}^{TX} = \frac{1}{\Delta t} \int_{t-\Delta t/2}^{t+\Delta t/2} \phi(x,y,z,\tau) d\tau$$

Phase average :

$$\overline{\phi}^{k} = \frac{\overline{\chi_{k}\phi_{k}}^{TX}}{\overline{\chi_{k}}^{TX}}$$

Local scale (DNS) / Averaged scale (RANS)



Local instantaneous description

Navier-Stokes equations :

$$\frac{D\rho_k \mathbf{u}_k}{Dt} = -\nabla P_k + \rho_k \mathbf{g} + \nabla \cdot \underbrace{\left[\mu_k \left(\nabla \mathbf{u}_k + \nabla^T \mathbf{u}_k\right)\right]}_{\tau_k}$$

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'one-fluid' variables : $\phi = \sum_k \chi_k \phi_k$

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Phase average :

$$\overline{\phi}^{k} = \frac{\overline{\chi_{k}\phi_{k}}^{TX}}{\overline{\chi_{k}}^{TX}}$$

Note
$$\alpha_k = \overline{\chi_k}^{TX}$$

$$\frac{D\alpha_{k}\rho_{k}\overline{\mathbf{u}_{k}}^{k}}{Dt} = -\nabla\left(\alpha_{k}\overline{P_{k}}^{k}\right) + \alpha_{k}\rho_{k}\mathbf{g} + \nabla\left(\alpha_{k}\overline{\tau_{k}}^{k}\right) \\ + \nabla\left(\alpha_{k}\overline{\Re_{k}}^{k}\right) \underbrace{-\left(\rho_{k}\mathbf{n}_{k} - \tau_{k}\cdot\mathbf{n}_{k}\right)\cdot\nabla\chi_{k}}_{\mathbf{M}_{k}}^{TX}$$

 $\mathbf{M}_{\mathbf{k}}$ is the interfacial force exerted on phase k

$$\mathbf{M}_{\mathbf{I}} + \mathbf{M}_{\mathbf{v}} = \overline{\sigma \kappa \mathbf{n} \delta^{i}}^{T \lambda}$$



Limitation of DNS





Framework hypotheses

- incompressible
- isothermal

Limitation of DNS

- Low void fraction \rightarrow to avoid coalescence (No contact line models)
- Limited Reynolds number \rightarrow moderate resolution of the mesh

 \rightarrow Unreachable industrial conditions for bubble columns

- \rightarrow Reachable industrial conditions for bubble swarms
- Models extracted from the DNS need a posteriori validation on experiments in reactor conditions



Numerical setup



Physical setup

- Bubble swarm in a flow initially at rest
- Fixed bubble simulation \rightarrow Spring force
- periodicity in x,y,z
- Different predefined population of bubbles
- Computation in typical reactor condition based on DEBORA experiments (freon 24 bar)
- $Re_b = 1176$ and Eo = 0.59

A Front-Tracking algorithm

- One-fluid equations are solved on an Eulerian / Cartesian mesh
- Interfaces are tracked on a Lagrangian mesh
- Validated by comparison with works of J.Lu and G.Tryggvason

HPC calculations

- ightarrow pprox 80 millions of cells
- ightarrow
 ightarrow pprox 1.000.000 h CPU a case







Introduction

Direct Numerical Simulations

Results and modelling on swarm calculations

Turbulent and non turbulent fluctuations Spectral analysis New turbulence modelling



Instantaneous velocity field from DNS with fixed bubbles SPT



Following F. Risso et al.

- Frame of reference of bubbles
 - \rightarrow Fixed bubble simulations
 - \rightarrow Spring force
- Total fluctuations



Instantaneous velocity field from DNS with fixed bubbles SPT



Temporal average \rightarrow Wake-induced fluctuations (WIF)



Following F. Risso et al.

- Frame of reference of bubbles
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- Total fluctuations

Wake Induced Fluctuations (WIF)

- Temporal average \rightarrow spatial fluctuations
- Due to the averaged wake
- Due to potential flow around bubbles
- It is not turbulence !



Instantaneous velocity field from DNS with fixed bubbles SPT



Temporal average \rightarrow Wake-induced fluctuations (WIF)



Wake-induced Turbulence (WIT)



Following F. Risso et al.

- Frame of reference of bubbles
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Wake Induced Fluctuations (WIF)

- Temporal average \rightarrow spatial fluctuations
- Due to the averaged wake
- Due to potential flow around bubbles
- It is not turbulence !

Wake Induced Turbulence (WIT)

- Temporal fluctuations
- Interactions and instabilities of wakes
- Is WIT similar to classical turbulence?

Modelling conclusion : WIF and WIT have to be modelled separately

Spectral analysis of WIT and WIF



PDF of velocity fluctuations (On \approx 8 million points)

PROMES

Spectral analysis of WIT and WIF



PDF of velocity fluctuations (On \approx 8 million points)



Spectral analysis of WIT and WIF





Modelling conclusion : WIT needs its own transport equation because its statistical signature is different than SPT

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Splitting of the transport equation

Dt



Splitting of the fluctuations



An innovative splitting of the R_{ij} transport equation

$$\frac{D\mathbf{R_{ij}}}{Dt} = -\mathbf{P_{ij}} + \mathbf{D_{ij}} + \phi_{ij} + \epsilon_{ij}$$

Exemple with the dissipation tensor

$$\epsilon_{11} = -2 \frac{\mu_I}{\rho_I} \overline{\chi_I} \frac{\partial u_I}{\partial x_b} \chi_I \frac{\partial u_I}{\partial x_b}^{TX}$$
(100%)





Splitting of the transport equation



Splitting of the fluctuations



An innovative splitting of the *R_{ij}* transport equation

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(100%)





With DNS \rightarrow post-treatment of all the statistical correlations in order to find scaling laws for the interfacial production, the dissipation etc...





Modelling conclusion :

- 1 BIF cannot be modelled as a kinetic energy source term

2 - WIF and WIT have to be modelled separately
3 - WIT needs its own transport equation because its statistical signature is different than SPT





Modelling conclusion :

- **1 BIF cannot be modelled as a kinetic energy source term**
- 2 WIF and WIT have to be modelled separately

3 - WIT needs its own transport equation because its statistical signature is different than SPT

Formal summary

$$\begin{split} \mathbf{R}_{ij} &= \mathbf{R}_{ij}^{\text{SPT}} + \mathbf{R}_{ij}^{\text{WIT}} + \mathbf{R}_{ij}^{\text{WIF}} \\ \frac{D\mathbf{R}_{ij}^{\text{SPT}}}{Dt} &= \text{single-phase transport equation} \\ \frac{D\mathbf{R}_{ij}^{\text{WIT}}}{Dt} &= -\mathbf{P}_{ij}^{\text{WIT}} + \mathbf{D}_{ij}^{\text{WIT}} + \phi_{ij}^{\text{WIT}} + \epsilon_{ij}^{\text{WIT}} \\ \mathbf{R}_{ij}^{\text{WIF}} &= \text{algebraic closure} \end{split}$$

Sufficient existing models for \mathbf{R}_{ii}^{SPT}





Modelling conclusion :

1 - BIF cannot be modelled as a kinetic energy source term

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Formal summary

$$\begin{split} \mathbf{R}_{ij} &= \mathbf{R}_{ij}^{\text{SPT}} + \mathbf{R}_{ij}^{\text{WIT}} + \mathbf{R}_{ij}^{\text{WIF}} \\ \frac{D\mathbf{R}_{ij}^{\text{SPT}}}{Dt} &= \text{single-phase transport equation} \\ \frac{D\mathbf{R}_{ij}^{\text{WIT}}}{Dt} &= -\mathbf{P}_{ij}^{\text{WIT}} + \mathbf{D}_{ij}^{\text{WIT}} + \phi_{ij}^{\text{WIT}} + \epsilon_{ij}^{\text{WIT}} \\ \mathbf{R}_{ij}^{\text{WIF}} &= \text{algebraic closure} \end{split}$$

Sufficient existing models for \mathbf{R}_{ij}^{SPT}

On going work

- Computation of bubble swarms at different void fraction and bubble Reynolds number
- Model for **R**^{WIF}_{ij} based on previous works (F.Risso and al.) on averaged wake and potential flow solution around bubbles
- Post-treatment of all the statistical correlations of the $\mathbf{R}_{ij}^{\text{WIT}}$ transport equation in order to find scaling laws for $\mathbf{P}_{ij}^{\text{WIT}}$, ϕ_{ij}^{WIT} and $\epsilon_{ij}^{\text{WIT}}$





Up-scaling process from DNS database

- Answer to complex industrial applications (PWR core evolution)
 - \rightarrow RANS Euler calculations need predictive model
 - \rightarrow DNS used as numerical experiments
- DNS of channel bubbly flows (not presented here)
 - \rightarrow Lots of data available for processing
 - \rightarrow Already used to model interfacial forces
 - DNS of swarms with fixed bubbles for the study of bubble-induced turbulence
 - \rightarrow (prospect) Characterise the impact of fixed bubbles
 - \rightarrow (prospect) Comparison with calculation of free bubbles
 - \rightarrow (prospect) Parametric analysis with different Reynolds number and different void fraction





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Turbulence modelling

- Bubble-induced turbulence is different than single-phase turbulence
 - \rightarrow Bubble-induced turbulence has a part of turbulent fluctuation (WIT) and a part of non turbulent fluctuations (WIF)
 - \rightarrow WIF is related to the averaged wake and to the potential flow around bubble
 - \rightarrow WIT is related to wakes interactions and instabilities
 - Those three fluctuations have to be modelled separately
 - \rightarrow SPT : classical transport equation
 - \rightarrow (prospect) WIT : new transport equation modelling
 - \rightarrow (prospect) WIF : algebraic closure

Thank you for your attention !

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